

APPENDIX A
ANCASTER TRANSPORTATION MASTER PLAN PHASE 1 REPORT

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1.0 Transportation Analysis

1.1 Existing Infrastructure and Traffic Data

1.1.1 Existing Infrastructure Inventory

An inventory of the existing roadway infrastructure was undertaken to determine roadway lane geometry, intersection control, intersection lane configurations and posted speed limits. The inventory is illustrated on **Figure 1**.

1.1.2 Existing Traffic Volumes

Existing peak hour turning movement volumes were provided by the City of Hamilton for the following intersections:

1. Fiddler's Green Road and Amberly Boulevard/Calvin Street.
2. Fiddler's Green Road and Garner Road.
3. Fiddler's Green Road and Gilbert Avenue.
4. Fiddler's Green Road and Highway 403 eastbound on ramp.
5. Fiddler's Green Road and Jerseyville Road.
6. Fiddler's Green Road and Wilson Street.
7. Garner Road and Highway 403 on and off ramps.
8. Garner Road and Kitty Murray Lane.
9. Garner Road and Shaver Road.
10. Garner Road and Hamilton Drive.
11. Garner Road and Southcote Road.
12. Golf Links Road and Cloverleaf Drive/Neville Drive.
13. Golf Links Road and Kitty Murray Lane.
14. Golf Links Road and Legend Court/Meadowlands Boulevard.
15. Golf Links Road and Martindale Crescent.
16. Golf Links Road and McNiven Road/Southcote Road.
17. Golf Links Road and Stone Church Road.
18. Highway 6 and Book Road.
19. Jerseyville Road and Lover's Lane.

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20. Jerseyville Road and Wilson Street.
21. Meadowlands Boulevard and Stonehenge Drive.
22. Mohawk Road and Filman Road.
23. Mohawk Road and Lincoln M. Alexander Parkway WB Ramps.
24. Mohawk Road and Scenic Drive/Upper Horning Drive.
25. Mohawk Road/Rousseaux Street and McNiven Road/Lime Kiln Road.
26. Rymal Road and Glancaster Road.
27. Shaver Road and Book Road.
28. Shaver Road and Jerseyville Road.
29. Southcote Road and Stonehenge Drive.
30. Stone Church Road and Harrogate Drive.
31. Stone Church Road and Stonehenge Drive.
32. Stonehenge Drive and Kitty Murray Lane.
33. Sulphur Springs Road and Lover's Lane.
34. Trinity Road and Book Road.
35. Upper Paradise Road and Garner Road/Rymal Road.
36. Wilson Street and Church Street/Sulphur Springs Road.
37. Wilson Street and Fortino's Plaza access.
38. Wilson Street and Garner Road on ramp (west of signal).
39. Wilson Street and Garner Road/Mason Drive.
40. Wilson Street and Halson Street.
41. Wilson Street and Highway 403 eastbound off ramp.
42. Wilson Street and Highway 403 westbound off ramp.
43. Wilson Street and Highway 52/Trinity Road.
44. Wilson Street and Montgomery Drive.
45. Wilson Street and Shaver Road.
46. Wilson Street and Tradewind Drive.
47. Wilson Street and Wal-Mart Plaza access.
48. Wilson Street East and Rousseaux Street/Old Dundas Road.

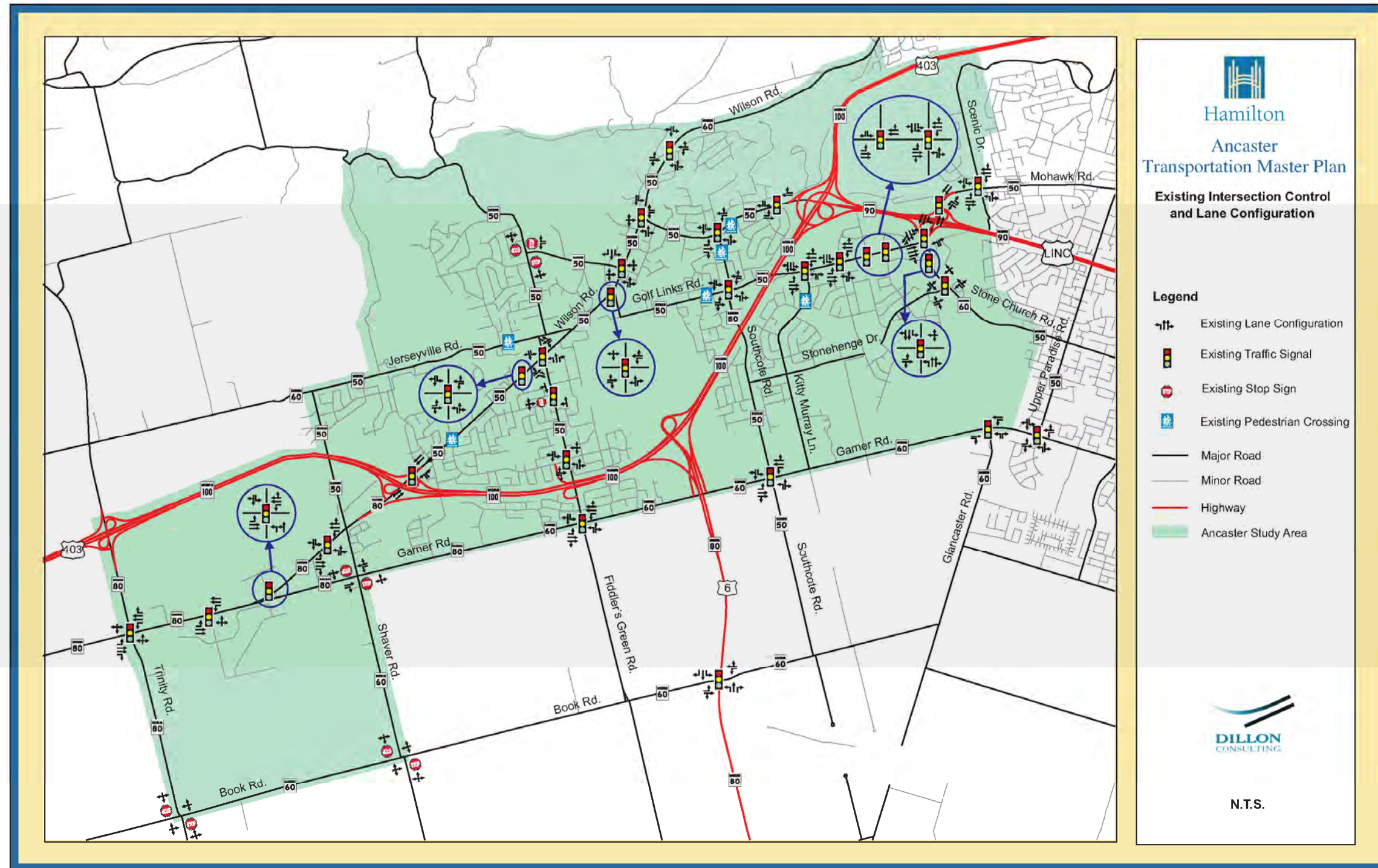


Figure 1 – Infrastructure Inventory

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The counts were undertaken by the City in early to late June of 2008.

Average Annual Daily Traffic (AADT) volumes were also provided for the following roadway segments:

1. Fiddler's Green north of Oakley Crescent.
2. Garner Road east of Shaver Road.
3. Garner Road west of Glancaster Road.
4. Garner Road west of Highway 403 off ramp.
5. Garner Road west of Southcote Road.
6. Golf Links Road west of Chancery Drive.
7. Golf Links Road west of Highway 403.
8. Golf Links Road west of Stone Church Road.
9. Highway 403 between Highway 6 and Lincoln M. Alexander Parkway.
10. Highway 403 east of Highway 52.
11. Highway 403 north of Lincoln M. Alexander Parkway.
12. Highway 52 north of Garner Road.
13. Jerseyville Road east of Lover's Lane.
14. Jerseyville Road west of Shaver.
15. Kitty Murray Lane between Garner Road and access to Redeemer College.
16. Lincoln M. Alexander Parkway east of Golf Links Road.
17. Mohawk Road east of Filman Road.
18. Mohawk Road west of McNiven Road.
19. Mohawk Road west of Scenic Drive/Upper Horning Drive.
20. Old Dundas Road north of Montgomery Drive.
21. Rousseaux Street west of McNiven Road/Lime Kiln Road.
22. Scenic Drive north of Mohawk Road.
23. Shaver Road south of Highway 403.
24. Southcote Road north of Garner Road.
25. Stone Church west of Omni Boulevard.
26. Stonehenge Drive east of Southcote Road.
27. Sulphur Springs Road north of Woodview Crescent.
28. Sulphur Springs Road west of Mansfield Drive.
29. Wilson Street between Highway 403 W-N/S ramp and S-E ramp.

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30. Wilson Street east of Trinity Road.
31. Wilson Street north of Montgomery Drive.
32. Wilson Street south of Academy Street.
33. Wilson Street west of Fiddler's Green.
34. Wilson Street west of Halson Street.

The AADT volumes are illustrated on **Figure 2**.

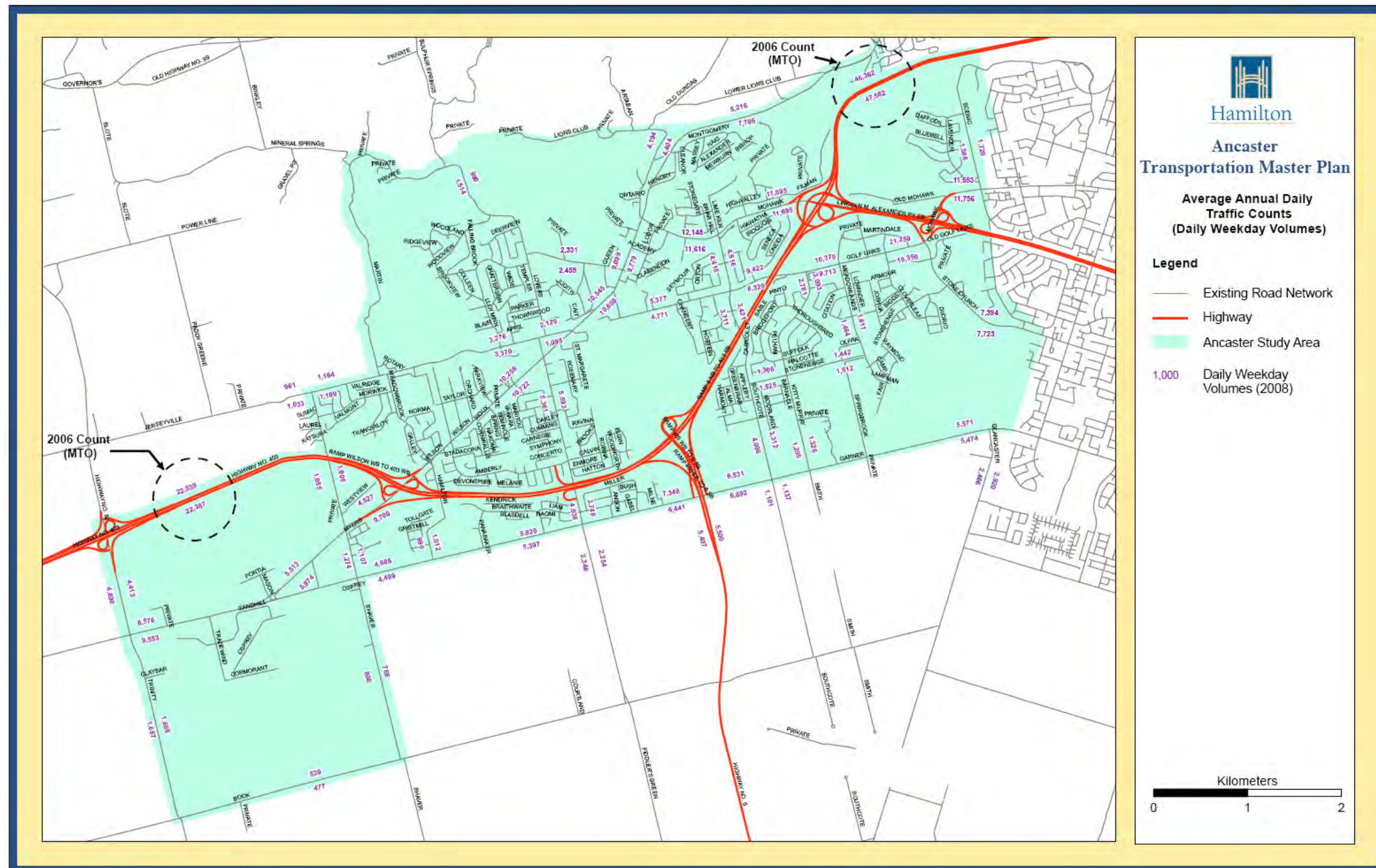


Figure 2 – Average Annual Daily Traffic Volumes

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1.1.3 Traffic Signal Timing and Phasing

Signal timing and phasing were provided for the 31 signalized intersections in the study area:

1. Fiddler's Green Road and Amberly Boulevard/Calvin Street;
2. Fiddler's Green Road and Gilbert Avenue;
3. Fiddler's Green Road and Wilson Street;
4. Golf Links Road and Cloverleaf Drive/Neville Drive;
5. Fiddler's Green Road and Amberly Boulevard/Calvin Street;
6. Fiddler's Green Road and Gilbert Avenue;
7. Fiddler's Green Road and Wilson Street;
8. Golf Links Road and Cloverleaf Drive/Neville Drive;
9. Golf Links Road and Kitty Murray Lane;
10. Golf Links Road and Legend Court/Meadowlands Boulevard;
11. Golf Links Road and Martindale Crescent;
12. Golf Links Road and McNiven Road/Southcote Road;
13. Highway 6 and Book Road;
14. Mohawk Road and Filman Road;
15. Mohawk Road and Lincoln M. Alexander Parkway WB Ramps;
16. Mohawk Road and McNiven Road/Lime Kiln Road;
17. Mohawk Road and Scenic Drive/Upper Horning Drive;
18. Stone Church Road and Golf Links Road;
19. Stone Church Road and Harrogate Drive;
20. Stone Church Road and Stonehenge Drive;
21. Upper Paradise Road and Garner Road/Rymal Road;
22. Wilson Street and Church Street/Sulphur Springs Road;
23. Wilson Street and Fortino's Plaza access;
24. Wilson Street and Garner Road;
25. Wilson Street and Halson Street;
26. Wilson Street and Highway 403 westbound off ramp;
27. Wilson Street and Highway 52/Trinity Road;
28. Wilson Street and Montgomery Drive;
29. Wilson Street and Rousseaux Street;

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30. Wilson Street and Tradewind Drive; and
31. Wilson Street and Wal-Mart Plaza access.

With the exception of the Book Road/Fiddler's Green Road, Garner Road/Southcote Road, Garner Road/Fiddler's Green Road, and Glanaster Road/Rymal Road intersections, all signal timings provided are relatively new.

1.2 Transportation Network Analysis

A transportation network operational analysis was undertaken to assess the existing conditions at signalized intersections for the Ancaster Transportation Master Plan study area.

1.2.1 Existing Transportation Assessment

The existing transportation assessment was undertaken for signalized intersections within the Ancaster study area for the weekday morning and afternoon peak periods to identify current capacity constraints. Additional assessment was conducted for signalized intersections along the Golf Links Road corridor for the Saturday peak period to reflect the increase in traffic demand generated by adjacent retail and commercial developments. The Synchro (version 6) software package was utilized to evaluate the operational performance of the signalized intersections. Synchro employs the Highway Capacity Manual (HCM) techniques for signalized intersections. This analysis method generates performance measures for signalized intersections, including average delay and Level of Service (LOS) for each intersection as a whole and on a per movement basis.

LOS is a measure used to quantify the amount of delay experienced by motorists at an intersection or particular movement. HCM measures Level of Service as a range from LOS A to LOS F, where LOS A reflects excellent conditions with little or no delay and LOS F reflects congested conditions and failure of the movement or intersection with significant delays experienced by motorist.

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The operational performance of the signalized intersections within the study area were measured using the intersection HCM (overall) volume-to-capacity (v/c) ratio and the corresponding LOS for the Weekday AM, PM, and Saturday peak hours. In the case of individual turning movements, those movements / lane groups with either a v/c ratio in excess of 0.85 or a LOS below D or both were identified as “critical” movements. Turning movements meeting these “critical” criteria are approaching capacity and prone to poor operation during the peak periods.

AM Peak Hour

The analysis indicates that the majority of the signalized intersections is currently operating at a LOS C or better during the Weekday AM peak hour (**Table 1**). The exception is the Wilson Street and Rousseaux Street/Old Ancaster Road, which operates at a LOS E with a corresponding v/c ratio of 0.82.

Table 1 – Weekday AM Peak Hour Signalized Intersection Performance

| Intersection Location | Overall Intersection | | Critical Movements | | | |
|--|----------------------|------|---------------------|-----|------------|-----------------|
| | LOS | v/c | Approach & Movement | LOS | v/c > 0.85 | Delay (sec/veh) |
| Fiddler’s Green Road and Amberly Boulevard/Calvin Street | B | 0.53 | N/A | | | |
| Fiddler’s Green Road and Gilbert Avenue | A | 0.37 | N/A | | | |
| Fiddler’s Green and Garner Road | B | 0.66 | N/A | | | |
| Fiddler’s Green Road and Wilson Street | C | 0.66 | NBL | F | 0.95 | 88.7 |
| Garner Road and Southcote Road | A | 0.47 | N/A | | | |
| Garner Road and Glancaster Road | B | 0.34 | N/A | | | |
| Golf Links Road and Cloverleaf Drive/Neville Drive | B | 0.45 | N/A | | | |
| Golf Links Road and Kitty Murray Lane | B | 0.37 | N/A | | | |

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| Intersection Location | Overall Intersection | | Critical Movements | | | |
|--|----------------------|------|---------------------|-----|------------|-----------------|
| | LOS | v/c | Approach & Movement | LOS | v/c > 0.85 | Delay (sec/veh) |
| Golf Links Road and Legend Court/Meadowlands Boulevard | B | 0.38 | N/A | | | |
| Golf Links Road and Martindale Crescent | B | 0.45 | N/A | | | |
| Golf Links Road and McNiven Road/Southcote Road | B | 0.60 | N/A | | | |
| Highway 6 and Book Road | A | 0.47 | N/A | | | |
| Mohawk Road and Filman Road | A | 0.82 | EBT | B | 0.86 | 10.9 |
| Mohawk Road and Lincoln M. Alexander Parkway WB Off-ramp | B | 0.39 | N/A | | | |
| Mohawk Road/Rousseaux Street and McNiven Road/Lime Kiln Road | C | 0.84 | EBT | C | 0.90 | 28.0 |
| Mohawk Road and Scenic Drive/Upper Horning Drive | B | 0.44 | N/A | | | |
| Rymal Road and Upper Paradise Road | B | 0.56 | N/A | | | |
| Stone Church Road and Golf Links Road | C | 0.58 | N/A | | | |
| Stone Church Road and Harrogate Drive | A | 0.21 | N/A | | | |
| Stone Church Road and Stonehenge Drive | A | 0.43 | N/A | | | |
| Wilson Street and Church Street/Sulphur Springs Road | B | 0.66 | N/A | | | |
| Wilson Street and Fortino's Plaza | B | 0.44 | N/A | | | |
| Wilson Street and Garner Road | A | 0.33 | N/A | | | |
| Wilson Street and Halson Street | B | 0.68 | N/A | | | |
| Wilson Street and Highway 403 WB Off-ramp | B | 0.78 | N/A | | | |

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| Intersection Location | Overall Intersection | | Critical Movements | | | |
|--|----------------------|------|---------------------|-----|------------|-----------------|
| | LOS | v/c | Approach & Movement | LOS | v/c > 0.85 | Delay (sec/veh) |
| Wilson Street and Highway 52/Trinity Road | B | 0.40 | N/A | | | |
| Wilson Street and Montgomery Drive | A | 0.71 | N/A | | | |
| Wilson Street and Rousseaux Street/Old Ancaster Road | D | 0.82 | EBT | E | 0.88 | 62.5 |
| | | | NBT | D | 0.85 | 53.6 |
| | | | SBL | D | 0.87 | 48.7 |
| Wilson Street and Tradewind Drive | C | 0.76 | N/A | | | |
| Wilson Street and Wal-Mart Plaza | A | 0.38 | N/A | | | |

Individual turning movements beyond the critical threshold (v / c ratio > 0.85) include the following:

Fiddler's Green Road and Wilson Street

The northbound left turn movement experiences a LOS F with a corresponding v/c ratio of 0.95. The movement experiences delays of 88.7 seconds per vehicle as motorists wait for a gap in opposing traffic to make the left turn movement.

Mohawk Road and Filman Road

The eastbound through movement experiences a LOS B with a corresponding v/c ratio of 0.86 and delays of 10.9 seconds per vehicle. Although the movement is beyond the critical threshold it is below capacity and the delay experienced is considered minor.

Mohawk Road/Rousseaux Street and McNiven Road/Lime Kiln Road

The eastbound through movement experiences a LOS C with a corresponding v/c ratio of 0.90 and delays of 28 seconds per vehicle. Although the movement is beyond the critical threshold it is below capacity and the delay experienced is considered acceptable.

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Wilson Street and Rousseaux Street/Old Ancaster Road

The eastbound through movement experiences a LOS E with a corresponding v/c ratio of 0.88 and delays of 62.5 seconds per vehicle. The northbound through movement experiences a LOS D with a corresponding v/c ratio of 0.85 and delays of 53.6 seconds per vehicle. The southbound left turn movement experiences a LOS D with a corresponding v/c ratio of 0.87 and delays of 48.7 seconds per vehicle.

PM Peak Hour

The analysis indicates that the majority of the signalized intersections are currently operating at a LOS C or better during the Weekday PM peak hour (**Table 2**). The exceptions are the intersections at Fiddler's Green Road and Wilson Street, and at Wilson Street and Rousseaux Street/Old Ancaster Road, which operates at a LOS D (v/c ratio of 0.89) and LOS E (v/c ratio of 1.04) respectively.

Table 2 – Weekday PM Peak Hour Signalized Intersection Performance

| Intersection Location | Overall Intersection | | Critical Movements | | | |
|--|----------------------|------|---------------------|-----|------------|-----------------|
| | LOS | v/c | Approach & Movement | LOS | v/c > 0.85 | Delay (sec/veh) |
| Fiddler's Green Road and Amberly Boulevard/Calvin Street | B | 0.61 | N/A | | | |
| Fiddler's Green Road and Gilbert Avenue | A | 0.40 | N/A | | | |
| Fiddler's Green and Garner Road | B | 0.42 | N/A | | | |
| Fiddler's Green Road and Wilson Street | D | 0.89 | NBL | E | 0.94 | 68.3 |
| | | | EBT | D | 0.88 | 35.9 |
| | | | WBL | D | 0.91 | 50.3 |
| | | | WBT | D | 0.93 | 43.8 |
| Garner Road and Southcote Road | A | 0.49 | N/A | | | |
| Garner Road and Glancaster Road | B | 0.35 | N/A | | | |
| Golf Links Road and Cloverleaf Drive/Neville Drive | C | 0.83 | NBL | F | 0.97 | 87.5 |
| | | | SBL | E | 0.93 | 56.7 |

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| Intersection Location | Overall Intersection | | Critical Movements | | | |
|--|----------------------|------|---------------------|-----|------------|-----------------|
| | LOS | v/c | Approach & Movement | LOS | v/c > 0.85 | Delay (sec/veh) |
| Golf Links Road and Kitty Murray Lane | C | 0.63 | N/A | | | |
| Golf Links Road and Legend Court/Meadowlands Boulevard | B | 0.53 | N/A | | | |
| Golf Links Road and Martindale Crescent | C | 0.93 | EBL | E | 0.91 | 62.8 |
| | | | WBT | C | 0.99 | 34.3 |
| | | | SBL | D | 0.86 | 48.2 |
| Golf Links Road and McNiven Road/Southcote Road | C | 0.90 | WBL | D | 0.91 | 51.3 |
| | | | SBL | D | 0.89 | 47.0 |
| Highway 6 and Book Road | B | 0.55 | N/A | | | |
| Mohawk Road and Filman Road | A | 0.49 | N/A | | | |
| Mohawk Road and Lincoln M. Alexander Parkway WB Off-ramp | C | 0.57 | N/A | | | |
| Mohawk Road/Rousseaux Street and McNiven Road/Lime Kiln Road | C | 0.80 | N/A | | | |
| Mohawk Road and Scenic Drive/Upper Horning Drive | B | 0.59 | N/A | | | |
| Rymal Road and Upper Paradise Road | B | 0.59 | N/A | | | |
| Stone Church Road and Golf Links Road | C | 0.82 | NBL | E | 0.88 | 55.7 |
| Stone Church Road and Harrogate Drive | A | 0.40 | N/A | | | |
| Stone Church Road and Stonehenge Drive | A | 0.61 | N/A | | | |
| Wilson Street and Church Street/Sulphur Springs Road | B | 0.60 | N/A | | | |
| Wilson Street and Fortino's Plaza | B | 0.77 | SBL | F | 0.95 | 83.1 |
| Wilson Street and Garner Road | B | 0.41 | N/A | | | |

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| Intersection Location | Overall Intersection | | Critical Movements | | | |
|--|----------------------|------|---------------------|-----|------------|-----------------|
| | LOS | v/c | Approach & Movement | LOS | v/c > 0.85 | Delay (sec/veh) |
| Wilson Street and Halson Street | C | 0.78 | NBTL | E | 0.95 | 57.4 |
| Wilson Street and Highway 403 WB Off-ramp | C | 0.84 | EBT | D | 0.97 | 44.1 |
| Wilson Street and Highway 52/Trinity Road | B | 0.52 | N/A | | | |
| Wilson Street and Montgomery Drive | A | 0.72 | N/A | | | |
| Wilson Street and Rousseaux Street/Old Ancaster Road | E | 1.00 | EBT | E | 0.92 | 76.6 |
| | | | WBL | E | 0.93 | 68.4 |
| | | | NBT | E | 0.85 | 58.9 |
| | | | SBL | F | 1.13 | 123.7 |
| Wilson Street and Tradewind Drive | C | 0.62 | NBLR | D | 0.88 | 37.2 |
| Wilson Street and Wal-Mart Plaza | A | 0.51 | N/A | | | |

Individual turning movements beyond the critical threshold (v / c ratio > 0.85) include the following:

Fiddler's Green Road and Wilson Street

The northbound left turn movement experiences a LOS E with a corresponding v/c ratio of 0.94 and delays of 68.3 seconds per vehicle. The eastbound through movement experiences a LOS D with a corresponding v/c ratio of 0.88 and delays of 35.9 seconds per vehicle. The westbound left turn movement experiences a LOS D with a corresponding v/c ratio of 0.91 and delays of 50.1 seconds per vehicle. The westbound left through movement experiences a LOS D with a corresponding v/c ratio of 0.93 and delays of 43.6 seconds per vehicle.

Golf Links Road and Cloverleaf Drive/Neville Drive

The northbound left turn movement experiences a LOS F with a corresponding v/c ratio of 0.97 and delays of 87.5 seconds per vehicle. The southbound left turn movement

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experiences a LOS E with a corresponding v/c ratio of 0.93 and delays of 56.7 seconds per vehicle.

Golf Links Road and Martindale Crescent

The eastbound left turn movement experiences a LOS E with a corresponding v/c ratio of 0.91 and delays of 62.8 seconds per vehicle. The westbound through movement experiences a LOS C with a v/c ratio of 0.99 and delays of 34.3 seconds per vehicle. The southbound left turn movement experiences a LOS D with a v/c ratio of 0.86 and delays of 48.2 seconds per vehicle.

Golf Links Road and McNiven Road/Southcote Road

The westbound left turn movement experiences a LOS D with a corresponding v/c ratio of 0.91 and delays of 51.3 seconds per vehicle. The southbound left turn movement also experiences a LOS D with a v/c ratio of 0.89 and delays of 47.0 seconds per vehicle.

Stone Church Road and Golf Links Road

The northbound left turn movement experiences a LOS D with a corresponding v/c ratio of 0.88 and delays of 54.5 seconds per vehicle.

Wilson Street and Fortino's Plaza

The southbound left turn movement experiences a LOS F with a corresponding v/c ratio of 0.95 and delays of 83.1 seconds per vehicle.

Wilson Street and Highway 403 WB Off-ramp

The eastbound through movement experiences a LOS D with a v/c ratio of 0.97 and delays of 44.1 seconds per vehicle.

Wilson Street and Rousseaux Street/Old Ancaster Road

The eastbound through movement experiences a LOS E with a corresponding v/c ratio of 0.92 and delays of 76.6 seconds per vehicle. The westbound left turn movement experiences a LOS E with a v/c ratio of 0.93 and delays of 68.4 seconds per vehicle. The northbound through movement also experiences a LOS E with a v/c ratio of 0.85 and delays of 58.9 seconds per vehicle. The southbound left turn movement is over

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capacity with a v/c ratio of 1.13 and corresponding LOS F, delays reach 123.7 seconds per vehicle.

Overall, the signalized intersections currently operate with sufficient capacity to accommodate the existing traffic volumes during the AM and PM peak hours with the exception of the Wilson Street and Rousseaux Street/Old Ancaster Road intersection, which is over capacity in the PM peak hour with a v/c ratio of 1.04. Congestion at the intersection can be attributed to the high volume of commuting traffic to/from the Lincoln M. Alexander Parkway and crossing the escarpment along Wilson Street. Old Ancaster Road is also utilized by commuters originating from the Town of Dundas to access the Lincoln M. Alexander Parkway and the Meadowlands commercial area, adding to the congestion experienced at the intersection.

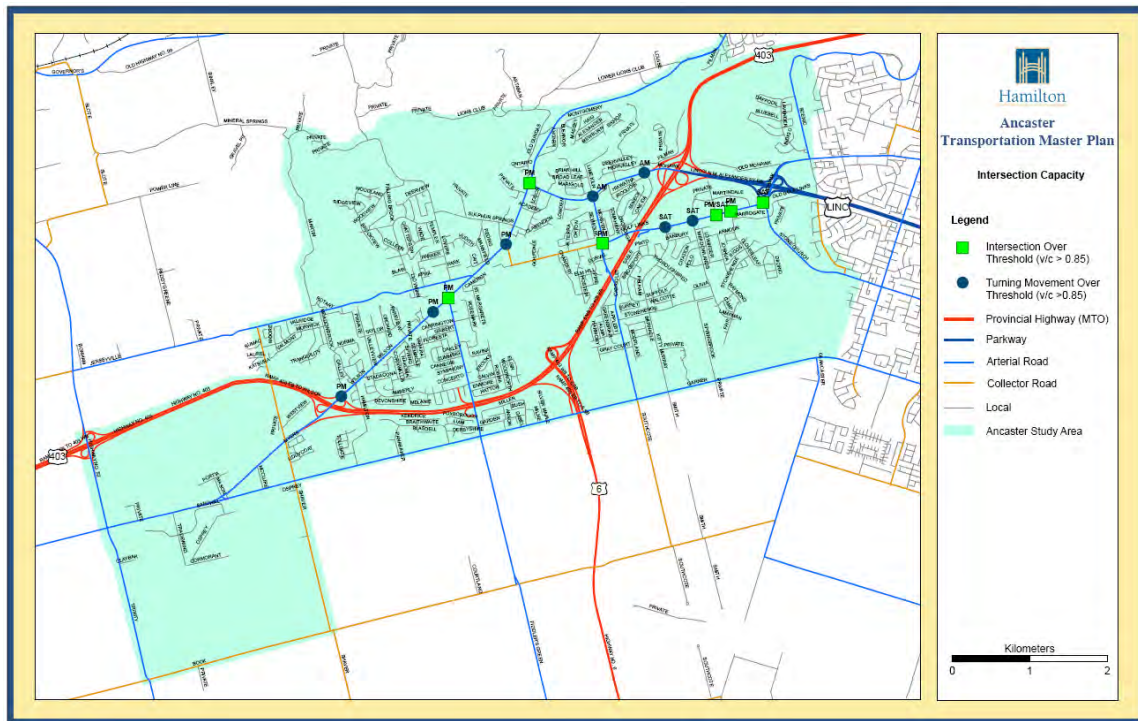


Figure 3 – Intersection Constraints

1.3 Existing Infrastructure Condition

1.3.1 Pavement Condition

The condition of the paved infrastructure within the Ancaster Study area has been assessed by City staff for each road segment and is illustrated on **Figure 4**. Pavement deterioration is site specific since it depends on many variables (environment, traffic, pavement type/structure and sub grade condition), which makes the deterioration rates vary significantly from one pavement section to another.



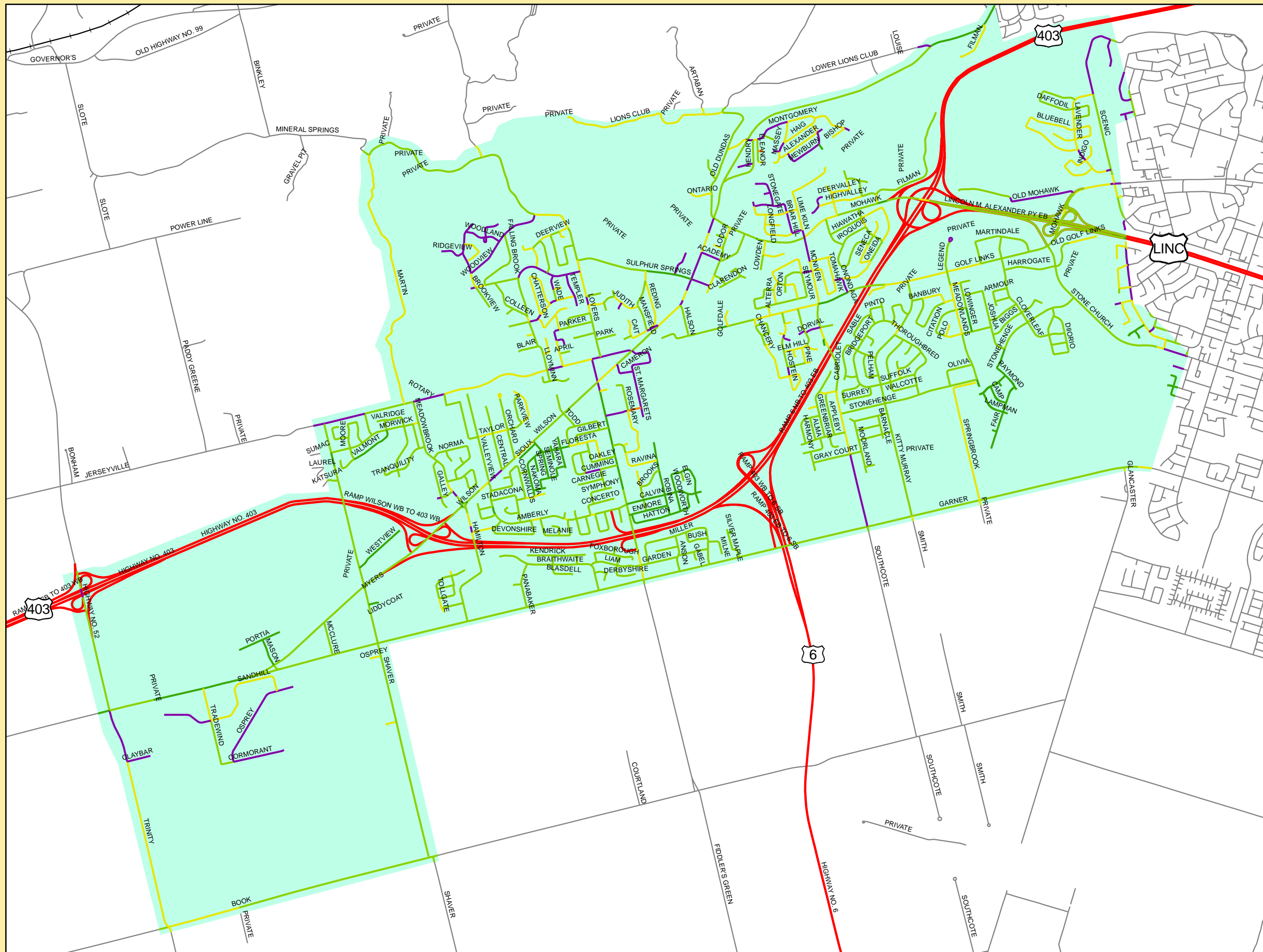
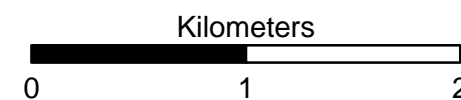
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Figure 4 Road Condition Index

Legend

- Existing Road Network
- Highway
- Ancaster Study Area
- Road Condition**
- Excellent
- Good
- Adequate
- Poor
- Deficient



The following major road segments within the Ancaster study area have been assessed as being deficient and may require preventative maintenance and/or rehabilitation:

- Southcote Road
 - South of Gray Court Drive
- Wilson Street
 - Between Valleyview Drive and Central Drive
 - Between Halson Street and Rousseaux Street
- Jerseyville Road
 - East of Fiddler's Green Road
 - Between Meadowbrook Drive and Valleyview Drive
 - West of Stevenson Street
- Stone Church Road
 - East of Omni Boulevard
- Scenic Drive
 - North of Daffodil Crescent
- Mohawk Road
 - East of Scenic Drive.

All other major roadways within the study area are currently within their functional life cycle.

1.3.2 Summary of Transportation Problems/Opportunities/Constraints

Based on an evaluation of the existing conditions and through input received from the public and technical agencies, there have been a number of transportation problems/opportunities identified. A summary of these problems/opportunities in a broad context are as follows:

- Impacts of commuter traffic infiltration and congestion on the ability to preserve Ancaster's historic urban street character;
- Safety and operational traffic problems and the potential need for increased capacity on roadways and intersections within the study area;
- Traffic impacts of development areas;
- Capacity constraints on external road linkages (i.e., escarpment crossings, Highway 403);
- Limited network connectivity to Highway 403 (lack of westbound ramps) to provide alternative access and deal with Highway 403 emergency/traffic congestion impacts;
- Lack of east-west network connectivity within the community;
- Impacts of external truck traffic;
- Travel Demand Management opportunities within the ATMP study area;
- Local transit service modifications/enhancements opportunities; and
- Cycling, trails and pedestrian facility enhancements opportunities.

APPENDIX C
TRANSPORTATION MODELLING REPORT

**City of Hamilton
Ancaster Transportation
Master Plan**

*Technical Paper on Travel Demand
Forecasting*

June 2011

City of Hamilton

Project No. 08-8952

Submitted by

**Dillon Consulting
Limited**

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Note: Exhibits are located at the end of this document.

LIST OF OPERATIONAL OUTPUTS

- FHWA Roundabout Analysis
- Synchro 2016 AM Peak Hour Recommended Mitigation
- Synchro 2016 PM Peak Hour Recommended Mitigation
- Synchro 2021 AM Peak Hour Recommended Mitigation
- Synchro 2021 PM Peak Hour Recommended Mitigation
- Synchro 2031 AM Peak Hour Recommended Mitigation
- Synchro 2031 PM Peak Hour Recommended Mitigation

Note: Operational Outputs are located at the end of this document.

1.0 INTRODUCTION

An analysis of the existing transportation network in the Ancaster Transportation Master Plan (ATMP) study area was undertaken using the City of Hamilton's AM Peak Hour Travel Demand Model that is used to help determine future transportation infrastructure needs.

The Hamilton model is built using Inro's EMME/2 software package and is comprised of approximately 400 transportation zones covering the Greater Golden Horseshoe area from Toronto to Niagara. The model is an AM peak period model, reflecting travel in the morning peak 3-hour period, comprising trips starting between 6:00 a.m. and 8:59 a.m. This AM peak 3-hour period has been adopted as a Greater Golden Horseshoe (GGH) standard for travel demand forecasting.

This document describes the steps taken to refine the model to a suitable level of detail in the Ancaster area for use in the ATMP.

1.1 Hamilton Model Trip Purposes

Travel in the model is estimated based on the three major trip purposes of home-based work, home-based school and home-based discretionary. Using Transportation Tomorrow Survey (TTS) definitions, work trips are categorized into professional, manufacturing and office, with each work category modeled separately. School was categorized into secondary school (high school) and post-secondary school.

1.2 Hamilton Model Travel Modes

The existing Hamilton model contained data representing trips with the auto travel mode, but did not contain transit, active, or other mode trip data. As such, the model used for this project relied on TTS data and did not specifically analyze non-auto modes.

Table 1 provides an overview of the various trip purposes for the Ancaster study area zones.

Table 1 – 2006 TTS Data - AM Peak Period (06:00 - 08:59)

| | Trip purpose | Auto Driver | Auto pas. | GO Rail | Local Transit | School bus | Walk/Cycle |
|------------------------------|--------------------------|--------------|--------------|-------------|---------------|--------------|-------------|
| Ancaster origins | | | | | | | |
| | Home-based Work | 91.0% | 5.9% | 1.7% | 0.7% | 0.0% | 0.7% |
| | Home-based School | 7.4% | 24.6% | 0.0% | 6.9% | 43.1% | 17.9% |
| | Home-based Discretionary | 89.9% | 9.1% | 0.0% | 0.6% | 0.0% | 0.5% |
| | Non Home-based | 93.5% | 2.5% | 4.0% | 0.0% | 0.0% | 0.0% |
| | Total | 69.9% | 11.0% | 1.1% | 2.2% | 10.9% | 4.9% |
| Ancaster destinations | | | | | | | |
| | Home-based Work | 88.1% | 8.1% | 0.0% | 3.1% | 0.0% | 0.7% |
| | Home-based School | 6.2% | 20.9% | 0.0% | 3.5% | 51.9% | 17.5% |
| | Home-based Discretionary | 93.7% | 5.2% | 0.0% | 0.6% | 0.0% | 0.6% |
| | Non Home-based | 83.6% | 7.5% | 0.0% | 2.0% | 7.0% | 0.0% |
| | Total | 65.4% | 11.1% | 0.0% | 2.5% | 15.6% | 5.4% |

2.0 MODEL REFINEMENT PROCESS

The development of the Ancaster sub-area from the city-wide model required the combination of data sources to develop the 2006 base year Ancaster model used for analysis. Examining the existing Hamilton city-wide model, the Ancaster sub-area did not contain sufficient enough detail. There was a need to perform changes to the model road network and transportation zone structure. The existing Hamilton model, developed by IBI Group, contains only network and trip table data for 2004 and 2011. Available land use data includes population and employment numbers for 2006, but not 2004. In order to resolve these discrepancies, the 2011 network was adopted as the most appropriate base network to represent the 2006 road network within the study area.

2.1 Model Input Data

Dillon obtained the following relevant information from the city-wide model as inputs to the Ancaster study area model:

- Networks for 2004, 2011, 2021 and 2031;
- AM peak hour auto trip matrices for 2004, 2011, 2021 and 2031;
- AM peak hour total person trip matrices for 2004, 2011, 2021 and 2031;
- City of Hamilton population data for 2001, 2006, 2011, 2016, 2021 and 2031;

- City of Hamilton employment data for 2001, 2011, 2021 and 2031; and
- IBI Group's Model Development Draft Report (Dated April 2005).

In order to ensure accuracy in the EMME/2 network, City of Hamilton input and available documentation was utilized including, but not limited to, the following:

- Scope of Work for Wilson Street at Rousseaux Street Intersection Operation Analysis (2007);
- GRIDS (Growth Related Infrastructure Development Strategy);
- Post-GRIDS population adjustments based on additional development approvals;
- Existing Ancaster Official Plan;
- City of Hamilton Transportation Master Plan (2007);
- Ancaster Comprehensive Transportation Study (2001);
- Relevant information from Vision 2020;
- City Capital Program;
- *City Planning and Economic Development Department* – Existing land use, community features, and development applications; and
- *City Public Works Department* – Existing traffic data and road network characteristics.

2.2 Road Network Modifications

The base year road network used in the Hamilton EMME/2 model was reviewed for accuracy within the study area, including speed and capacity, and additional detail added for consistency with the zone system. Changes made include the addition of roadway links, the splitting of various zones to reflect current land use patterns and barriers, the addition of required centroid connectors, and revisions to existing connectors.

In order to more accurately represent existing conditions, road network modifications were made in the 2006 base EMME/2 network as shown in **Table 2** and illustrated in **Figure 1**. The resulting base network speed and capacity diagram is shown in **Figure 2**.

Care was taken to accurately depict the model road network based on existing conditions. At this level of analysis, model performance is evaluated on a “screenline” level of detail (i.e. a comparison of simulated vs. counted vehicle volumes along key sections). As such, road network attributes (i.e. speed, capacity, etc.) may have been modified in order to match model results to existing conditions.

The 2016, 2021, and 2031 road network modifications are discussed in **Section 4.0**.

Table 2 – 2006 Base EMME/2 Network Modifications

| Location | Network Modification | Justification |
|--|---|--|
| Highway 6 between Highway 403 and Upper James | <ul style="list-style-type: none"> Roadway link added | <ul style="list-style-type: none"> Accurately represent existing road network |
| Garth Street between Rymal Road and Twenty Road | <ul style="list-style-type: none"> Roadway link added | <ul style="list-style-type: none"> Accurately represent existing road network |
| Hamilton Drive from Wilson Street to Garner Road | <ul style="list-style-type: none"> Roadway link added representing residential collector with 50 km/h speed | <ul style="list-style-type: none"> Roadway represents a significant access point to/from Ancaster and surrounding area |
| Kitty Murray Lane from Golf Links Road to Garner Road | <ul style="list-style-type: none"> Roadway link added representing residential collector with 50 km/h speed | <ul style="list-style-type: none"> Differentiate demand from parallel Southcote Rd corridor for north-south trips accessing Ancaster and Redeemer College Better represent demand at Southcote & Golf Links intersection |
| Stonehenge Road from Kitty Murray Lane to Southcote Road | <ul style="list-style-type: none"> Roadway link added representing residential collector with 50 km/h speed | <ul style="list-style-type: none"> Differentiate demand from parallel Golf Links Rd corridor for east-west trips accessing Ancaster and Redeemer College Better represent demand at Southcote & Golf Links intersection |
| Sulphur Springs Road from Lovers Lane to Wilson Street | <ul style="list-style-type: none"> Roadway link added representing residential / commercial collector with 50 km/h speed | <ul style="list-style-type: none"> Better represent demand along Wilson Street at Fiddler's Green and Jerseyville intersections |
| Old Dundas Road from Wilson Street to Old Ancaster Road | <ul style="list-style-type: none"> Roadway link added representing residential / commercial collector with 50 km/h speed | <ul style="list-style-type: none"> Better represent demand along Wilson Street in northeast area of Ancaster |
| Lovers Lane & Sulphur Springs Road from Jerseyville Road to Governors Road | <ul style="list-style-type: none"> Modify link speed limit to 50 km/h | <ul style="list-style-type: none"> Accurately represent existing network conditions |
| Hwy 403 / Mohawk Road interchange | <ul style="list-style-type: none"> Mohawk Road eastbound to Hwy 403 southbound ramp removed | <ul style="list-style-type: none"> Accurately depict existing network at interchange |
| Mohawk Road from McNiven Road to Highway 403 | <ul style="list-style-type: none"> Reduce roadway capacity to represent 2-lane residential arterial | <ul style="list-style-type: none"> Accurately represent existing network conditions |

| Location | Network Modification | Justification |
|---|--|---|
| Wilson Street from Montgomery Drive to Highway 403 | <ul style="list-style-type: none"> • Modify link speed limit to 60 km/h • Reduce capacity to represent two-lane urban arterial | <ul style="list-style-type: none"> • Accurately represent existing network conditions |
| Old Dundas Road from Montgomery Drive to Wilson Street | <ul style="list-style-type: none"> • Roadway link added representing one-way residential collector | <ul style="list-style-type: none"> • Accurately represent existing network conditions |
| Garner Road from Wilson Street to Southcote Road | <ul style="list-style-type: none"> • Reduce capacity to represent 2-lane major arterial | <ul style="list-style-type: none"> • Accurately represent existing network conditions |
| McNiven Road from Mohawk Road to Golf Links Road | <ul style="list-style-type: none"> • Reduce capacity to represent 2-lane minor arterial | <ul style="list-style-type: none"> • Accurately represent existing network conditions |
| Southcote Road from Golf Links Road to Garner Road | <ul style="list-style-type: none"> • Reduce speed limit to 50 km/h | <ul style="list-style-type: none"> • Accurately represent existing network conditions |
| Jerseyville Road from Meadowbrook Drive to Fiddler's Green Road | <ul style="list-style-type: none"> • Reduce speed limit to 70 km/h | <ul style="list-style-type: none"> • Accurately represent existing network conditions |
| Morwick Drive from Shaver Road to Meadowbrook Drive | <ul style="list-style-type: none"> • Roadway link added representing a residential collector | <ul style="list-style-type: none"> • Added to better load vehicle trips onto network from local traffic zone |
| Stevenson Street from Jerseyville Road to Morwick Drive | <ul style="list-style-type: none"> • Roadway link added representing a residential collector | <ul style="list-style-type: none"> • Added to better load vehicle trips onto network from local traffic zone |
| Lloyminn Avenue from Jerseyville Road to Lovers Lane | <ul style="list-style-type: none"> • Roadway link added representing a residential collector | <ul style="list-style-type: none"> • Added to better load vehicle trips onto network from local traffic zone |
| Mohawk Road, west of Highway 403 interchange | <ul style="list-style-type: none"> • Added turning movement ban for U-turns | <ul style="list-style-type: none"> • Illegal turning movements being performed in model • Forces trips onto proper ramp |

Notes:

¹ *Future Horizon Years (2016, 2021, 2031) Only*











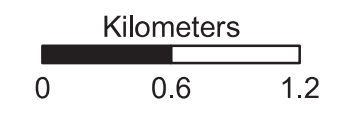
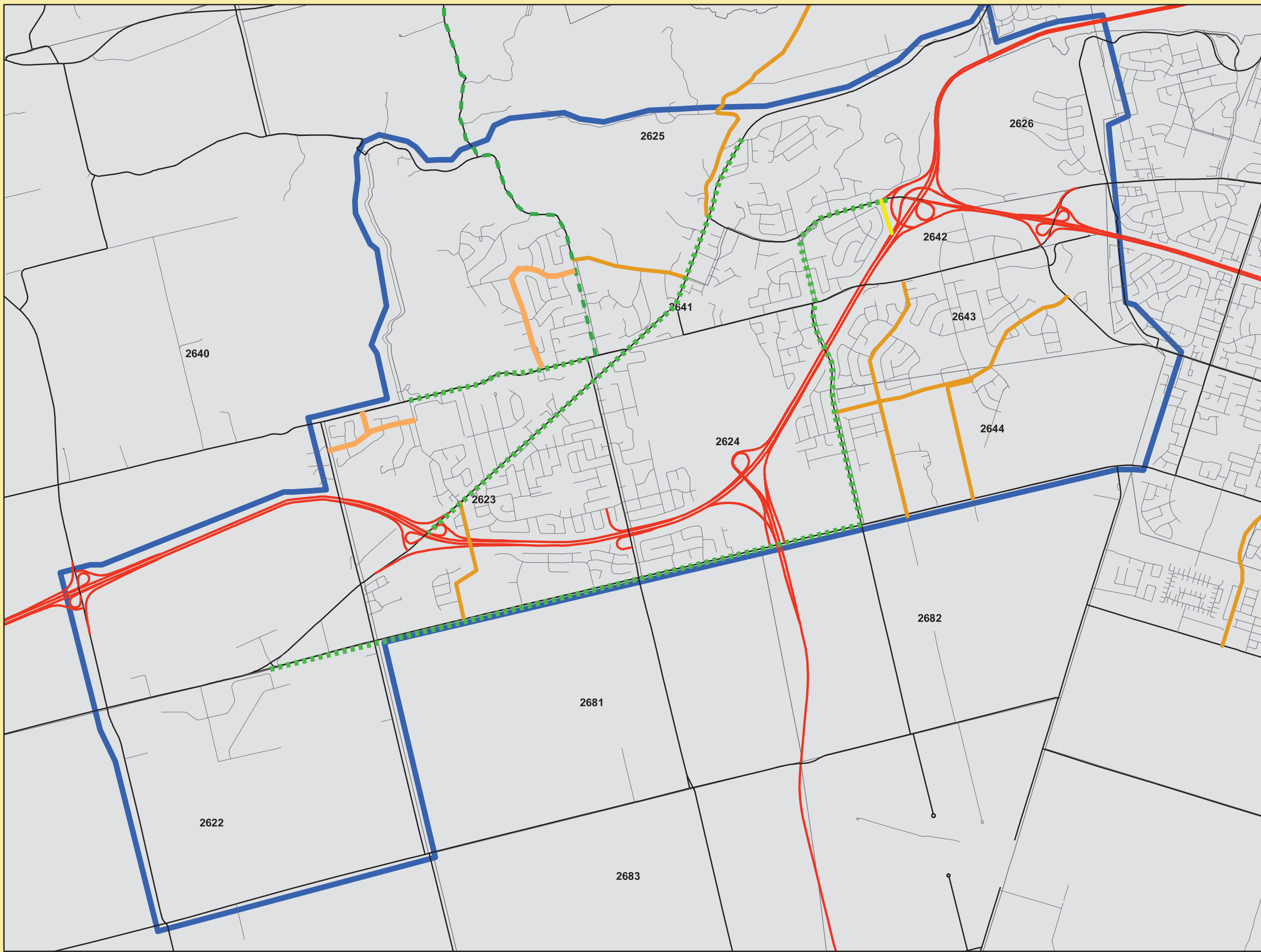
Hamilton

Ancaster Transportation Master Plan

Figure 1
Network Modifications

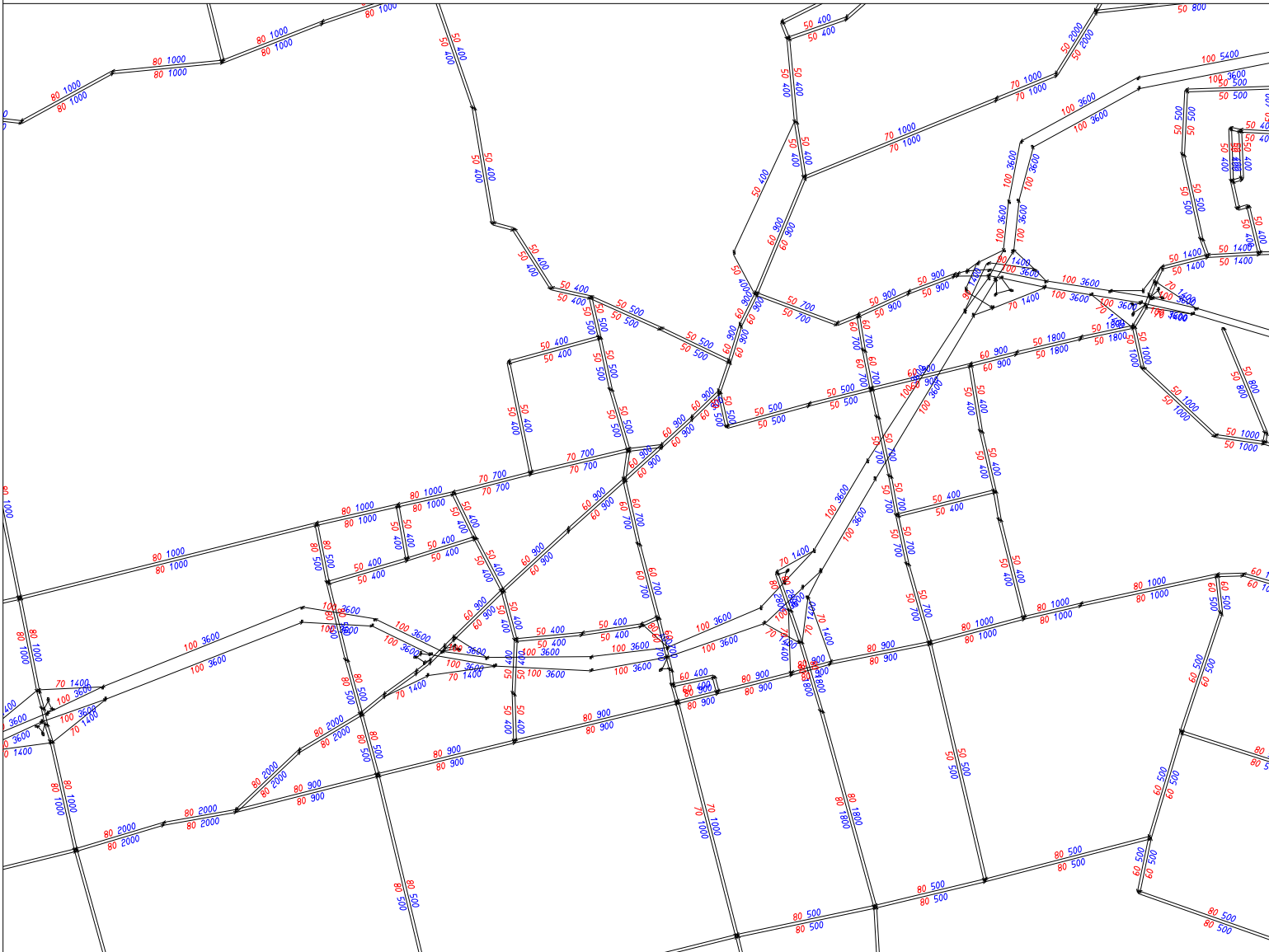
Legend

-  Deleted Link
-  Modified Link
-  New Links
-  Highway
-  Major Road
-  Minor Road
-  Ancaster Study Area
-  Model Zones



FREE FLOW SPEED & TOTAL ROAD CAPACITY (1 WAY)

emme/2



LINKS:
mod=c
&!ci=1
&!cj=1

LAYERS:
Capacity
Speed

Figure 2

WINDOW:
577261/ 781716
587402/ 789321

EMME/2 PROJECT: Hamilton Airport
SCENARIO 5000: 2006 Ancaster TMP (2010-08-13)

10-08-13 16:59
MODULE: 2.13
DMG.UTYU...jdk

2.3 Modifications to Base Zone Structure

The data used as input to the Hamilton model is based on the modified Greater Toronto Area (GTA) zone system developed by the Data Management Group (DMG). Overall, there are 195 zones in Hamilton, ten of which make up the majority of the Ancaster study area. The original zone system used as part of the Hamilton Transportation Master Plan (HTMP) is illustrated on **Figure 3**.

In order to provide a finer level of evaluation, reflect recent development patterns, and delineate a number of combined commercial/residential zones, the zone system in Ancaster sub-area was expanded to 26 zones. The zone system used in the Ancaster Transportation Master Plan (ATMP) is shown in **Figure 4**.



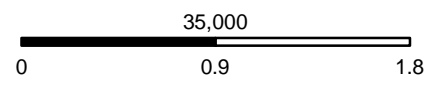
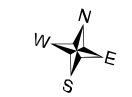
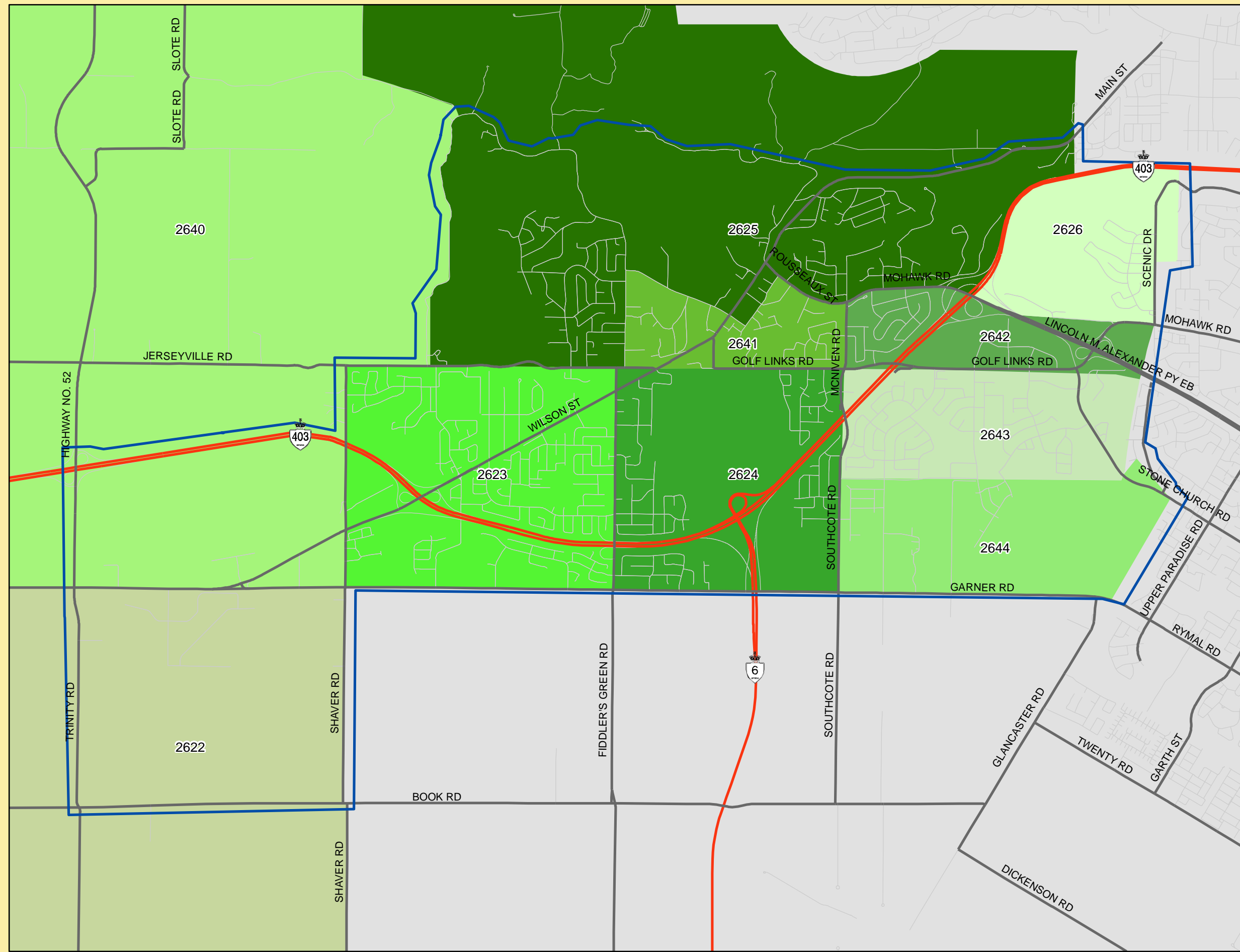
Hamilton

Ancaster Transportation Master Plan

Figure 3 Transportation Zones

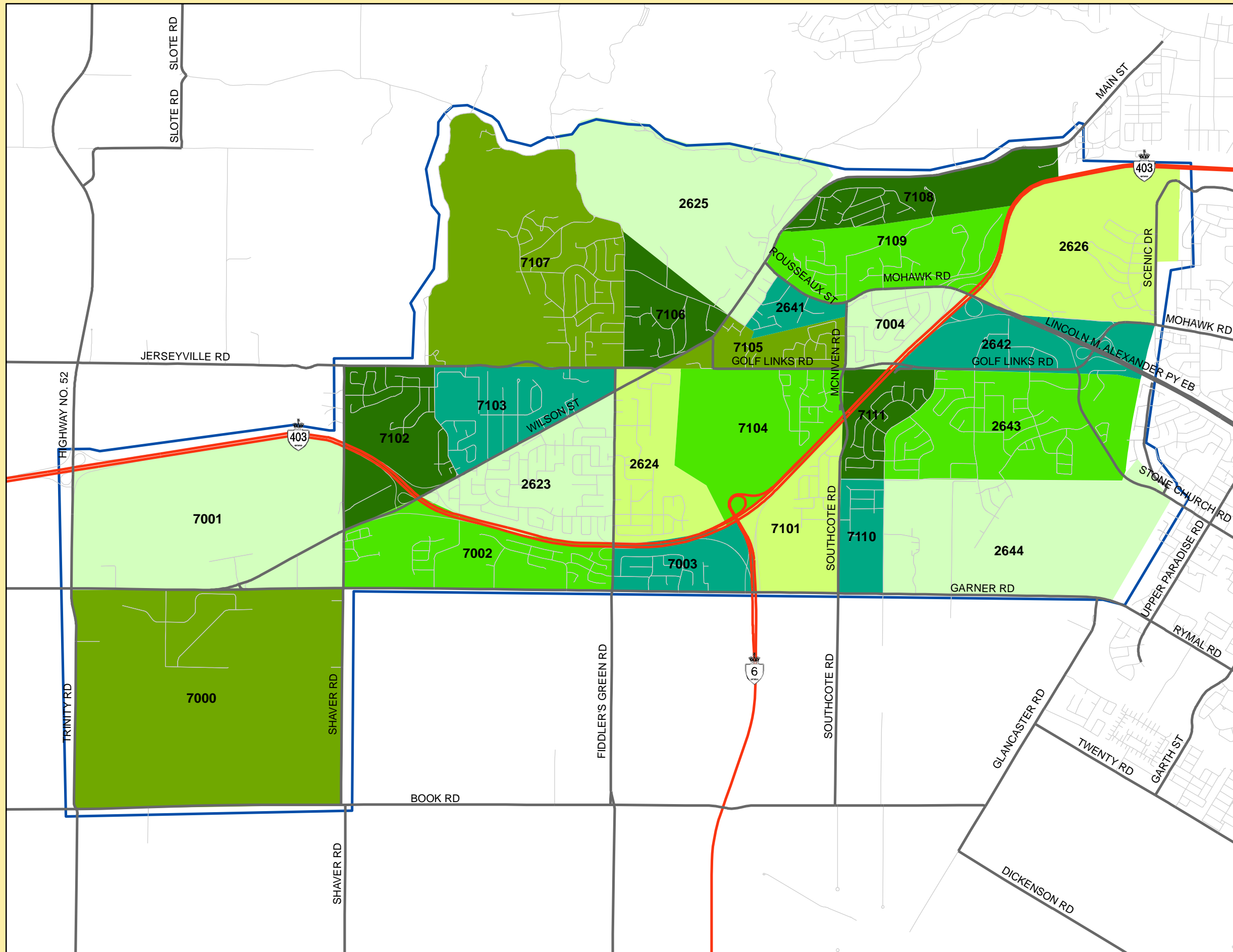
Legend

- Minor Road
- Major Road
- Highway
- External Zones
- Study Area Zones
- Ancaster Study Area








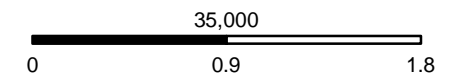
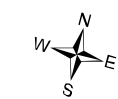
Created By: SFG
 Checked By: JK
 Date Created: 072210
 Date Modified: 022511
 File Path: I:\GIS\088971 - Ancaster\
 Mapping\Transporation Zones.mxd

**Ancaster
Transportation Master Plan**
**Figure 4
Modified Transportation Zones**



Legend

-  Minor Road
-  Major Road
-  Highway
-  Transportation Zones
-  Ancaster Study Area



Created By: SFG
Checked By: JK
Date Created: 072210
Date Modified: 022311
File Path: I:\GIS\088971 - Ancaster\
Mapping\Transportation Zones.mxd

2.3.1 HTMP and GRIDS Population Comparison

The existing population and employment data, based on the Hamilton Transportation Master Plan (HTMP), was split to reflect estimated redistribution of population and employment in the revised zone system, based on the examination of aerial imagery. Population adjustments as a result of the Growth Related Integrated Development Strategy (GRIDS) were considered for existing and future horizon year models. Due to both the uncertainty of the Ancaster population redistribution in GRIDS and the insignificant differences between GRIDS and HTMP figures (within $\pm 5\%$), HTMP figures were used in the model. **Table 3** show the comparison between HTMP and GRIDS population figures and **Table 4** provides a summary of the population and employment revisions.

Table 3 – HTMP and GRIDS Population Comparison

| Horizon | HTMP | GRIDS | Difference | % Change |
|----------------|-------------|--------------|-------------------|-----------------|
| 2006 | 33,170 | 32,226 | 944 | 2.8% |
| 2011 | 36,314 | 35,308 | 1,006 | 2.8% |
| 2016 | 38,532 | 39,509 | -977 | 2.5% |
| 2021 | 39,571 | 41,019 | -1,448 | 3.7% |
| 2026 | 39,143 | 40,893 | -1,750 | 4.5% |
| 2031 | 39,221 | 41,110 | -1,889 | 4.8% |

In order to ensure that the HTMP figures were sufficient for model analysis without significant revisions to the EMME/2 trip tables, a model sensitivity test was performed. In the sensitivity model run, an additional population of 2,000 was added to the high-growth area encompassed by Golf Links Road to the north, Garner Road to the south, Stone Church Road and the hydro easement to the east, and Kitty Murray Lane to the west. This area coincides with the EMME/2 Zones 2643 and 2644.

As a result of the model run, an additional 299 trips originating from and an additional 23 trips destined to the area of interest was observed. As expected, the vehicle trip growth was mostly localized around zones 2643 and 2644. The roadway experiencing the greatest impact was Garner Road westbound, between Springbrook Avenue and Highway 6, with an additional 124 trips (representing 8.4% growth) on the peak link. Critical network links (v/c greater than 0.85) in the Ancaster area experienced insignificant auto volume growth not exceeding 2%.

Based on these findings, we conclude that the GRIDS sensitivity test did not affect the EMME/2 network in the Ancaster area significantly. The existing HTMP trip tables will be used in the EMME/2 model for future year analysis in 2016, 2021, and 2031.

2.3.2 Post-GRIDS Population Adjustments

Following GRIDS, there have been additional developments approved within the Ancaster area (referred to as Post-GRIDS). Unlike GRIDS, which aggregated population changes to Ancaster as a whole, Post-GRIDS developments were based on individual parcels of land. This made it possible to identify developments in specific EMME/2 zones within Ancaster and adjust population figures accordingly.

The City of Hamilton provided persons per unit (PPU) values for Ancaster which allowed for the calculation of population changes. **Table 4** denotes the conversion factors used to translate the number of units into population and **Table 5** displays the Post-GRIDS population changes applied to Ancaster. **Table 6** represents the overall Ancaster area population and employment modifications, including Post-GRIDS adjustments.

2.3.3 Airport Employment Growth District

Another area of interest to the Ancaster model is Hamilton's Airport Employment Growth District (AEGD). It is known that the AEGD will experience significant employment growth by the year 2031, which will impact travel demand in the Ancaster area. The EMME/2 zones in the 2031 horizon contain employment figures of **approximately 29,000 jobs in the AEGD area**. In order to be consistent with the AEGD TMP, the existing 6 zones in the AEGD have been split into 13 for the 2016, 2021, and 2031 horizon years. The employment and population of these 13 zones has been modified to reflect growth in the AEGD over that time in order to examine the impacts on the Ancaster area.

Table 4 – Ancaster Persons per Unit (PPU) Factors

| Year | Single Family | Semi-Detached | Row | Apartment |
|------|---------------|---------------|-------|-----------|
| 2001 | 3.170 | 2.733 | 2.113 | 1.590 |
| 2006 | 3.083 | 2.658 | 2.076 | 1.553 |
| 2011 | 2.996 | 2.593 | 2.031 | 1.517 |
| 2016 | 2.919 | 2.537 | 1.994 | 1.480 |
| 2021 | 2.887 | 2.509 | 1.972 | 1.461 |
| 2026 | 2.876 | 2.499 | 1.972 | 1.461 |
| 2031 | 2.865 | 2.490 | 1.972 | 1.461 |

Table 5 – Post-GRIDS Ancaster Population Adjustments

| Emme Zones | 2016 Population Change | 2021 Population Change | 2031 Population Change |
|------------|------------------------|------------------------|------------------------|
| 2624 | 26 | 26 | 26 |
| 2625 | -118 | -117 | -116 |
| 2643 | 178 | 176 | 176 |
| 2644 | 473 | 468 | 466 |
| 7002 | 186 | 183 | 183 |
| 7003 | 61 | 61 | 60 |
| 7101 | 434 | 428 | 429 |
| 7102 | -38 | -38 | -37 |
| 7109 | 29 | 29 | 29 |
| 7110 | 1,417 | 1,402 | 1,392 |
| Total | 2,649 | 2,618 | 2,609 |

Table 6 – Ancaster Population and Employment Modifications

| Emme Zones | | Population | | | | | Employment | | | | | % Adjustment | |
|------------|------|------------|--------|--------|--------|--------|------------|-------|-------|-------|-------|--------------|------|
| Old | New | 2001 | 2006 | 2016 | 2021 | 2031 | 2001 | 2006 | 2016 | 2021 | 2031 | Pop | Emp |
| 2622 | 2622 | 1,149 | 1,170 | 1,112 | 1,096 | 1,075 | 74 | 79 | 90 | 94 | 105 | 100% | 10% |
| | 7000 | 0 | 0 | 0 | 0 | 0 | 669 | 715 | 807 | 850 | 948 | 0% | 90% |
| 2623 | 2623 | 2,504 | 2,713 | 2,924 | 2,930 | 2,895 | 366 | 400 | 441 | 462 | 495 | 30% | 30% |
| | 7002 | 2,504 | 2,713 | 3,109 | 3,113 | 3,079 | 183 | 200 | 220 | 231 | 248 | 30% | 15% |
| | 7102 | 1,669 | 1,809 | 1,911 | 1,916 | 1,893 | 61 | 67 | 73 | 77 | 83 | 20% | 5% |
| | 7103 | 1,669 | 1,809 | 1,949 | 1,953 | 1,930 | 611 | 667 | 735 | 770 | 825 | 20% | 50% |
| 2624 | 2624 | 1,814 | 1,806 | 2,416 | 2,573 | 2,532 | 396 | 423 | 498 | 564 | 602 | 45% | 65% |
| | 7003 | 605 | 602 | 858 | 910 | 896 | 0 | 0 | 0 | 0 | 0 | 15% | 0% |
| | 7101 | 605 | 602 | 1,230 | 1,277 | 1,265 | 30 | 33 | 38 | 43 | 46 | 15% | 5% |
| | 7104 | 1,008 | 1,004 | 1,328 | 1,415 | 1,393 | 183 | 195 | 230 | 260 | 278 | 25% | 30% |
| 2625 | 2625 | 791 | 818 | 693 | 779 | 805 | 195 | 200 | 224 | 235 | 265 | 15% | 25% |
| | 7107 | 2,372 | 2,453 | 2,434 | 2,688 | 2,764 | 507 | 519 | 582 | 610 | 688 | 45% | 65% |
| | 7108 | 791 | 818 | 811 | 896 | 921 | 0 | 0 | 0 | 0 | 0 | 15% | 0% |
| | 7109 | 1,318 | 1,363 | 1,381 | 1,522 | 1,564 | 78 | 80 | 90 | 94 | 106 | 25% | 10% |
| 2626 | 2626 | 1,309 | 1,289 | 1,293 | 1,274 | 1,250 | 196 | 193 | 197 | 195 | 208 | 100% | 100% |
| 2640 | 2640 | 1,018 | 1,038 | 986 | 972 | 954 | 27 | 28 | 30 | 31 | 34 | 100% | 10% |
| | 7001 | 0 | 0 | 0 | 0 | 0 | 242 | 250 | 271 | 277 | 305 | 0% | 90% |
| 2641 | 2641 | 521 | 509 | 510 | 533 | 526 | 161 | 164 | 173 | 175 | 186 | 25% | 45% |
| | 7105 | 626 | 611 | 611 | 639 | 631 | 0 | 0 | 0 | 0 | 0 | 30% | 0% |
| | 7106 | 938 | 916 | 917 | 959 | 946 | 196 | 201 | 211 | 214 | 228 | 45% | 55% |
| 2642 | 2642 | 0 | 0 | 0 | 0 | 0 | 196 | 211 | 223 | 226 | 238 | 0% | 100% |
| | 7004 | 1,155 | 1,314 | 1,251 | 1,233 | 1,211 | 0 | 0 | 0 | 0 | 0 | 100% | 0% |
| 2643 | 2643 | 2,857 | 4,795 | 4,828 | 4,923 | 4,842 | 772 | 887 | 989 | 1,042 | 1,111 | 70% | 100% |
| | 7111 | 1,224 | 2,055 | 1,993 | 2,034 | 2,000 | 0 | 0 | 0 | 0 | 0 | 30% | 0% |
| 2644 | 2644 | 316 | 580 | 3,559 | 3,511 | 3,456 | 311 | 574 | 830 | 1,052 | 1,099 | 65% | 100% |
| | 7110 | 210 | 386 | 1,661 | 1,639 | 1,610 | 0 | 0 | 0 | 0 | 0 | 35% | 0% |
| Totals | | 28,971 | 33,170 | 39,763 | 40,788 | 40,437 | 5,454 | 6,085 | 6,952 | 7,500 | 8,096 | | |

2.4 Trip Generation and Distribution

The 2006 base matrix was created using a three-step process with the 2011 TMP peak period auto driver matrix as original input.

The trip end totals were adjusted to reflect the difference in population and employment numbers between 2006 and 2011. The origin adjustment factor was weighted using 95% of population and 5% of employment; the destination factor was weighted using 90% employment and 10% population. Origins and destinations external to the City of Hamilton were reduced by 2.4% and 4.5% respectively based on the total difference in population and employment for the City as a whole.

Using the standard Fratar distribution procedure, the 2011 matrix was re-balanced to the 2006 trip end totals, including the new Ancaster sub-zones added in **Table 6**.

For the future horizon year of 2016, a mean value matrix of the 2011 and 2021 trip matrices was calculated and factored to include the new sub-zones using the Fratar distribution procedure. The future horizon years of 2021 and 2031 were also factored to include the new sub-zones.

A peak hour factor of 0.5 was applied to the trip matrix prior to trip assignment in order to convert from the AM peak period (three hours) to the AM peak hour. The 0.5 factor is unusually high, but was selected to give a good average fit between the assigned traffic volumes and observed traffic counts within the study area.

Table 7 provides a summary of the number of trips attracted and produced by the Ancaster model during the AM Peak in the study area.

2.5 Trip Assignment

For the Ancaster model, the auto trip assignment was performed using EMME/2's standard equilibrium assignment and Tangent volume delay functions. Several iterations of the trip assignment algorithm were completed and analyzed for consistency with the Ancaster roadway network goals and assumptions.

2.6 Base Year Validation

Model validation requires comparing traffic simulated by the model to counted traffic in the field along contrived barriers called screenlines representing both imaginary and actual physical barriers. In order to facilitate this comparison, a comprehensive set of data (ATR) was collected as part of the data collection program for the study. The existing peak hour count volumes are illustrated on **Figure 5**.

Table 7 – Trip Generation by Zone

| Zone | Origins | | | | Destinations | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| | 2006 | 2016 | 2021 | 2031 | 2006 | 2016 | 2021 | 2031 |
| 422-424 | 728 | 751 | 755 | 762 | 1,599 | 1,664 | 1,681 | 1,745 |
| 503-504 | 1,717 | 1,767 | 1,793 | 1,835 | 1,303 | 1,240 | 1,242 | 1,342 |
| 2622 | 185 | 160 | 161 | 169 | 55 | 49 | 51 | 55 |
| 2623 | 566 | 432 | 456 | 480 | 255 | 157 | 184 | 198 |
| 2624 | 297 | 317 | 353 | 370 | 205 | 204 | 229 | 243 |
| 2625 | 134 | 108 | 116 | 126 | 137 | 113 | 119 | 129 |
| 2626 | 182 | 179 | 179 | 182 | 92 | 87 | 88 | 92 |
| 2640 | 173 | 135 | 135 | 142 | 25 | 18 | 19 | 20 |
| 2641 | 89 | 82 | 82 | 84 | 74 | 65 | 65 | 67 |
| 2642 | 11 | 10 | 9 | 10 | 135 | 124 | 123 | 127 |
| 2643 | 608 | 598 | 610 | 689 | 339 | 329 | 336 | 378 |
| 2644 | 115 | 540 | 614 | 615 | 198 | 333 | 370 | 389 |
| 7000 | 9 | 7 | 7 | 8 | 242 | 212 | 219 | 236 |
| 7001 | 7 | 6 | 6 | 6 | 122 | 86 | 86 | 92 |
| 7002 | 562 | 453 | 479 | 502 | 141 | 102 | 103 | 110 |
| 7003 | 188 | 107 | 118 | 124 | 25 | 5 | 6 | 6 |
| 7004 | 207 | 185 | 183 | 186 | 15 | 13 | 13 | 14 |
| 7101 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7102 | 375 | 278 | 293 | 308 | 57 | 41 | 41 | 43 |
| 7103 | 396 | 304 | 322 | 340 | 409 | 294 | 298 | 314 |
| 7104 | 165 | 174 | 194 | 203 | 97 | 97 | 108 | 115 |
| 7105 | 98 | 90 | 90 | 93 | 5 | 5 | 5 | 5 |
| 7106 | 157 | 143 | 144 | 148 | 92 | 81 | 83 | 84 |
| 7107 | 382 | 359 | 378 | 409 | 344 | 287 | 303 | 328 |
| 7108 | 125 | 117 | 123 | 132 | 9 | 7 | 8 | 8 |
| 7109 | 211 | 201 | 211 | 228 | 65 | 54 | 57 | 62 |
| 7110 | 71 | 239 | 273 | 272 | 9 | 12 | 13 | 14 |
| 7111 | 284 | 264 | 267 | 296 | 12 | 12 | 12 | 13 |
| Total | 8,042 | 8,006 | 8,351 | 8,719 | 6,061 | 5,691 | 5,862 | 6,229 |



Hamilton

Ancaster Transportation Master Plan

Figure 5 Average Annual Daily Traffic Counts (Weekday Peak)

Legend

- Existing Road Network
- Highway
- Ancaster Study Area
- 100 (100) AM (PM) Weekday Peak Hour Volumes (2007)

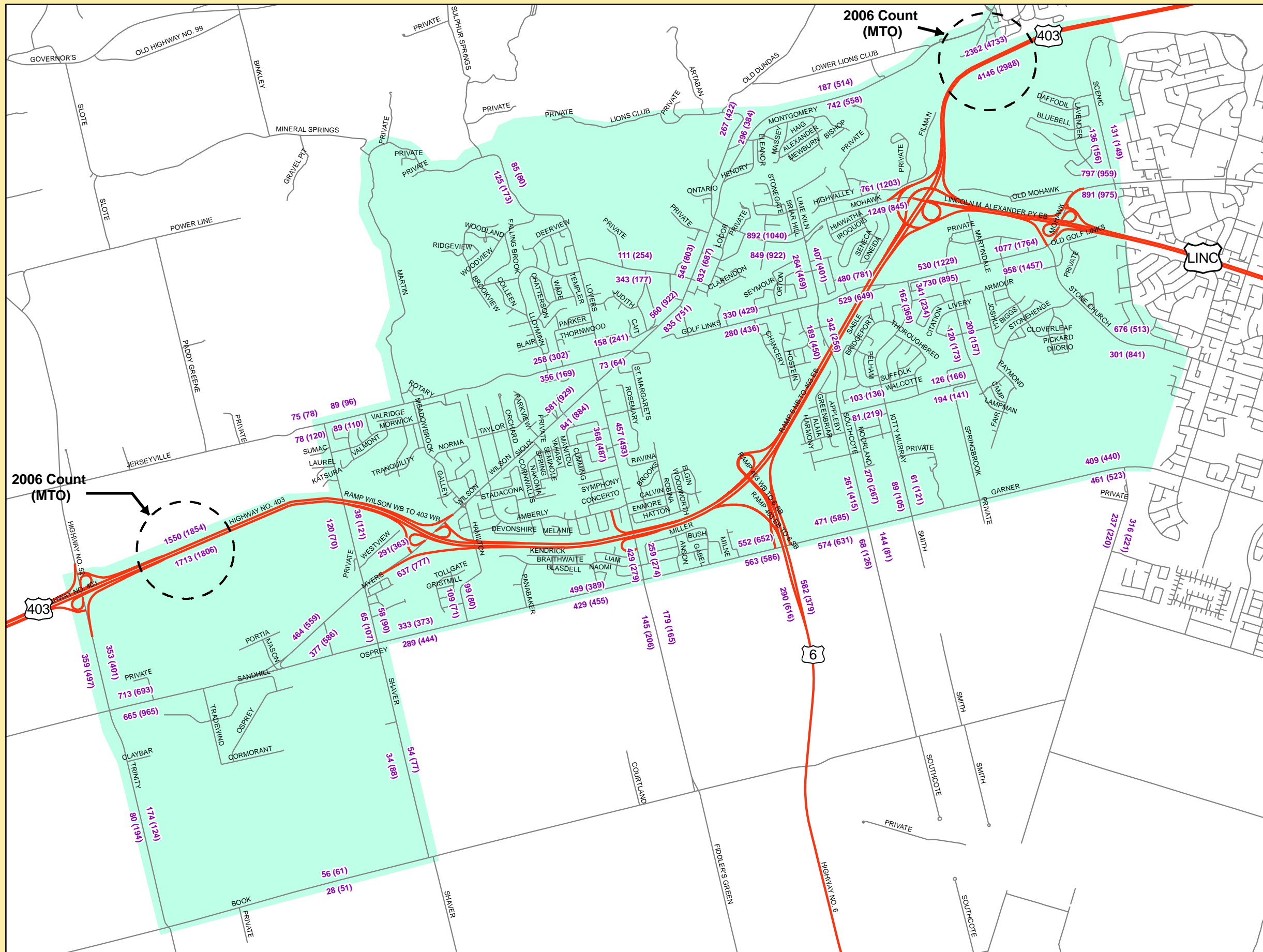


Exhibit 7

Kilometers



An initial test assignment showed an over representation of traffic trips to and from the west on Highway 403 at the boundary with Brant County. **Table 8** provides a comparison of the external trips generated by the Hamilton model with data from the 2006 TTS. Previous TTSs have not included data for the City of Brantford, Brant County, and the Region of Waterloo.

Table 8 – External Trip Comparison (No Adjustment)

| Zone # | Zone Description | Inbound to Hamilton | | Outbound from Hamilton | |
|-----------|--------------------|---------------------|------------------------|------------------------|------------------------|
| | | Hamilton Model | 2006 TTS (07:30-08:29) | Hamilton model | 2006 TTS (07:30-08:29) |
| 504 | City of Brantford | 1237 | 1025 | 356 | 1158 |
| 503 | County of Brant | 481 | 421 | 939 | 216 |
| Sub-Total | | 1718 | 1446 | 1295 | 1374 |
| 422-424 | Region of Waterloo | 407 | 673 | 847 | 689 |
| Total | | 2125 | 2119 | 2142 | 2063 |

The total number of simulated external trips is remarkably close to the observed TTS value although the distribution is somewhat different. To correct for those differences a factor of three has been applied to all outbound trip movements from the City of Hamilton to Zone 504. Trips to Zone 503 have been reduced by 75%.

The TMP network included a centroid connector that joined the zone centroid representing Brant County (503) directly to Highway 403. That connector has been removed. These changes resulted in a significant improvement in simulated traffic volumes on Highway 403 relative to the traffic counts.

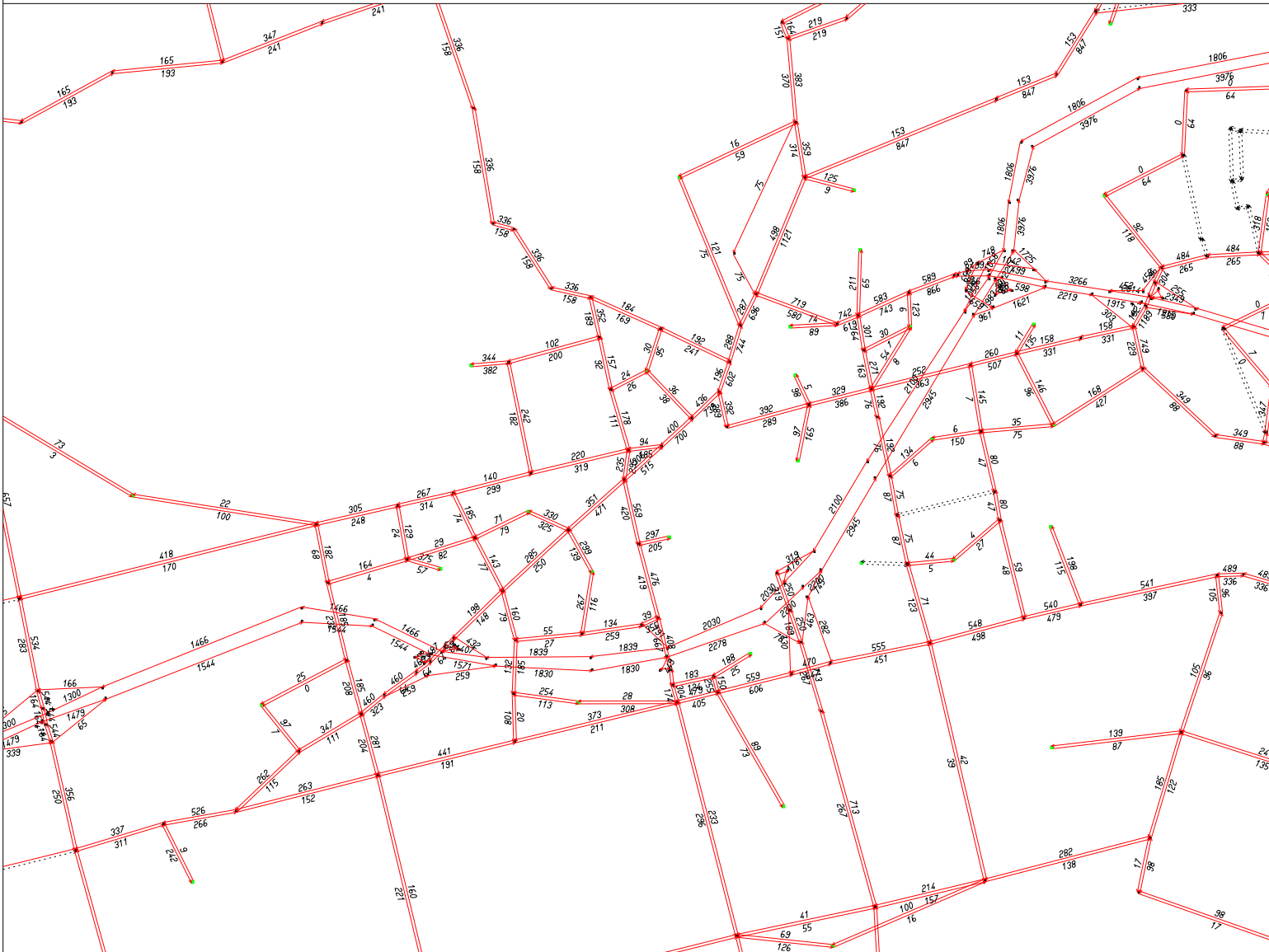
The 2006 simulated volumes are illustrated in **Figures 6**.

2.7 Screenline Volume Comparison

A comparison of counted and simulated volumes and capacity across a number of screenlines was completed for the 2006 existing scenario. **Table 9** provides an overview of the screenline validation of AM Peak Hour simulated trips and 2006 count data.

AUTO VOLUMES

emme/2



LINKS:
all

Figure 6

WINDOW:
577261/ 781716
587402/ 789321

EMME/2 PROJECT: Hamilton Airport
SCENARIO 5000: 2006 Ancaster TMP (2010-08-13)

10-08-13 17:13
MODULE: 6.12
DMG.UTYU...jdx

Table 9 – Screenline Validation

| Number | Screenline | Road Name | Direction | AM Peak 2006 Vol Counted | AM Peak 2006 Vol Simulated | Screenline Ratio |
|-------------------|---------------------------|----------------------|-----------|--------------------------------|----------------------------------|---------------------|
| 1 | South of Garner Road | Trinity Road | NB | 174 | 343 | |
| | | | SB | 80 | 49 | |
| | | Shaver Road | NB | 54 | 160 | |
| | | | SB | 34 | 221 | |
| | | Fiddler's Green Road | NB | 170 | 233 | |
| | | | SB | 145 | 296 | |
| | | Highway 6 | NB | 582 | 713 | |
| | | | SB | 290 | 267 | |
| | | Southcote Road | NB | 144 | 42 | |
| | | | SB | 68 | 39 | |
| Glancaster Road | NB | 316 | 96 | | | |
| | SB | 237 | 105 | | | |
| Totals | NB | 1,440 | 1,587 | 1.10 | | |
| | SB | 854 | 977 | 1.14 | | |
| 2 | North of Garner Road | Trinity Road | NB | 353 | 356 | |
| | | | SB | 359 | 250 | |
| | | Wilson Street | NB | 377 | 115 | |
| | | | SB | 464 | 262 | |
| | | Shaver Road | NB | 58 | 281 | |
| | | | SB | 65 | 204 | |
| | | Hamilton Drive | NB | 99 | 20 | |
| | | | SB | 199 | 108 | |
| | | Fiddler's Green Road | NB | 259 | 304 | |
| | | | SB | 429 | 174 | |
| | | Highway 6 | NB | 582 | 713 | |
| | | | SB | 290 | 267 | |
| | | Highway 403 Ramp | NB | 133 | 282 | |
| | | | SB | 69 | 130 | |
| Southcote Road | NB | 270 | 71 | | | |
| | SB | 261 | 123 | | | |
| Kitty Murray Lane | NB | 61 | 59 | | | |
| | SB | 89 | 48 | | | |
| Totals | NB | 2,192 | 2,201 | 1.00 | | |
| | SB | 2,225 | 1,566 | 0.70 | | |
| 3 | South of Jerseyville Road | Shaver Road | NB | 38 | 182 | |
| | | | SB | 120 | 68 | |
| | | Meadowbrook Drive | NB | - | 185 | |
| | | | SB | - | 74 | |
| | | Fiddler's Green Road | NB | 457 | 295 | |
| | | | SB | 368 | 235 | |
| | | Wilson Street | NB | 841 | 515 | |
| | | | SB | 581 | 306 | |
| | | Southcote Road | NB | 342 | 192 | |
| | | | SB | 189 | 76 | |
| Kitty Murray Lane | NB | 341 | 145 | | | |
| | SB | 162 | 7 | | | |
| Stone Church Road | NB | 676 | 749 | | | |
| | SB | 301 | 229 | | | |
| Totals | NB | 2,695 | 2,263 | 0.84 | | |
| | SB | 1,721 | 995 | 0.58 | | |
| 4 | South of Lions Club Road | Sulphur Springs Road | NB | 85 | 336 | |
| | | | SB | 125 | 158 | |
| | | Old Dundas Road | NB | 296 | 383 | |
| | | | SB | 267 | 370 | |
| | | Wilson Street | NB | 742 | 847 | |
| | | | SB | 187 | 153 | |
| | | Highway 403 | NB | 4,146 | 3,976 | |
| | | | SB | 2,362 | 1,806 | |
| Totals | NB | 5,269 | 5,542 | 1.05 | | |
| | SB | 2,941 | 2,487 | 0.85 | | |
| 5 | East of Shaver Road | Garner Road | EB | 289 | 191 | |
| | | | WB | 333 | 441 | |
| | | Wilson Street | EB | 637 | 323 | |
| | | | WB | 291 | 460 | |
| | | Highway 403 | EB | 1,713 | 1,544 | |
| | | | WB | 1,550 | 1,466 | |
| | | Jerseyville Road | EB | 89 | 248 | |
| | | | WB | 89 | 305 | |
| Totals | EB | 2,728 | 2,306 | 0.85 | | |
| | WB | 2,263 | 2,672 | 1.18 | | |
| 6 | West of Fiddler's Green | Garner Road | EB | 429 | 211 | |
| | | | WB | 499 | 373 | |

| Number | Screenline | Road Name | Direction | AM Peak 2006 Vol Counted | AM Peak 2006 Vol Simulated | Screenline Ratio |
|-------------------------------|------------------------------|-------------------------|-----------|--------------------------------|----------------------------------|---------------------|
| | Road | Highway 403 | EB | 2,143 | 1,830 | |
| | | | WB | 1,939 | 1,839 | |
| | | Amberly Blvd | EB | 514 | 355 | |
| | | | WB | 121 | 39 | |
| | | Wilson Street | EB | 841 | 471 | |
| | | | WB | 581 | 351 | |
| | | Jerseyville Road | EB | 356 | 319 | |
| | | | WB | 258 | 220 | |
| | | Totals | EB | 4,283 | 3,186 | 0.74 |
| | | | WB | 3,398 | 2,822 | 0.83 |
| 7 | West of Highway 6 | Garner Road | EB | 563 | 606 | |
| | | | WB | 552 | 559 | |
| | | Highway 403 | EB | 2,247 | 2,278 | |
| | | | WB | 2,033 | 2,030 | |
| | | Wilson Street | EB | 835 | 738 | |
| | | | WB | 560 | 436 | |
| | | Sulphur Springs Road | EB | 343 | 241 | |
| | | | WB | 111 | 192 | |
| | | Totals | EB | 3,988 | 3,863 | 0.97 |
| | | | WB | 3,256 | 3,217 | 0.99 |
| 8 | West of Southcote Road | Garner Road | EB | 574 | 451 | |
| | | | WB | 471 | 555 | |
| | | Highway 403 | EB | 2,629 | 2,945 | |
| | | | WB | 2,379 | 2,100 | |
| | | Golf Links Road | EB | 280 | 386 | |
| | | | WB | 330 | 329 | |
| | | Mohawk Road | EB | 849 | 619 | |
| | | | WB | 892 | 742 | |
| | | Totals | EB | 4,332 | 4,401 | 1.02 |
| | | | WB | 4,072 | 3,726 | 0.92 |
| 9 | West of Stone Church Road | Garner Road | EB | 461 | 397 | |
| | | | WB | 409 | 541 | |
| | | Mohawk Road | EB | 958 | 331 | |
| | | | WB | 1,077 | 158 | |
| | | Totals | EB | 1,419 | 728 | 0.51 |
| | | | WB | 1,486 | 699 | 0.47 |
| NB/EB (Peak Direction) Totals | | | | 28,346 | 26,077 | 0.92 |
| SB/WB Totals | | | | 22,216 | 19,161 | 0.86 |
| GRAND TOTAL | | | | 50,562 | 45,238 | 0.89 |

Based on a review of the 2006 AM Peak Hour counted and simulated volumes from the modified EMME/2 model for the Ancaster study area, the model is operating within acceptable parameters having overall simulated/counted ratios within approximately $\pm 15\%$ in the peak direction (northbound and eastbound in the AM Peak Hour). The ratio of $\pm 15\%$ was chosen based on the level of detail available in the EMME/2 model. This value provides a good fit for a high-level analysis of Ancaster and the surrounding area.

Overall the model is operating acceptably, however there are several screenlines, particularly in the peak direction, which appear to under-simulate volumes compared to counted values. This occurs at the screenlines west of Fiddler's Green Road and west of Stone Church Road. During the model analysis, the screenline variances were recognized in the evaluation of each scenario.

It should be noted that the City of Hamilton is currently undertaking an update of the Hamilton EMME/2 model to reflect the 2006 Transportation Tomorrow Survey and future modifications may arise as a result of that process.

3.0 SCREENLINE CAPACITY ANALYSIS

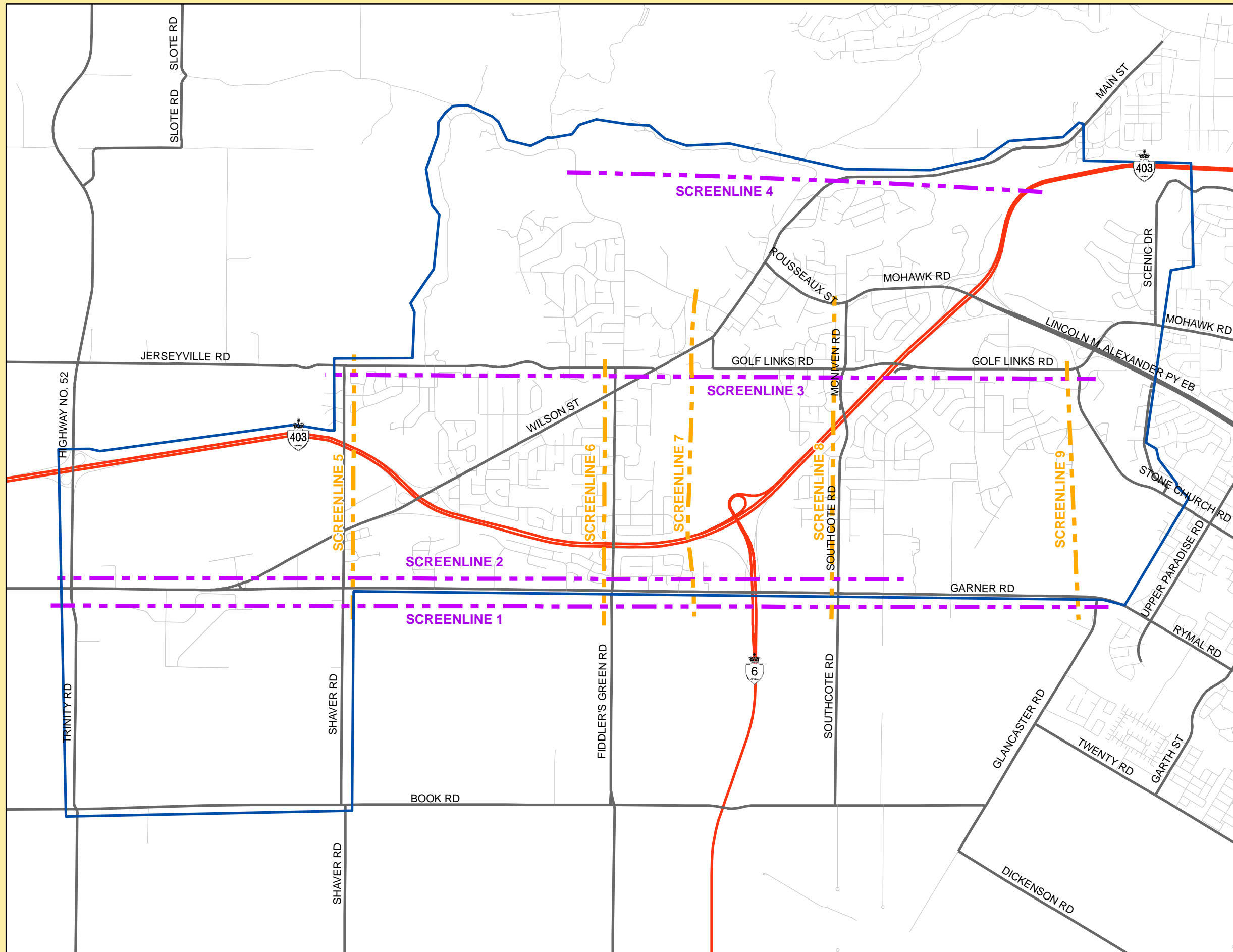
A comparison of counted and simulated volumes versus roadway capacity across a number of screenlines was completed for the 2006 existing scenario to help understand existing network deficiencies across screenlines. **Figure 7** illustrates the screenlines that were used in this analysis.

Volume to capacity (v/c) ratios in excess of 0.85 were used as an indicator of potential problems for both screenlines and individual links. **Table 10** provides an overview of the link and screenline volume to capacity ratios using AM and PM counted volumes and 2006 simulated trips.



Under 2006 existing conditions, there are a number of screenlines and individual links that are congested. Screenline 4 (South of Lions Clubs Road), along the Niagara Escarpment, exhibits an overall screenline capacity constraint as well as individual link constraints on Highway 403 and Old Dundas Road. Capacity constraints are also observed along Screenline 8 (West of Southcote Road) and specifically along Golf Links Road and Mohawk Road.

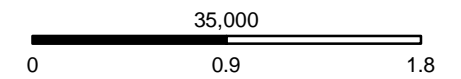
Ancaster Transportation Master Plan

Figure 7 Travel Demand Screenlines



Legend

-  Minor Road
-  Major Road
-  Highway
-  Ancaster Study Area
-  Screenlines



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 Checked By: JK
 Date Created: 072210
 Date Modified: 022311
 File Path: I:\GIS\088971 - Ancaster\
 Mapping\Transportation Zones.mxd

Table 10 – 2006 Link and Screenline Volume to Capacity Ratios

| Number | Screenline | Road Name | Direction | Capacity (1-way) | AM Peak 2006 Vol Counted | AM Peak 2006 Vol Simulated | PM Peak 2006 Vol Counted | AM Peak 2006 V/C Counted | AM Peak 2006 V/C Simulated | PM Peak 2006 V/C Counted |
|-------------------|---------------------------|----------------------|-----------|------------------|--------------------------|----------------------------|--------------------------|--------------------------|----------------------------|--------------------------|
| 1 | South of Garner Road | Trinity Road | NB | 1,000 | 174 | 343 | 124 | 0.17 | 0.34 | 0.12 |
| | | | SB | 1,000 | 80 | 49 | 194 | 0.08 | 0.05 | 0.19 |
| | | Shaver Road | NB | 500 | 54 | 160 | 77 | 0.11 | 0.32 | 0.15 |
| | | | SB | 500 | 34 | 221 | 88 | 0.07 | 0.44 | 0.18 |
| | | Fiddler's Green Road | NB | 1,000 | 170 | 233 | 165 | 0.17 | 0.23 | 0.17 |
| | | | SB | 1,000 | 145 | 296 | 206 | 0.15 | 0.30 | 0.21 |
| | | Highway 6 | NB | 1,800 | 582 | 713 | 379 | 0.32 | 0.40 | 0.21 |
| | | | SB | 1,800 | 290 | 267 | 616 | 0.16 | 0.15 | 0.34 |
| | | Southcote Road | NB | 500 | 144 | 42 | 81 | 0.29 | 0.08 | 0.16 |
| | | | SB | 500 | 68 | 39 | 126 | 0.14 | 0.08 | 0.25 |
| Glancaster Road | NB | 500 | 316 | 96 | 221 | 0.63 | 0.19 | 0.44 | | |
| | SB | 500 | 237 | 105 | 220 | 0.47 | 0.21 | 0.44 | | |
| Totals | NB | 5,300 | 1,440 | 1,587 | 1,047 | 0.27 | 0.30 | 0.20 | | |
| | SB | 5,300 | 854 | 977 | 1,450 | 0.16 | 0.18 | 0.27 | | |
| 2 | North of Garner Road | Trinity Road | NB | 1,000 | 353 | 356 | 401 | 0.35 | 0.36 | 0.40 |
| | | | SB | 1,000 | 359 | 250 | 497 | 0.36 | 0.25 | 0.50 |
| | | Wilson Street | NB | 2,000 | 377 | 115 | 586 | 0.19 | 0.06 | 0.29 |
| | | | SB | 2,000 | 464 | 262 | 559 | 0.23 | 0.13 | 0.28 |
| | | Shaver Road | NB | 500 | 58 | 281 | 90 | 0.12 | 0.56 | 0.18 |
| | | | SB | 500 | 65 | 204 | 107 | 0.13 | 0.41 | 0.21 |
| | | Hamilton Drive | NB | 400 | 99 | 20 | 80 | 0.25 | 0.05 | 0.20 |
| | | | SB | 400 | 199 | 108 | 107 | 0.50 | 0.27 | 0.27 |
| | | Fiddler's Green Road | NB | 700 | 259 | 304 | 274 | 0.37 | 0.43 | 0.39 |
| | | | SB | 700 | 429 | 174 | 279 | 0.61 | 0.25 | 0.40 |
| | | Highway 6 | NB | 1,800 | 582 | 713 | 379 | 0.32 | 0.40 | 0.21 |
| | | | SB | 1,800 | 290 | 267 | 616 | 0.16 | 0.15 | 0.34 |
| | | Highway 403 Ramp | NB | 1,400 | 133 | 282 | 77 | 0.10 | 0.20 | 0.06 |
| | | | SB | 1,400 | 69 | 130 | 145 | 0.05 | 0.09 | 0.10 |
| Southcote Road | NB | 700 | 270 | 71 | 267 | 0.39 | 0.10 | 0.38 | | |
| | SB | 700 | 261 | 123 | 415 | 0.37 | 0.18 | 0.59 | | |
| Kitty Murray Lane | NB | 400 | 61 | 59 | 121 | 0.15 | 0.15 | 0.30 | | |
| | SB | 400 | 89 | 48 | 105 | 0.22 | 0.12 | 0.26 | | |
| Totals | NB | 8,900 | 2,192 | 2,201 | 2,275 | 0.25 | 0.25 | 0.26 | | |
| | SB | 8,900 | 2,225 | 1,566 | 2,830 | 0.25 | 0.18 | 0.32 | | |
| 3 | South of Jerseyville Road | Shaver Road | NB | 500 | 38 | 182 | 121 | 0.08 | 0.36 | 0.24 |
| | | | SB | 500 | 120 | 68 | 70 | 0.24 | 0.14 | 0.14 |
| | | Meadowbrook Drive | NB | 400 | - | 185 | - | - | 0.46 | - |
| | | | SB | 400 | - | 74 | - | - | 0.19 | - |
| | | Fiddler's Green Road | NB | 700 | 457 | 295 | 493 | 0.65 | 0.42 | 0.70 |
| | | | SB | 700 | 368 | 235 | 487 | 0.53 | 0.34 | 0.70 |
| | | Wilson Street | NB | 900 | 841 | 515 | 884 | 0.93 | 0.57 | 0.98 |
| | | | SB | 900 | 581 | 306 | 929 | 0.65 | 0.34 | 1.03 |
| | | Southcote Road | NB | 700 | 342 | 192 | 256 | 0.49 | 0.27 | 0.37 |
| | | | SB | 700 | 189 | 76 | 450 | 0.27 | 0.11 | 0.64 |
| Kitty Murray Lane | NB | 400 | 341 | 145 | 234 | 0.85 | 0.36 | 0.59 | | |
| | SB | 400 | 162 | 7 | 368 | 0.41 | 0.02 | 0.92 | | |
| Stone Church Road | NB | 1,000 | 676 | 749 | 513 | 0.68 | 0.75 | 0.51 | | |
| | SB | 1,000 | 301 | 229 | 841 | 0.30 | 0.23 | 0.84 | | |
| Totals | NB | 4,600 | 2,695 | 2,263 | 2,501 | 0.59 | 0.49 | 0.54 | | |
| | SB | 4,600 | 1,721 | 995 | 3,145 | 0.37 | 0.22 | 0.68 | | |
| 4 | South of Lions Club Road | Sulphur Springs Road | NB | 400 | 85 | 336 | 80 | 0.21 | 0.84 | 0.20 |
| | | | SB | 400 | 125 | 158 | 173 | 0.31 | 0.40 | 0.43 |
| | | Old Dundas Road | NB | 400 | 296 | 383 | 384 | 0.74 | 0.96 | 0.96 |
| | | | SB | 400 | 267 | 370 | 422 | 0.67 | 0.93 | 1.06 |
| | | Wilson Street | NB | 1,000 | 742 | 847 | 558 | 0.74 | 0.85 | 0.56 |
| | | | SB | 1,000 | 187 | 153 | 514 | 0.19 | 0.15 | 0.51 |
| Highway 403 | NB | 3,600 | 4,146 | 3,976 | 2,988 | 1.15 | 1.10 | 0.83 | | |
| | SB | 3,600 | 2,362 | 1,806 | 4,733 | 0.66 | 0.50 | 1.31 | | |
| Totals | NB | 5,400 | 5,269 | 5,542 | 4,010 | 0.98 | 1.03 | 0.74 | | |
| | SB | 5,400 | 2,941 | 2,487 | 5,842 | 0.54 | 0.46 | 1.08 | | |
| 5 | East of Shaver Road | Garner Road | EB | 900 | 289 | 191 | 444 | 0.32 | 0.21 | 0.49 |
| | | | WB | 900 | 333 | 441 | 373 | 0.37 | 0.49 | 0.41 |
| | | Wilson Street | EB | 2,000 | 637 | 323 | 777 | 0.32 | 0.16 | 0.39 |
| | | | WB | 2,000 | 291 | 460 | 363 | 0.15 | 0.23 | 0.18 |
| | | Highway 403 | EB | 3,600 | 1,713 | 1,544 | 1,806 | 0.48 | 0.43 | 0.50 |
| | | | WB | 3,600 | 1,550 | 1,466 | 1,854 | 0.43 | 0.41 | 0.52 |
| Jerseyville Road | EB | 1,000 | 89 | 248 | 110 | 0.09 | 0.25 | 0.11 | | |
| | WB | 1,000 | 89 | 305 | 96 | 0.09 | 0.31 | 0.10 | | |
| Totals | EB | 7,500 | 2,728 | 2,306 | 3,137 | 0.36 | 0.31 | 0.42 | | |
| | WB | 7,500 | 2,263 | 2,672 | 2,686 | 0.30 | 0.36 | 0.36 | | |
| 6 | West of Fiddler's | Garner Road | EB | 900 | 429 | 211 | 455 | 0.48 | 0.23 | 0.51 |

| | | | | | | | | | | |
|--------|---------------------------|----------------------|-------|-------|-------|-------|-------|------|------|------|
| | | | WB | 900 | 499 | 373 | 389 | 0.55 | 0.41 | 0.43 |
| | | Highway 403 | EB | 3,600 | 2,143 | 1,830 | 2,259 | 0.60 | 0.51 | 0.63 |
| | | | WB | 3,600 | 1,939 | 1,839 | 2,320 | 0.54 | 0.51 | 0.64 |
| | | Amberly Blvd | EB | 400 | 514 | 355 | 512 | 1.29 | 0.89 | 1.28 |
| | | | WB | 400 | 121 | 39 | 136 | 0.30 | 0.10 | 0.34 |
| | | Wilson Street | EB | 900 | 841 | 471 | 884 | 0.93 | 0.52 | 0.98 |
| | | | WB | 900 | 581 | 351 | 929 | 0.65 | 0.39 | 1.03 |
| | | Jerseyville Road | EB | 700 | 356 | 319 | 169 | 0.51 | 0.46 | 0.24 |
| | | | WB | 700 | 258 | 220 | 302 | 0.37 | 0.31 | 0.43 |
| | | Totals | EB | 6,500 | 4,283 | 3,186 | 4,279 | 0.66 | 0.49 | 0.66 |
| | | | WB | 6,500 | 3,398 | 2,822 | 4,076 | 0.52 | 0.43 | 0.63 |
| 7 | West of Highway 6 | Garner Road | EB | 900 | 563 | 606 | 586 | 0.63 | 0.67 | 0.65 |
| | | | WB | 900 | 552 | 559 | 652 | 0.61 | 0.62 | 0.72 |
| | | Highway 403 | EB | 3,600 | 2,247 | 2,278 | 2,369 | 0.62 | 0.63 | 0.66 |
| | | | WB | 3,600 | 2,033 | 2,030 | 2,432 | 0.56 | 0.56 | 0.68 |
| | | Wilson Street | EB | 900 | 835 | 738 | 751 | 0.93 | 0.82 | 0.83 |
| | | | WB | 900 | 560 | 436 | 922 | 0.62 | 0.48 | 1.02 |
| | | Sulphur Springs Road | EB | 500 | 343 | 241 | 177 | 0.69 | 0.48 | 0.35 |
| | | | WB | 500 | 111 | 192 | 254 | 0.22 | 0.38 | 0.51 |
| Totals | EB | 5,900 | 3,988 | 3,863 | 3,883 | 0.68 | 0.65 | 0.66 | | |
| | WB | 5,900 | 3,256 | 3,217 | 4,260 | 0.55 | 0.55 | 0.72 | | |
| 8 | West of Southcote Road | Garner Road | EB | 900 | 574 | 451 | 631 | 0.64 | 0.50 | 0.70 |
| | | | WB | 900 | 471 | 555 | 585 | 0.52 | 0.62 | 0.65 |
| | | Highway 403 | EB | 3,600 | 2,629 | 2,945 | 2,772 | 0.73 | 0.82 | 0.77 |
| | | | WB | 3,600 | 2,379 | 2,100 | 2,845 | 0.66 | 0.58 | 0.79 |
| | | Golf Links Road | EB | 500 | 280 | 386 | 436 | 0.56 | 0.77 | 0.87 |
| | | | WB | 500 | 330 | 329 | 429 | 0.66 | 0.66 | 0.86 |
| | | Mohawk Road | EB | 700 | 849 | 619 | 922 | 1.21 | 0.88 | 1.32 |
| | | | WB | 700 | 892 | 742 | 1,040 | 1.27 | 1.06 | 1.49 |
| Totals | EB | 5,700 | 4,332 | 4,401 | 4,761 | 0.76 | 0.77 | 0.84 | | |
| | WB | 5,700 | 4,072 | 3,726 | 4,899 | 0.71 | 0.65 | 0.86 | | |
| 9 | West of Stone Church Road | Garner Road | EB | 1,000 | 461 | 397 | 523 | 0.46 | 0.40 | 0.52 |
| | | | WB | 1,000 | 409 | 541 | 440 | 0.41 | 0.54 | 0.44 |
| | | Mohawk Road | EB | 1,800 | 958 | 331 | 1,457 | 0.53 | 0.18 | 0.81 |
| | | | WB | 1,800 | 1,077 | 158 | 1,764 | 0.60 | 0.09 | 0.98 |
| | | Totals | EB | 2,800 | 1,419 | 728 | 1,980 | 0.51 | 0.26 | 0.71 |
| | | | WB | 2,800 | 1,486 | 699 | 2,204 | 0.53 | 0.25 | 0.79 |

| | |
|--|------------------------------------|
| | Individual Link Congestion (>0.85) |
| | Screenline Congestion (>0.85) |

4.0 FUTURE HORIZONS AND SCENARIOS

4.1 Overview

Once validation for the Ancaster model was complete for 2006 base year conditions, the “do nothing” scenario (existing base conditions) was run with the projected population and employment data for the future horizon years of 2016, 2021, and 2031.

4.2 “Do Nothing” Scenario

The “do nothing” scenarios in the 2016, 2021, and 2031 horizons took into consideration any projects that were approved or planned from the capital budget, development charge studies, secondary plans, and EA studies undertaken by the City of Hamilton within the 2031 horizon year. These projects included, but are not limited to:

- AEGD TMP study area;
- Trinity Church connection;
- Red Hill Valley Parkway;
- GRIDS (Growth Related Infrastructure Development Strategy); and
- Additional approved Ancaster developments (Post-GRIDS).

The “do nothing” scenarios identified Ancaster network capacity deficiencies with the increase in population and employment by 2031. Under this scenario, more roadway links and screenlines will become congested. **Table 11** provides an overview of the link and screenline volume to capacity ratios for the AM Peak Hour in the 2006 and 2031 existing network.

Additional capacity constraints are anticipated along Screenlines 1 and 2 (North/South of Garner Road) and along Garner Road, corresponding to the development of the Airport Employment Growth District (AEGD). Transportation analysis associated with this development is addressed in the AEGD TMP report.

In order to address these additional network deficiencies, two main areas were examined:

- Opportunities for enhanced connectivity to Highway 403; and
- Consideration of options that would divert/alleviate traffic from the Wilson Street core area.

Table 11 – 2006 and 2031 Link and Screenline Volume to Capacity Ratios

| Number | Screenline | Road Name | Direction | Capacity (1-way) | AM Peak 2006 Vol Counted | AM Peak 2006 Vol Simulated | AM Peak 2031 Vol Simulated | AM Peak 2006 V/C Simulated | AM Peak 2031 V/C Simulated |
|-------------------|---------------------------|----------------------|-----------|------------------|--------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| 1 | South of Garner Road | Trinity Road | NB | 1,000 | 174 | 343 | 458 | 0.34 | 0.46 |
| | | | SB | 1,000 | 80 | 49 | 177 | 0.05 | 0.18 |
| | | Shaver Road | NB | 500 | 54 | 160 | 224 | 0.32 | 0.45 |
| | | | SB | 500 | 34 | 221 | 201 | 0.44 | 0.40 |
| | | Fiddler's Green Road | NB | 1,000 | 170 | 233 | 429 | 0.23 | 0.43 |
| | | | SB | 1,000 | 145 | 296 | 424 | 0.30 | 0.42 |
| | | Highway 6 | NB | 1,800 | 582 | 713 | 1,837 | 0.40 | 1.02 |
| | | | SB | 1,800 | 290 | 267 | 1,547 | 0.15 | 0.86 |
| | | Southcote Road | NB | 500 | 144 | 42 | 289 | 0.08 | 0.58 |
| | | | SB | 500 | 68 | 39 | 393 | 0.08 | 0.79 |
| Glancaster Road | NB | 500 | 316 | 96 | 182 | 0.19 | 0.36 | | |
| | SB | 500 | 237 | 105 | 859 | 0.21 | 1.72 | | |
| Totals | NB | 5,300 | 1,440 | 1,587 | 3,419 | 0.30 | 0.65 | | |
| | SB | 5,300 | 854 | 977 | 3,601 | 0.18 | 0.68 | | |
| 2 | North of Garner Road | Trinity Road | NB | 1,000 | 353 | 356 | 473 | 0.36 | 0.47 |
| | | | SB | 1,000 | 359 | 250 | 501 | 0.25 | 0.50 |
| | | Wilson Street | NB | 2,000 | 377 | 115 | 104 | 0.06 | 0.05 |
| | | | SB | 2,000 | 464 | 262 | 454 | 0.13 | 0.23 |
| | | Shaver Road | NB | 500 | 58 | 281 | 409 | 0.56 | 0.82 |
| | | | SB | 500 | 65 | 204 | 335 | 0.41 | 0.67 |
| | | Hamilton Drive | NB | 400 | 99 | 20 | 61 | 0.05 | 0.15 |
| | | | SB | 400 | 199 | 108 | 151 | 0.27 | 0.38 |
| | | Fiddler's Green Road | NB | 700 | 259 | 304 | 503 | 0.43 | 0.72 |
| | | | SB | 700 | 429 | 174 | 217 | 0.25 | 0.31 |
| | | Highway 6 | NB | 1,800 | 582 | 713 | 1,837 | 0.40 | 1.02 |
| | | | SB | 1,800 | 290 | 267 | 1,547 | 0.15 | 0.86 |
| | | Highway 403 Ramp | NB | 1,400 | 133 | 282 | 115 | 0.20 | 0.08 |
| | | | SB | 1,400 | 69 | 130 | 582 | 0.09 | 0.42 |
| Southcote Road | NB | 700 | 270 | 71 | 242 | 0.10 | 0.35 | | |
| | SB | 700 | 261 | 123 | 548 | 0.18 | 0.78 | | |
| Kitty Murray Lane | NB | 400 | 61 | 59 | 60 | 0.15 | 0.15 | | |
| | SB | 400 | 89 | 48 | 341 | 0.12 | 0.85 | | |
| Totals | NB | 8,900 | 2,192 | 2,201 | 3,804 | 0.25 | 0.43 | | |
| | SB | 8,900 | 2,225 | 1,566 | 4,676 | 0.18 | 0.53 | | |
| 3 | South of Jerseyville Road | Shaver Road | NB | 500 | 38 | 182 | 272 | 0.36 | 0.54 |
| | | | SB | 500 | 120 | 68 | 186 | 0.14 | 0.37 |
| | | Meadowbrook Drive | NB | 400 | - | 185 | 194 | 0.46 | 0.49 |
| | | | SB | 400 | - | 74 | 58 | 0.19 | 0.15 |
| | | Fiddler's Green Road | NB | 700 | 457 | 295 | 309 | 0.42 | 0.44 |
| | | | SB | 700 | 368 | 235 | 319 | 0.34 | 0.46 |
| | | Wilson Street | NB | 900 | 841 | 515 | 636 | 0.57 | 0.71 |
| | | | SB | 900 | 581 | 306 | 518 | 0.34 | 0.58 |
| | | Southcote Road | NB | 700 | 342 | 192 | 394 | 0.27 | 0.56 |
| | | | SB | 700 | 189 | 76 | 374 | 0.11 | 0.53 |
| Kitty Murray Lane | NB | 400 | 341 | 145 | 172 | 0.36 | 0.43 | | |
| | SB | 400 | 162 | 7 | 122 | 0.02 | 0.31 | | |
| Stone Church Road | NB | 1,000 | 676 | 749 | 839 | 0.75 | 0.84 | | |
| | SB | 1,000 | 301 | 229 | 376 | 0.23 | 0.38 | | |
| Totals | NB | 4,600 | 2,695 | 2,263 | 2,816 | 0.49 | 0.61 | | |
| | SB | 4,600 | 1,721 | 995 | 1,953 | 0.22 | 0.42 | | |
| 4 | South of Lions Club Road | Sulphur Springs Road | NB | 400 | 85 | 336 | 472 | 0.84 | 1.18 |
| | | | SB | 400 | 125 | 158 | 256 | 0.40 | 0.64 |
| | | Old Dundas Road | NB | 400 | 296 | 383 | 478 | 0.96 | 1.20 |
| | | | SB | 400 | 267 | 370 | 421 | 0.93 | 1.05 |
| | | Wilson Street | NB | 1,000 | 742 | 847 | 1,130 | 0.85 | 1.13 |
| | | | SB | 1,000 | 187 | 153 | 389 | 0.15 | 0.39 |
| Highway 403 | NB | 3,600 | 4,146 | 3,976 | 4,790 | 1.10 | 1.33 | | |
| | SB | 3,600 | 2,362 | 1,806 | 3,000 | 0.50 | 0.83 | | |
| Totals | NB | 5,400 | 5,269 | 5,542 | 6,870 | 1.03 | 1.27 | | |
| | SB | 5,400 | 2,941 | 2,487 | 4,066 | 0.46 | 0.75 | | |
| 5 | East of Shaver Road | Garner Road | EB | 900 | 289 | 191 | 382 | 0.21 | 0.42 |
| | | | WB | 900 | 333 | 441 | 708 | 0.49 | 0.79 |
| | | Wilson Street | EB | 2,000 | 637 | 323 | 284 | 0.16 | 0.14 |
| | | | WB | 2,000 | 291 | 460 | 640 | 0.23 | 0.32 |
| | | Highway 403 | EB | 3,600 | 1,713 | 1,544 | 1,770 | 0.43 | 0.49 |
| | | | WB | 3,600 | 1,550 | 1,466 | 1,366 | 0.41 | 0.38 |
| Jerseyville Road | EB | 1,000 | 89 | 248 | 122 | 0.25 | 0.12 | | |
| | WB | 1,000 | 89 | 305 | 285 | 0.31 | 0.29 | | |
| Totals | EB | 7,500 | 2,728 | 2,306 | 2,558 | 0.31 | 0.34 | | |
| | WB | 7,500 | 2,263 | 2,672 | 2,999 | 0.36 | 0.40 | | |
| 6 | West of Fiddler's | Garner Road | EB | 900 | 429 | 211 | 491 | 0.23 | 0.55 |

| | | | | | | | | | |
|----|---------------------------|----------------------|-------|-------|-------|-------|-------|------|------|
| | Green Road | | WB | 900 | 499 | 373 | 728 | 0.41 | 0.81 |
| | | Highway 403 | EB | 3,600 | 2,143 | 1,830 | 2,110 | 0.51 | 0.59 |
| | | | WB | 3,600 | 1,939 | 1,839 | 1,957 | 0.51 | 0.54 |
| | | Amberly Blvd | EB | 400 | 514 | 355 | 356 | 0.89 | 0.89 |
| | | | WB | 400 | 121 | 39 | 47 | 0.10 | 0.12 |
| | | Wilson Street | EB | 900 | 841 | 471 | 322 | 0.52 | 0.36 |
| | | | WB | 900 | 581 | 351 | 293 | 0.39 | 0.33 |
| | | Jerseyville Road | EB | 700 | 356 | 319 | 258 | 0.46 | 0.37 |
| | | | WB | 700 | 258 | 220 | 242 | 0.31 | 0.35 |
| | | Totals | EB | 6,500 | 4,283 | 3,186 | 3,537 | 0.49 | 0.54 |
| WB | 6,500 | | 3,398 | 2,822 | 3,267 | 0.43 | 0.50 | | |
| 7 | West of Highway 6 | Garner Road | EB | 900 | 563 | 606 | 989 | 0.67 | 1.10 |
| | | | WB | 900 | 552 | 559 | 1,039 | 0.62 | 1.15 |
| | | Highway 403 | EB | 3,600 | 2,247 | 2,278 | 2,489 | 0.63 | 0.69 |
| | | | WB | 3,600 | 2,033 | 2,030 | 2,156 | 0.56 | 0.60 |
| | | Wilson Street | EB | 900 | 835 | 738 | 820 | 0.82 | 0.91 |
| | | | WB | 900 | 560 | 436 | 499 | 0.48 | 0.55 |
| | | Sulphur Springs Road | EB | 500 | 343 | 241 | 198 | 0.48 | 0.40 |
| | | | WB | 500 | 111 | 192 | 214 | 0.38 | 0.43 |
| | | Totals | EB | 5,900 | 3,988 | 3,863 | 4,496 | 0.65 | 0.76 |
| | | | WB | 5,900 | 3,256 | 3,217 | 3,908 | 0.55 | 0.66 |
| 8 | West of Southcote Road | Garner Road | EB | 900 | 574 | 451 | 1,514 | 0.50 | 1.68 |
| | | | WB | 900 | 471 | 555 | 1,087 | 0.62 | 1.21 |
| | | Highway 403 | EB | 3,600 | 2,629 | 2,945 | 3,402 | 0.82 | 0.95 |
| | | | WB | 3,600 | 2,379 | 2,100 | 3,257 | 0.58 | 0.90 |
| | | Golf Links Road | EB | 500 | 280 | 386 | 512 | 0.77 | 1.02 |
| | | | WB | 500 | 330 | 329 | 489 | 0.66 | 0.98 |
| | | Mohawk Road | EB | 700 | 849 | 619 | 799 | 0.88 | 1.14 |
| | | | WB | 700 | 892 | 742 | 1,000 | 1.06 | 1.43 |
| | | Totals | EB | 5,700 | 4,332 | 4,401 | 6,227 | 0.77 | 1.09 |
| | | | WB | 5,700 | 4,072 | 3,726 | 5,833 | 0.65 | 1.02 |
| 9 | West of Stone Church Road | Garner Road | EB | 1,000 | 461 | 397 | 525 | 0.40 | 0.53 |
| | | | WB | 1,000 | 409 | 541 | 1,243 | 0.54 | 1.24 |
| | | Mohawk Road | EB | 1,800 | 958 | 331 | 228 | 0.18 | 0.13 |
| | | | WB | 1,800 | 1,077 | 158 | 225 | 0.09 | 0.13 |
| | | Totals | EB | 2,800 | 1,419 | 728 | 422 | 0.26 | 0.15 |
| | | | WB | 2,800 | 1,486 | 699 | 405 | 0.25 | 0.14 |

| | |
|--|----------------------------|
| | Individual Link Congestion |
| | Screenline Congestion |

4.3 HTMP Improvements Scenario

Using the “do nothing” scenario as a starting point, proposed HTMP roadway projects were added to the Ancaster model networks, as appropriate, for the 2016, 2021, and 2031 horizon years. These modifications reflect the *Proposed Road Infrastructure Improvements* table outlined in the HTMP.

Table 12 summarizes the HTMP improvements recommended for implementation in Ancaster, as input into the model. The horizon denotes the earliest year a specific improvement was included in the model.

Table 12 - HTMP Planned Infrastructure Improvements (Ancaster Projects)

| Road Name | From | To | Description | Horizon ¹ |
|------------------|-------------------------------|----------------------|-------------------------|----------------------|
| Garner Road | Shaver Road | Fiddler’s Green Road | Road Widening and TWLTL | 2021 |
| Golf Links Road | McNiven Road | Kitty Murray Lane | TWLTL | 2021 |
| Jerseyville Road | Shaver Road | Wilson Street | TWLTL | 2021 |
| McNiven Road | Rousseaux Street | Golf Links Road | Road Widening | 2016 |
| Mohawk Road | McNiven Road | Highway 403 | Road Widening | 2016 |
| Scenic Drive | Lavender Drive (South Leg) | Old City Limits | TWLTL | 2016 |
| Shaver Road | Wilson Street | Garner Road | TWLTL | 2021 ² |
| Southcote Road | Golf Links Road | Garner Road | Road Widening | 2021 |
| Trinity Road | 1km S of Wilson St | Highway 403 | Road Widening | 2031 |
| Wilson Street | Hamilton Drive | Halsen Street | Road Widening | 2021 |
| | | | | |

Notes:

¹ Denotes the earliest year a specific improvement was included in the model.

² Project implemented earlier than HTMP anticipated timing.

TWLTL = Two-Way Left Turn Lane

4.4 Future Horizon Years and Base Scenarios

In the Ancaster transportation demand model, three future horizon years were examined: 2016, 2021, and 2031.

The 2016 and 2021 horizons are interim years in the Ancaster TMP. The primary use of the 2016 and 2021 horizons were to review the impacts of increased population and employment on the existing road network under a “do nothing” scenario and to evaluate the impacts of the HTMP proposed improvements. The 2016 and 2021 horizons were also used in the phasing (i.e. timing) of recommended roadway projects determined in the 2031 horizon.

The 2031 horizon year was primarily used for the testing of various roadway scenarios in the Ancaster area. This was used to compare suggested roadway modification scenarios to the proposed HTMP improvements (used as the base case). The transportation scenario results from the EMME/2 Ancaster model were used with the overall transportation master plan (TMP) evaluation criteria to determine the recommended scenario, as evaluated in the Ancaster TMP report.

The following exhibits represent the auto volumes and volume-to-capacity (v/c) ratios for the 2016, 2021, and 2031 horizons:

- **Exhibits 1 to 2** – 2016 “Do Nothing” Scenario
- **Exhibits 3 to 4** – 2016 HTMP Improvements Scenario
- **Exhibits 5 to 6** – 2021 “Do Nothing” Scenario
- **Exhibits 7 to 8** – 2021 HTMP Improvements Scenario
- **Exhibits 9 to 10** – 2031 “Do Nothing” Scenario
- **Exhibits 11 to 12** – 2031 HTMP Improvements Scenario

Note: Exhibits are located at the end of this document.

4.5 2031 Scenario Testing

Various scenarios were tested in the 2031 horizon Ancaster model to examine proposed network capacity and access improvements. The results of each scenario can then be analyzed compared to the base 2031 conditions (i.e. HTMP Improvements Scenario) to determine the impact of each proposed roadway improvement. Modifications to the roadway network for each scenario are listed in **Table 13** below and shown in **Figure 8**.

Table 13 – 2031 Scenario Descriptions

| Scenario Name | Description |
|---|--|
| “Do Nothing” (S0) | <ul style="list-style-type: none"> • No improvements. Same roadway network as 2006 Base Year. |
| HTMP Improvements (S1) | <ul style="list-style-type: none"> • Added the proposed HTMP improvements as outlined in Table 12. |
| Mohawk On-Ramp to Hwy 403 WB (S2) | <ul style="list-style-type: none"> • Re-establish an on-ramp from EB Mohawk Road to WB Highway 403. |
| Golf Links Ramps (S3) | <ul style="list-style-type: none"> • Add off-ramp from Highway 403 EB to Golf Links Road. • Add on-ramp from Golf Links Road to Highway 403 WB. |
| Widen Rousseaux (S4) | <ul style="list-style-type: none"> • Widening to four-lane cross section between Wilson Street and McNiven Road. |
| Wilson Two-Way Left Turn Lane (S5) | <ul style="list-style-type: none"> • Three-lane cross section, including two-way left turn lane, between Fiddler’s Green Road and Halson Street. |
| Widen Rousseaux and Maintain Mohawk Cross-Section (S6) | <ul style="list-style-type: none"> • Widen Rousseaux (same as S4) and maintain current two-lane cross section on Mohawk (no HTMP improvement) between McNiven Road and Highway 403. |
| Maintain McNiven Cross-Section (S7) | <ul style="list-style-type: none"> • Maintain existing two-lane cross section (no HTMP improvement) between Mohawk Road and Golf Links Road. |
| Combination of S3 & S7 (S8) | <ul style="list-style-type: none"> • Combination of roadway improvements listed in S3 and S7. |
| Combination of S3 & S4 (S9) | <ul style="list-style-type: none"> • Combination of roadway improvements listed in S3 and S7. |
| Lime Kiln Link (S10) | <ul style="list-style-type: none"> • Two-lane extension of Lime Kiln Road north of Mohawk Road to Wilson Street. |
| Combination of S5, S6, & S7 (S11) | <ul style="list-style-type: none"> • Combination of roadway improvements listed in S5, S6, and S7. |
| Wilson, Rousseaux, Mohawk, and McNiven Two-Way Left Turn Lane (S12) | <ul style="list-style-type: none"> • Three-lane cross-sections with two-way left turn lanes on selected links: <ul style="list-style-type: none"> ○ Wilson Street between Fiddler’s Green Road and Halson Street. ○ Rousseaux Street / Mohawk Road between Wilson Street and Highway 403. ○ McNiven Road between Mohawk Road and Golf Links Road. |

HAMILTON TRANSPORTATION MASTER PLAN RECOMMENDATIONS*

- Includes all planned HTMP improvements to 2031
- AM Peak Volume Impacts: Wilson (Town Centre) 790 vph, Rousseaux 1010 vph, Mohawk 1240 vph, McNiven 830 vph

MOHAWK ON-RAMP TO HWY 403 WB (S2)

- Negligible network impacts
- No support from MTO
- AM Peak Volume Impacts: Wilson (Town Centre) 790 vph, Rousseaux 1000 vph, Mohawk 1280 vph, McNiven 820 vph

GOLF LINKS RAMPS (S3)

- Traffic primarily to/from south and east Ancaster (e.g. not Town Centre area)
- AM Peak Volume Impacts: Wilson (Town Centre) 780 vph, Rousseaux 980 vph, Mohawk 1290 vph, McNiven 870 vph

WIDEN ROUSSEAUX (S4)

- Some traffic drawn from Halson / Golf Links to extra capacity on Rousseaux
- AM Peak Volume Impacts: Wilson (Town Centre) 790 vph, Rousseaux 1460 vph, Mohawk 1370 vph, McNiven 810 vph

MAINTAIN MCNIVEN CROSS-SECTION (S7)

- Reduce speed to 40 km/h
- Reduced volumes on McNiven and Mohawk
- Minor volume increase on Wilson (Town Centre)
- AM Peak Volume Impacts: Wilson (Town Centre) 840 vph, Rousseaux 1000 vph, Mohawk 1080 vph, McNiven 500 vph

LIME KILN LINK (S10)

- Not to be carried forward due to technical confirmation
- More volume to Wilson / Rousseaux Area
- Lime Kiln draws significant volume of 560 vph
- AM Peak Volume Impacts: Wilson (Town Centre) 740 vph, Rousseaux 830 vph, Mohawk 1290 vph, McNiven 870 vph

COMBINATION OF S3 & S7 (S8)

- Minor improvement on Halson / Golf Links
- Travel favoured on Wilson (Town Centre)
- AM Peak Volume Impacts: Wilson (Town Centre) 890 vph, Rousseaux 970 vph, Mohawk 1140 vph, McNiven 480 vph

COMBINATION OF S5, S6, & S7 (S11)

- Minor improvement on Halson / Golf Links
- Travel favoured on Wilson (Town Centre)
- AM Peak Volume Impacts: Wilson (Town Centre) 890 vph, Rousseaux 970 vph, Mohawk 1140 vph, McNiven 480 vph

WILSON TWO-WAY LEFT TURN LANE (S5)

- Negligible network impacts
- AM Peak Volume Impacts: Wilson (Town Centre) 780 vph, Rousseaux 1010 vph, Mohawk 1230 vph, McNiven 830 vph

WIDEN ROUSSEAUX & MAINTAIN MOHAWK CROSS-SECTION (S6)

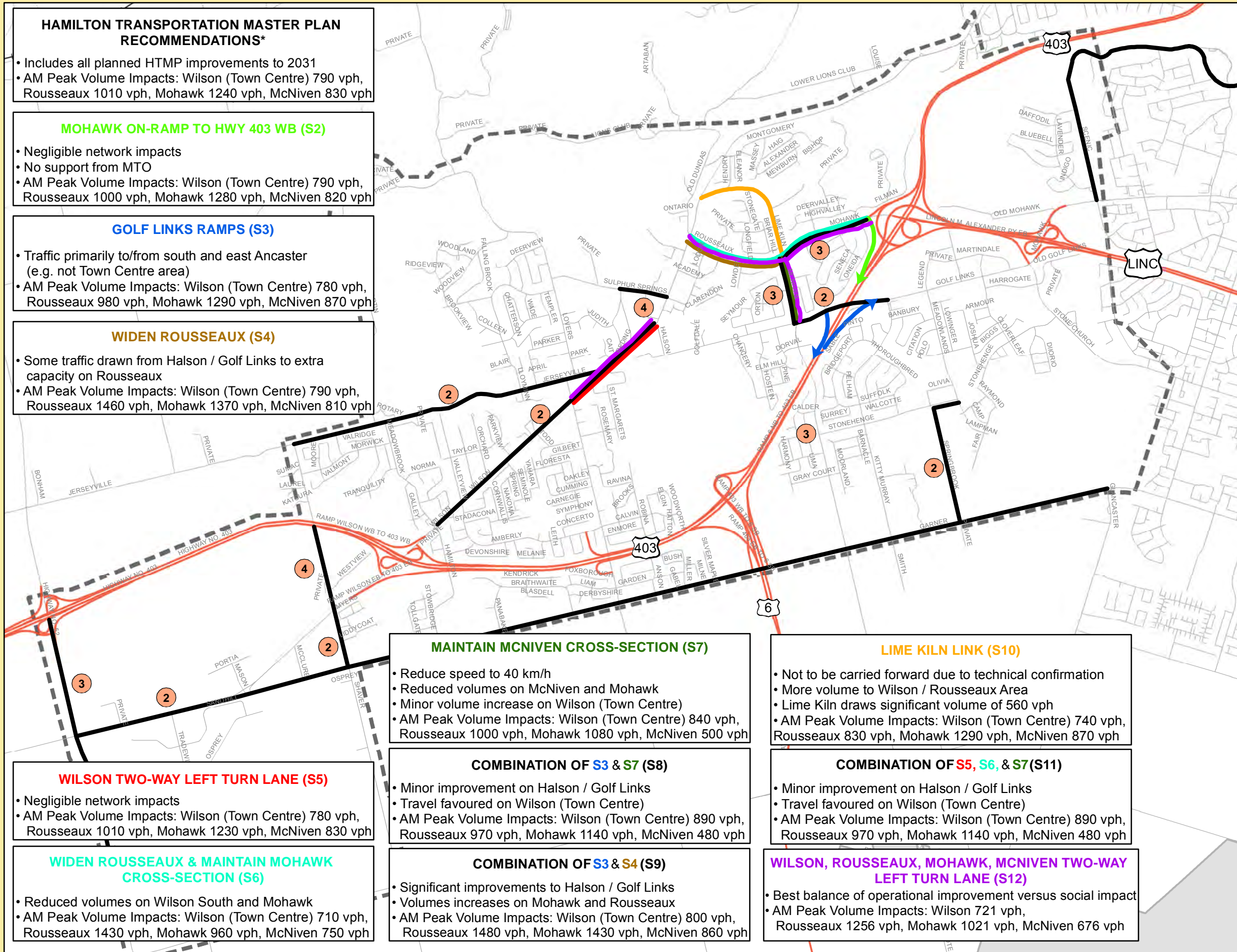
- Reduced volumes on Wilson South and Mohawk
- AM Peak Volume Impacts: Wilson (Town Centre) 710 vph, Rousseaux 1430 vph, Mohawk 960 vph, McNiven 750 vph

COMBINATION OF S3 & S4 (S9)

- Significant improvements to Halson / Golf Links
- Volumes increases on Mohawk and Rousseaux
- AM Peak Volume Impacts: Wilson (Town Centre) 800 vph, Rousseaux 1480 vph, Mohawk 1430 vph, McNiven 860 vph

WILSON, ROUSSEAUX, MOHAWK, MCNIVEN TWO-WAY LEFT TURN LANE (S12)

- Best balance of operational improvement versus social impact
- AM Peak Volume Impacts: Wilson 721 vph, Rousseaux 1256 vph, Mohawk 1021 vph, McNiven 676 vph



- Legend**
- Highway
 - Existing Road Network
 - - - Ancaster Study Area
- Hamilton Transportation Master Plan Improvements (May 2007)**
- ② Two-Way Left Turn Lane
 - ③ Road Widening
 - ④ Conversion to Urban Cross-Section

*HTMP recommendations are shown as they relate to a number of scenarios.

Note:
Scenario 1-Do Nothing was not included as it represents the existing roadway network conditions

4.5.1 EMME/2 2031 Ancaster Result Plots

For each scenario defined in **Table 13**, the EMME/2 network was modified to reflect the change and an assignment run completed to determine the impacts on the network.

The following result plots have been produced for each scenario run in EMME/2:

- **Exhibits 13 to 15** – Mohawk On-Ramp to Hwy 403 WB (S2) volume, select link, and v/c plots.
- **Exhibits 16 to 18** – Golf Links Ramps (S3) volume, select link, and v/c plots.
- **Exhibits 19 to 21** – Widen Rousseaux (S4) volume, select link, and v/c plots.
- **Exhibits 22 to 23** – Wilson Two-Way Left Turn Lane (S5) volume and v/c plots.
- **Exhibits 24 to 25** – Widen Rousseaux and Maintain Mohawk Cross-Section (S6) volume and v/c plots.
- **Exhibits 26 to 27** – Maintain McNiven Cross-Section (S7) volume and v/c plots.
- **Exhibits 28 to 29** – Combination of S3 and S7 (S8) volume and v/c plots.
- **Exhibits 30 to 31** – Combination of S3 and S4 (S9) volume and v/c plots.
- **Exhibits 32 to 34** – Lime Kiln Link (S10) volume, select link, and v/c plots.
- **Exhibits 35 to 36** – Combination of S5, S6, and S7 (S11) volume and v/c plots.
- **Exhibits 37 to 38** – Wilson, Rousseaux, Mohawk, and McNiven Two-Way Left Turn Lane (S12) volume and v/c plots.

Note: Exhibits are located at the end of this document.

4.5.2 EMME/2 2031 Ancaster Corridor Impacts

In order to compare and contrast the Ancaster model results between the various scenarios tested in EMME/2, a summary sheet was created in **Table 14**. This table identifies key corridors and examines the peak direction roadway link volumes, change in volume compared to the base HTMP Improvements (S0) scenario, and the volume-to-capacity (v/c) ratio experienced.

Table 14 – 2031 Corridor Impacts

| Corridor Name | Wilson Street | | | | | | | | | Rousseaux Street / Mohawk Road | | | | | | McNiven Road | | | Golf Links Road | | | Fiddler's Green Road | | | | | |
|---|-------------------------------------|----------------------------|------|---------------------------------------|----------------------------|------|-----------------------------------|----------------------------|------|--------------------------------------|----------------------------|------|-------------------------------|----------------------------|------|-----------------------------|----------------------------|------|--------------------------------|----------------------------|------|-------------------------------|----------------------------|------|------------------------------|----------------------------|------|
| | Highway 403 to Fiddler's Green Road | | | Fiddler's Green Road to Halson Street | | | Halson Street to Rousseaux Street | | | Rousseaux Street to Montgomery Drive | | | Wilson Street to McNiven Road | | | McNiven Road to Highway 403 | | | Mohawk Road to Golf Links Road | | | Halson Street to McNiven Road | | | Wilson Street to Highway 403 | | |
| Scenario Descriptions | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C | Volume ¹ | Volume Change ² | V/C |
| "Do Nothing" Conditions (S0) | 370 | - | 0.41 | 820 | - | 0.91 | 760 | - | 0.84 | 1,510 | - | 1.67 | 1,000 | - | 1.40 | 910 | - | 1.01 | 580 | - | 0.82 | 530 | - | 1.06 | 750 | - | 1.07 |
| Hamilton Transportation Master Plan (HTMP) Improvements (S1) | 380 | - | 0.23 | 890 | - | 0.49 | 790 | - | 0.87 | 1,530 | - | 1.70 | 1,010 | - | 1.41 | 1,240 | - | 0.69 | 840 | - | 0.60 | 530 | - | 1.06 | 730 | - | 1.04 |
| Mohawk On-Ramp to Highway 403 WB (S2) | 370 | -10 | 0.31 | 880 | -10 | 0.49 | 790 | 0 | 0.88 | 1,520 | -10 | 1.68 | 1,000 | -10 | 1.38 | 1,280 | 40 | 0.71 | 830 | -10 | 0.59 | 530 | 0 | 1.06 | 730 | 0 | 1.04 |
| Golf Links Ramps (S3) | 380 | 0 | 0.28 | 840 | -50 | 0.47 | 780 | -10 | 0.87 | 1,530 | 0 | 1.69 | 990 | -20 | 1.35 | 1,300 | 60 | 0.72 | 870 | 30 | 0.62 | 510 | -20 | 1.02 | 730 | 0 | 1.04 |
| Widen Rousseaux Street (S4) | 400 | 20 | 0.32 | 770 | -120 | 0.42 | 790 | 0 | 0.87 | 1,610 | 80 | 1.78 | 1,460 | 450 | 1.04 | 1,370 | 130 | 0.76 | 810 | -30 | 0.56 | 450 | -80 | 0.89 | 680 | -50 | 0.97 |
| Wilson Two-Way Left Turn Lane (S5) | 370 | -10 | 0.32 | 870 | -20 | 0.64 | 790 | 0 | 0.87 | 1,530 | 0 | 1.69 | 1,010 | 0 | 1.41 | 1,240 | 0 | 0.69 | 840 | 0 | 0.59 | 530 | 0 | 1.05 | 740 | 10 | 1.04 |
| Widen Rousseaux Street and Maintain Mohawk Cross-Section (S6) | 380 | 0 | 0.34 | 750 | -140 | 0.41 | 710 | -80 | 0.78 | 1,600 | 70 | 1.78 | 1,440 | 430 | 1.01 | 970 | -270 | 1.07 | 750 | -90 | 0.53 | 480 | -50 | 0.95 | 690 | -40 | 0.98 |
| Maintain McNiven Cross-Section (S7) | 380 | 0 | 0.33 | 870 | -20 | 0.48 | 850 | 60 | 0.93 | 1,520 | -10 | 1.68 | 1,000 | -10 | 1.39 | 1,080 | -160 | 0.60 | 500 | -340 | 0.71 | 520 | -10 | 1.04 | 750 | 20 | 1.06 |
| Combine S3 & S7 (S8) | 370 | -10 | 0.30 | 740 | -150 | 0.41 | 900 | 110 | 0.99 | 1,530 | 0 | 1.69 | 980 | -30 | 1.34 | 1,150 | -90 | 0.63 | 490 | -350 | 0.69 | 510 | -20 | 1.01 | 750 | 20 | 1.07 |
| Combine S3 & S4 (S9) | 410 | 30 | 0.25 | 760 | -130 | 0.42 | 810 | 20 | 0.89 | 1,620 | 90 | 1.79 | 1,480 | 470 | 1.03 | 1,440 | 200 | 0.80 | 870 | 30 | 0.62 | 420 | -110 | 0.84 | 690 | -40 | 0.98 |
| Lime Kiln Link (S10) | 370 | -10 | 0.35 | 780 | -110 | 0.43 | 740 | -50 | 0.82 | 1,660 | 130 | 1.84 | 840 | -170 | 1.16 | 1,300 | 60 | 0.72 | 870 | 30 | 0.60 | 490 | -40 | 0.97 | 690 | -40 | 0.98 |
| Combine S5, S6, & S7 (S11) | 370 | -10 | 0.35 | 750 | -140 | 0.55 | 740 | -50 | 0.82 | 1,590 | 60 | 1.76 | 1,360 | 350 | 0.97 | 950 | -290 | 1.05 | 570 | -270 | 0.76 | 480 | -50 | 0.95 | 690 | -40 | 0.98 |
| Wilson, Rousseaux, Mohawk, and McNiven Two-Way Left Turn Lane (S12) | 370 | -10 | 0.33 | 780 | -110 | 0.57 | 730 | -60 | 0.78 | 1,570 | 40 | 1.74 | 1,260 | 250 | 1.17 | 1,030 | -210 | 0.97 | 680 | -160 | 0.64 | 490 | -40 | 0.97 | 690 | -40 | 0.98 |

Notes:

¹ Represents highest peak direction link volume on corridor; Rounded up to nearest 10 vph

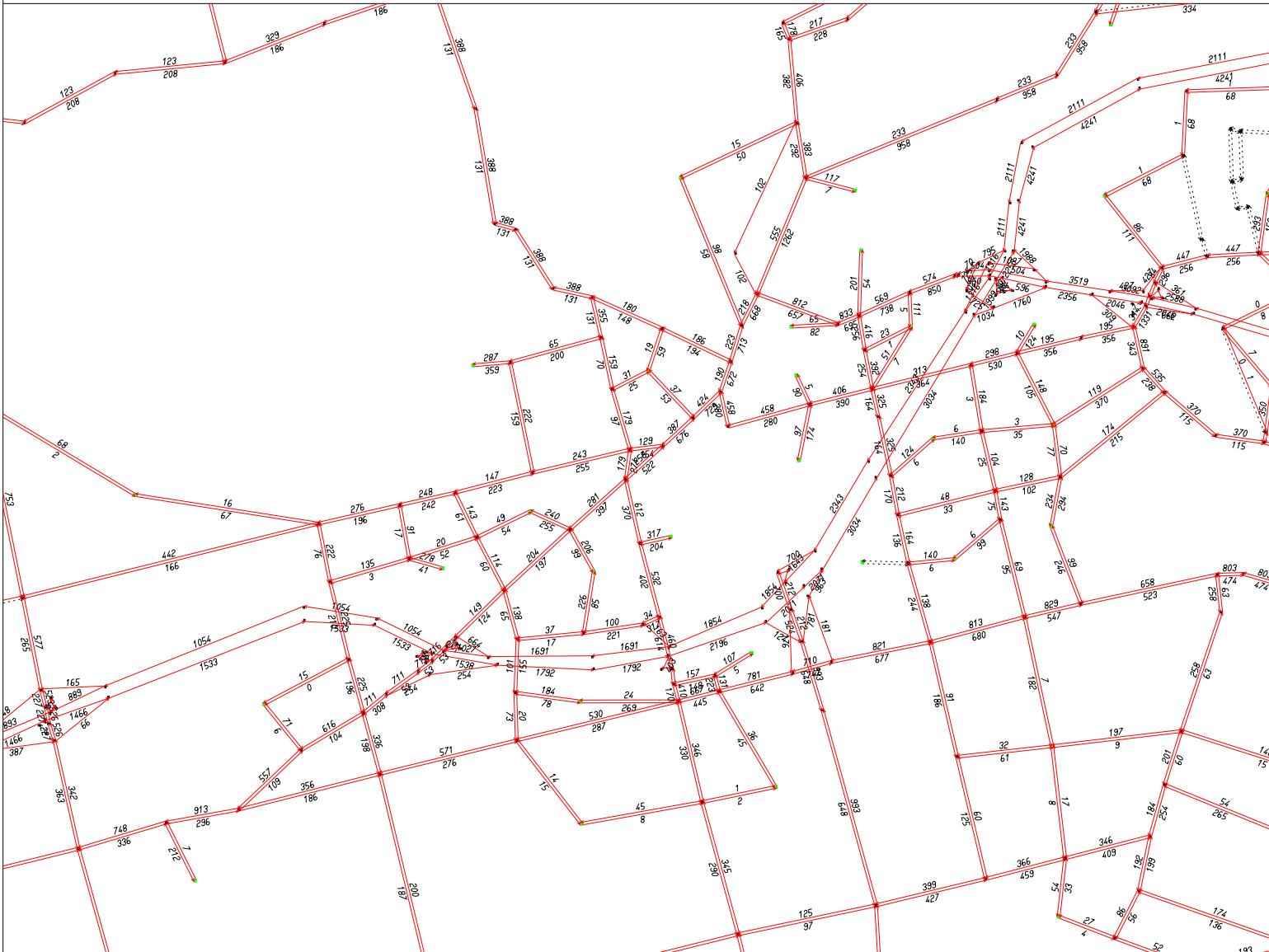
² Volume change compared to HTMP Improvements (S1)

EXHIBITS

AUTO VOLUMES

emme/2

Exhibit 1:
2016
"Do Nothing"
Volumes



10-08-13 18:07
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

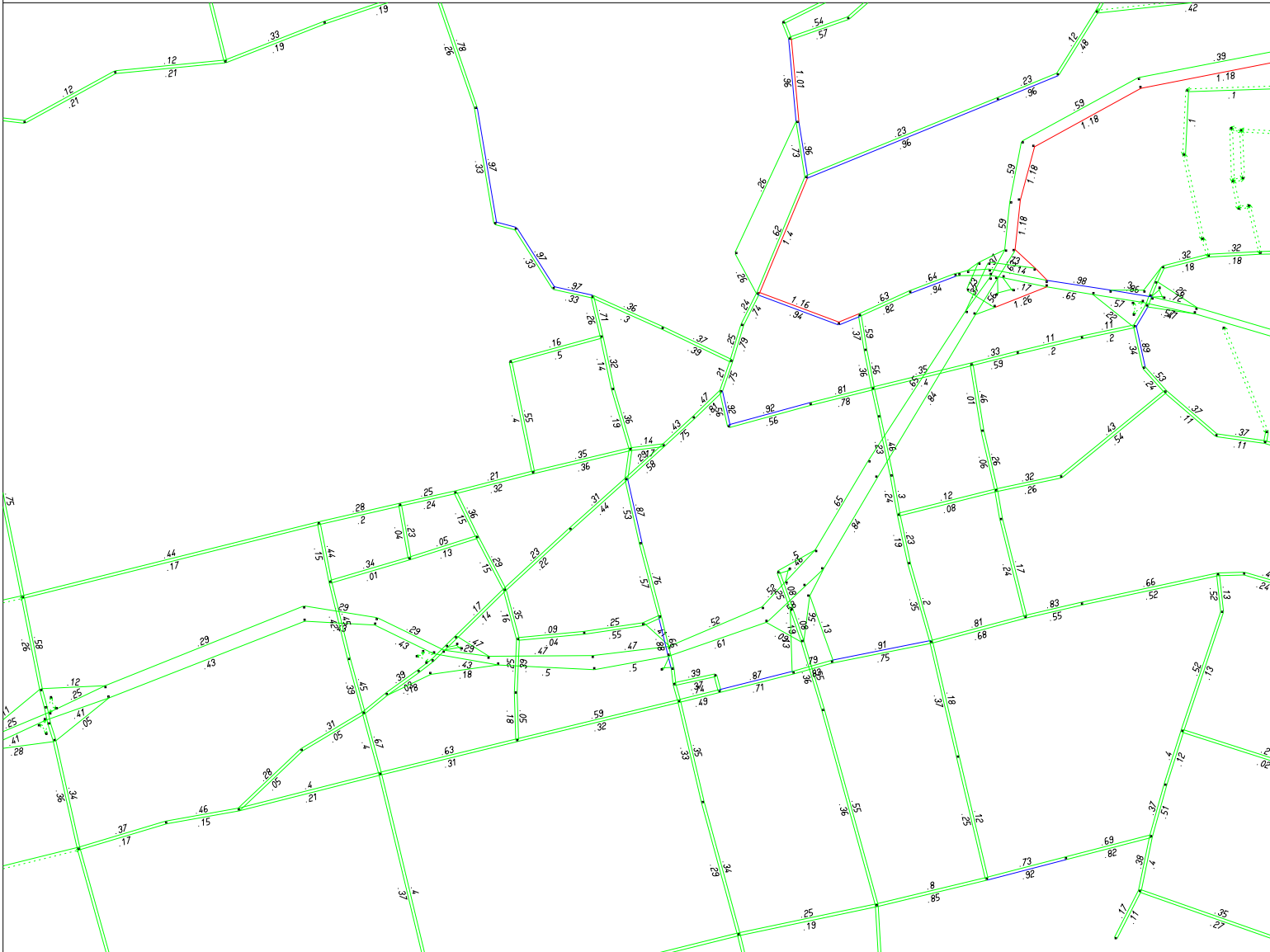


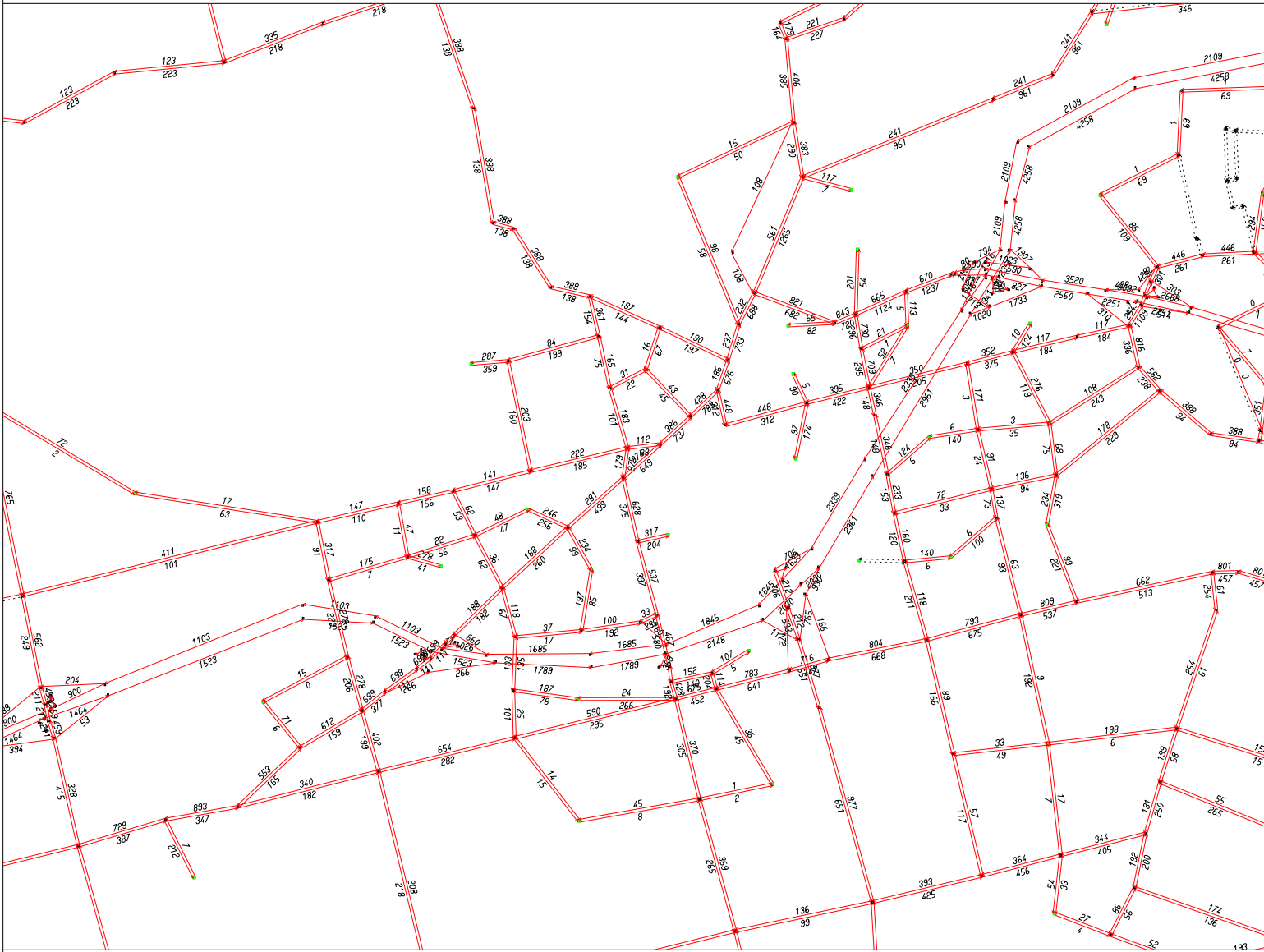
Exhibit 2:
2016
"Do Nothing"
V/C

10-08-13 18:08
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 3:
2016
HTMP
Improvements
Volumes



10-08-13 18:52
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

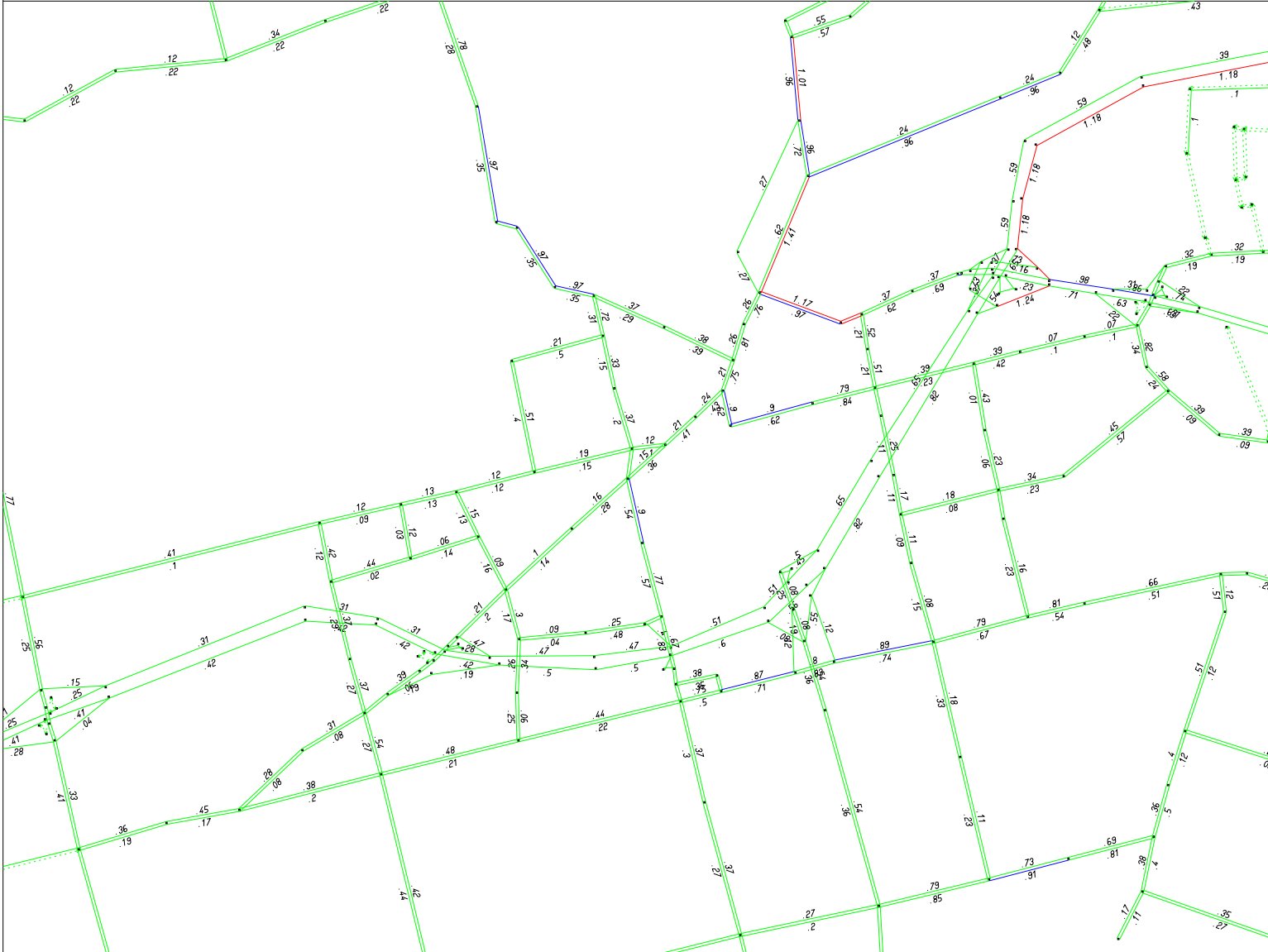


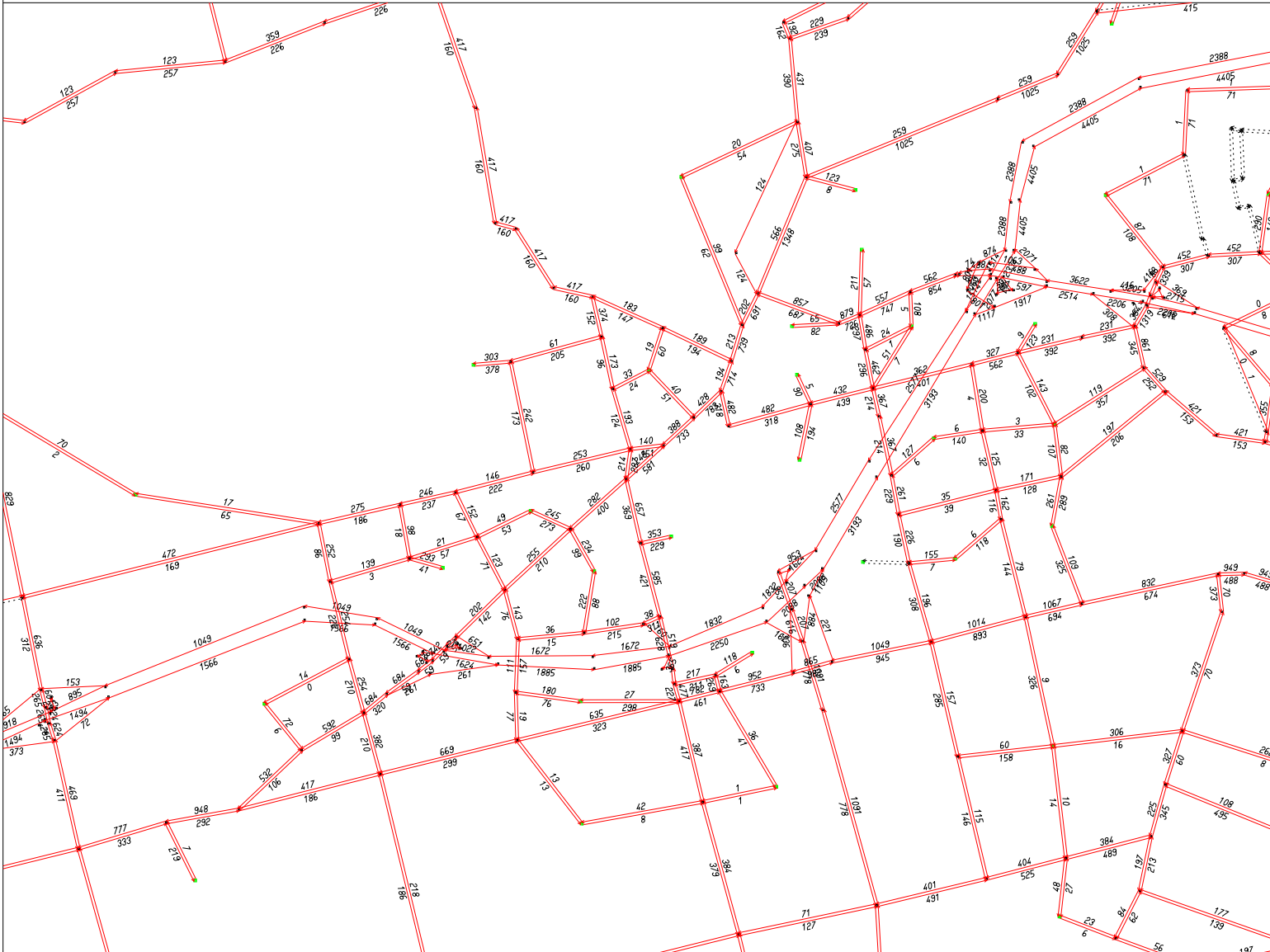
Exhibit 4:
2016
HTMP
Improvements
V/C

10-08-13 18:54
MODULE: 2.13
DMG.UTYU...j dk

AUTO VOLUMES

emme/2

Exhibit 5:
2021
"Do Nothing"
Volumes



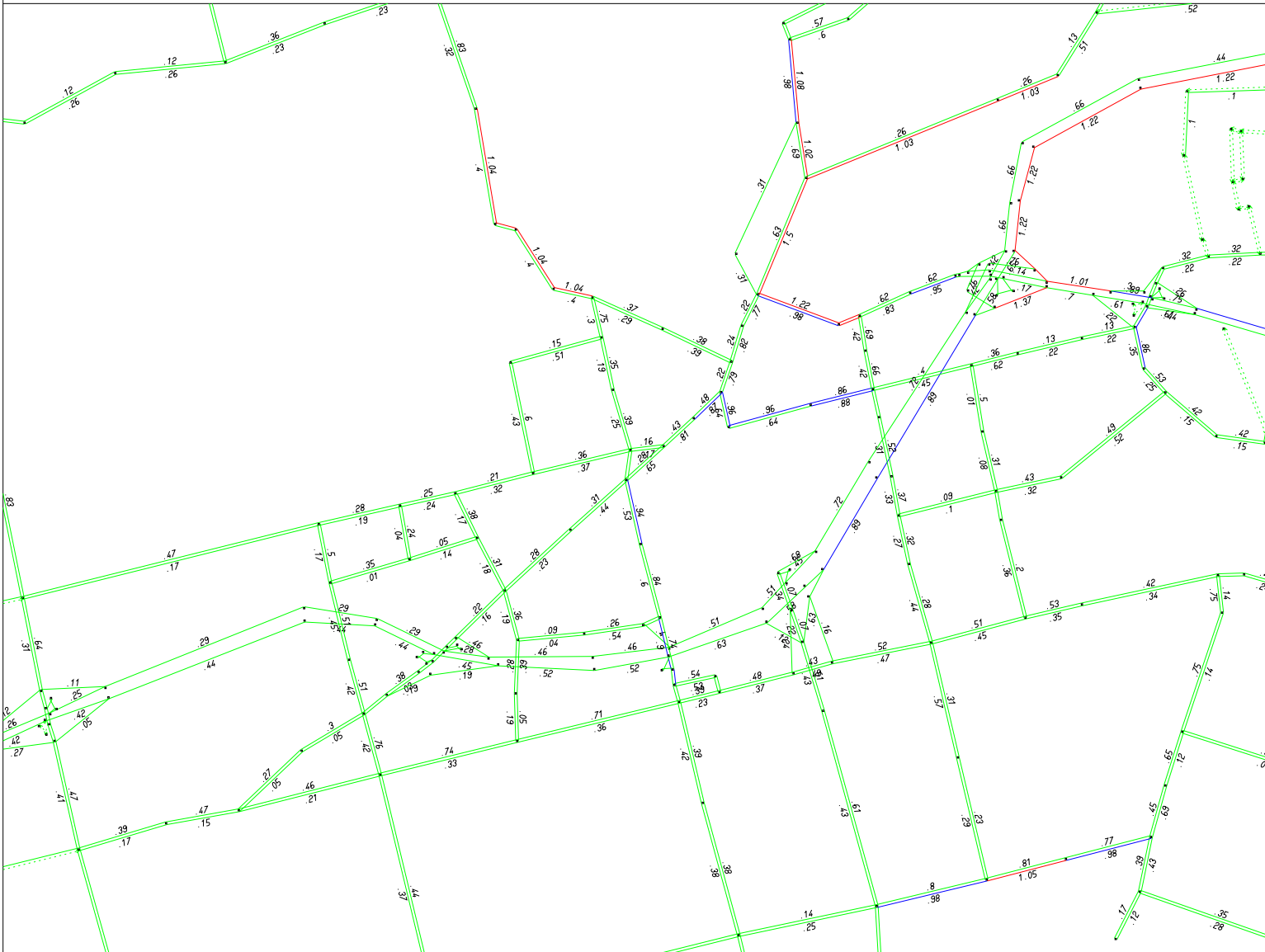
10-08-13 18:09
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 6:
2021
"Do Nothing"
V/C

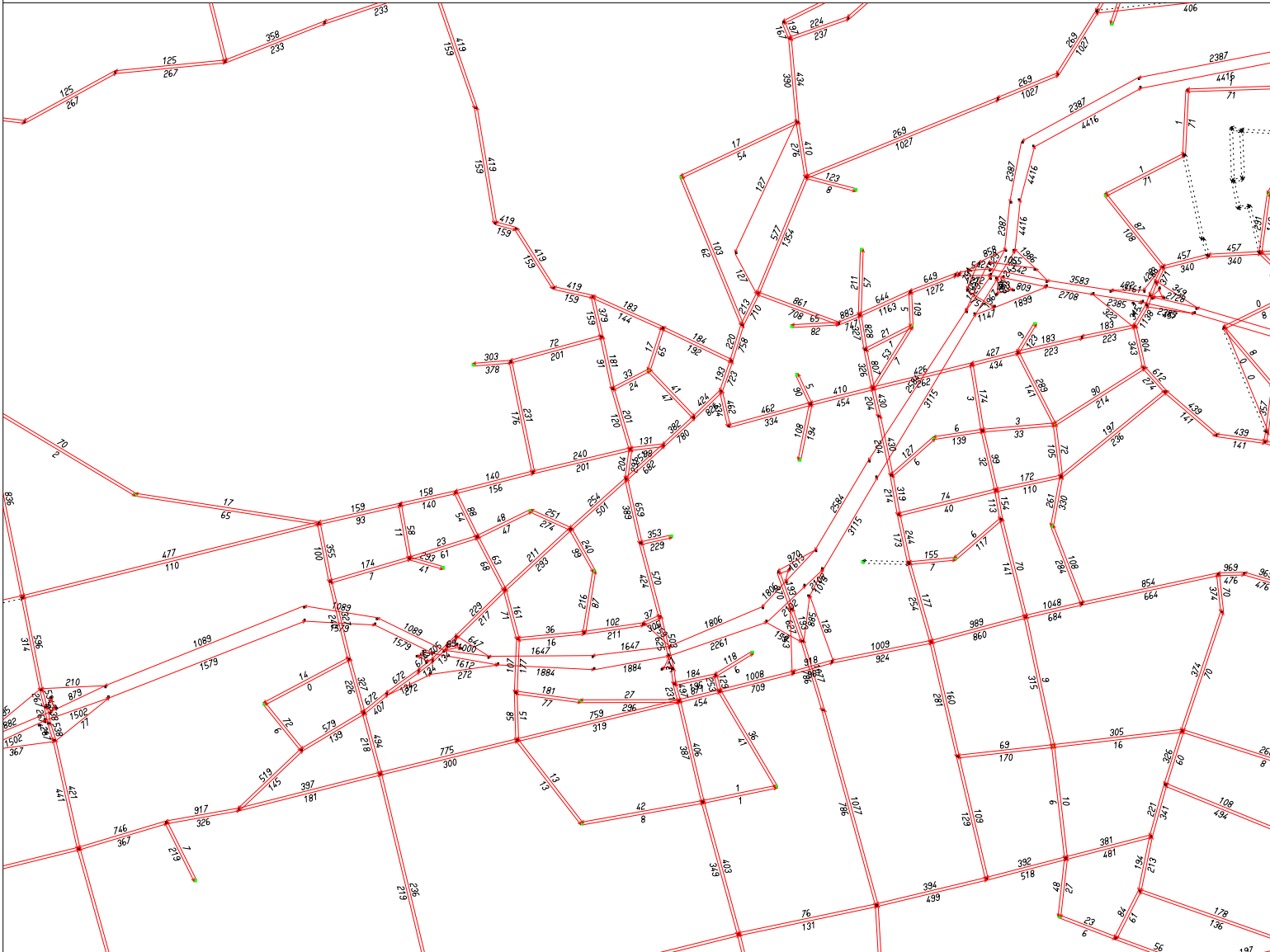


10-08-13 18:09
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 7:
2021
HTMP
Improvements
Volumes



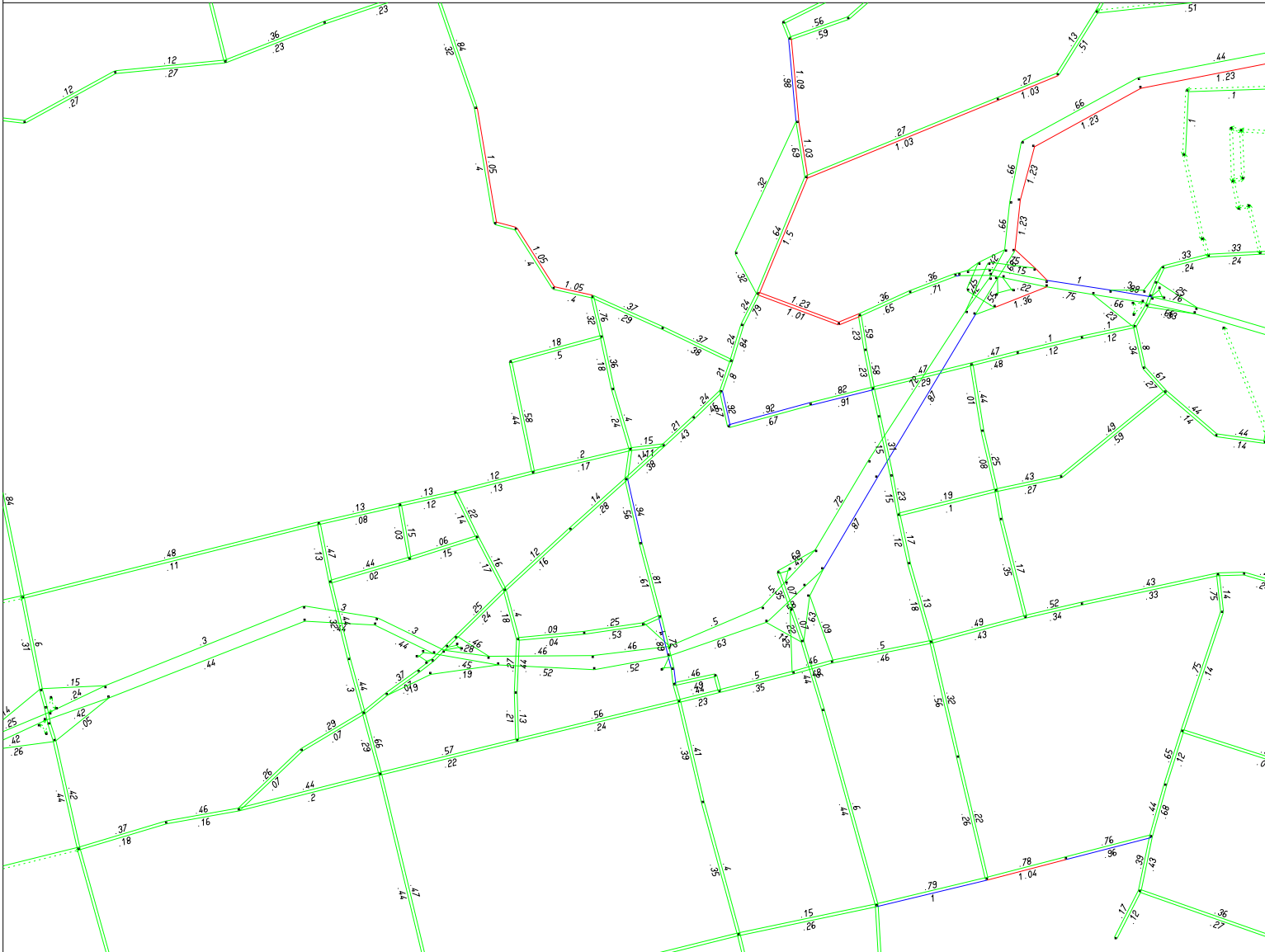
10-08-16 08:18
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 8:
2021
HTMP
Improvements
V/C

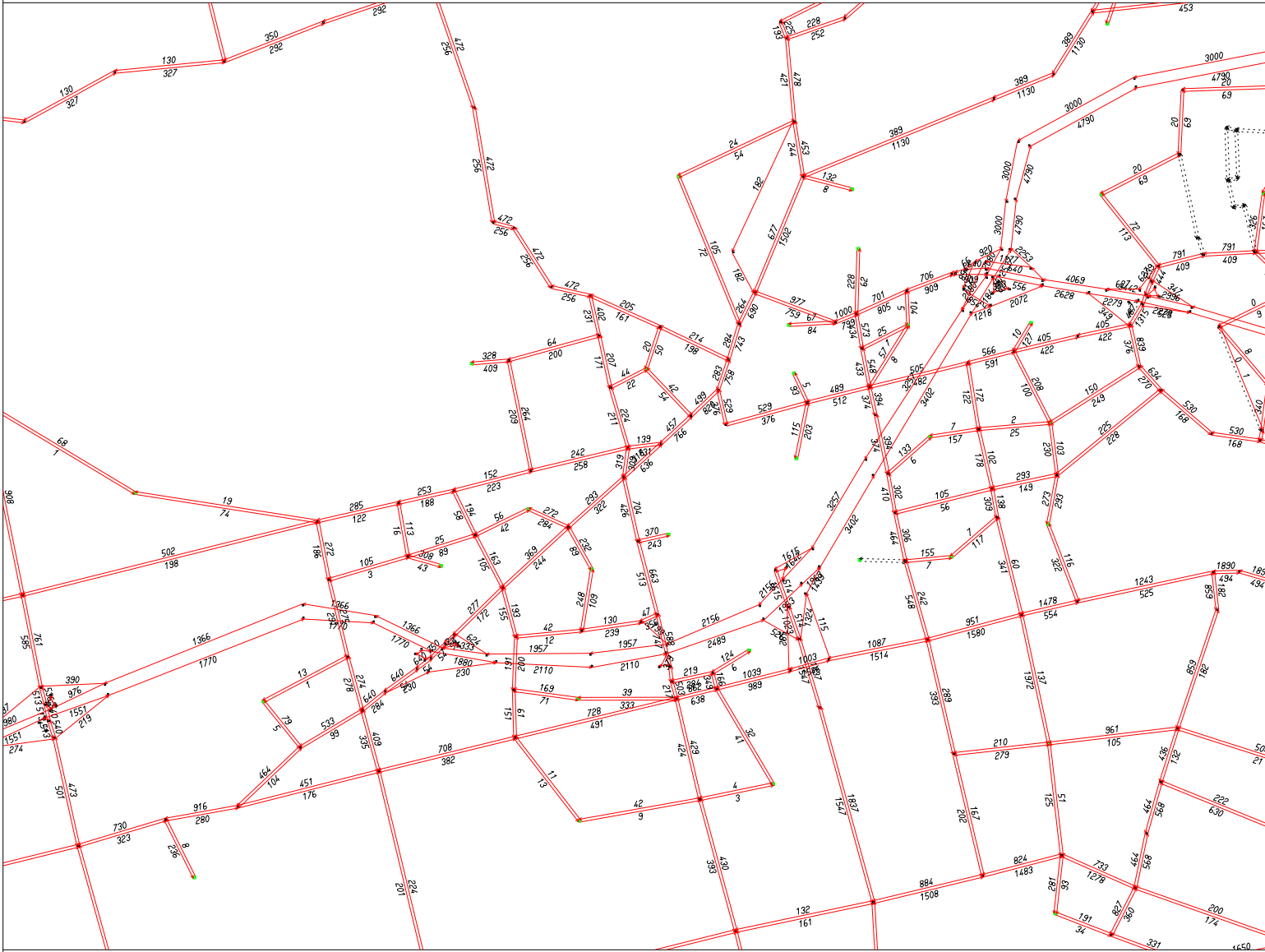


10-08-16 08:19
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 9: 2031 "Do Nothing" Volumes



BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme2

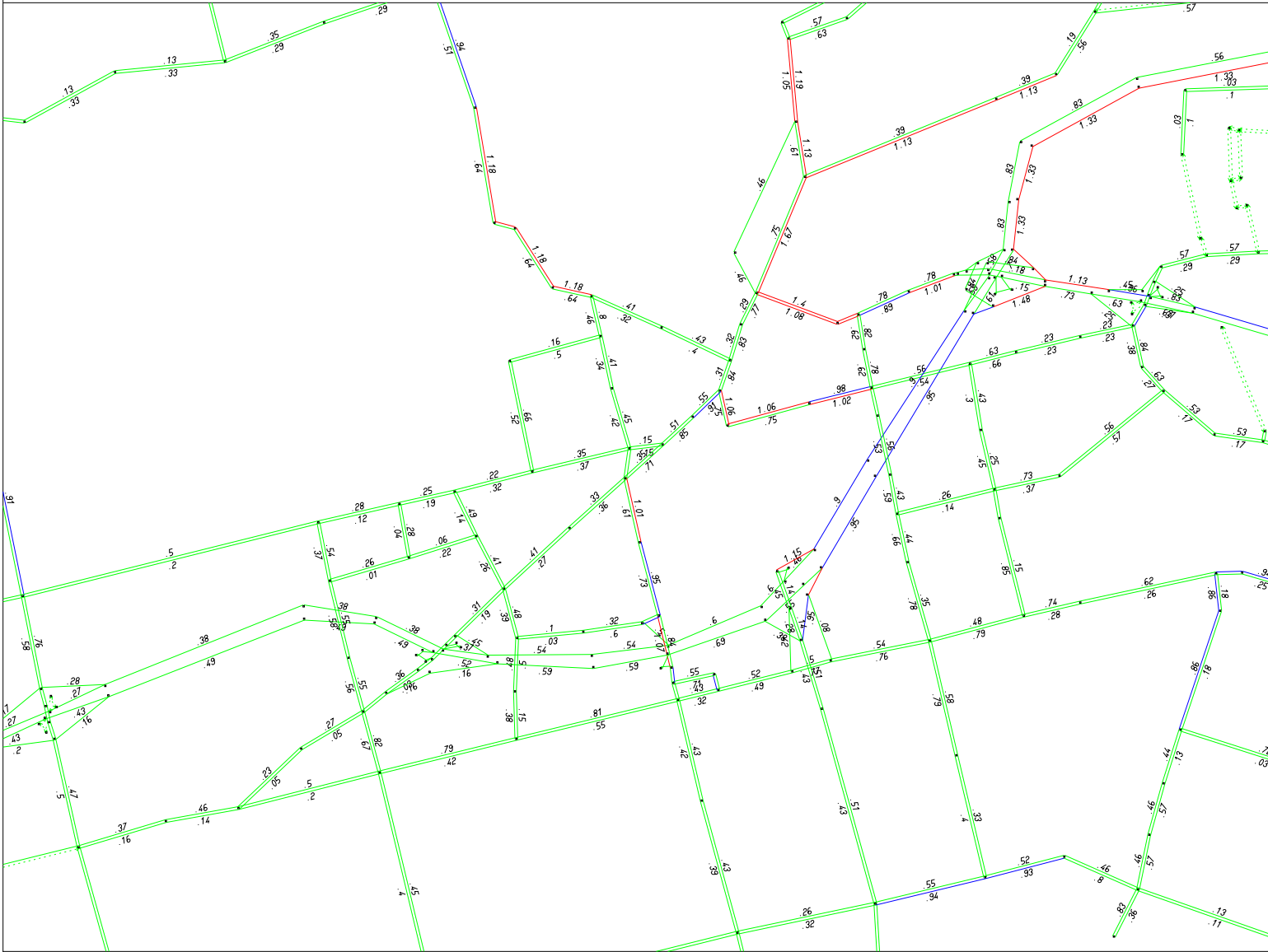
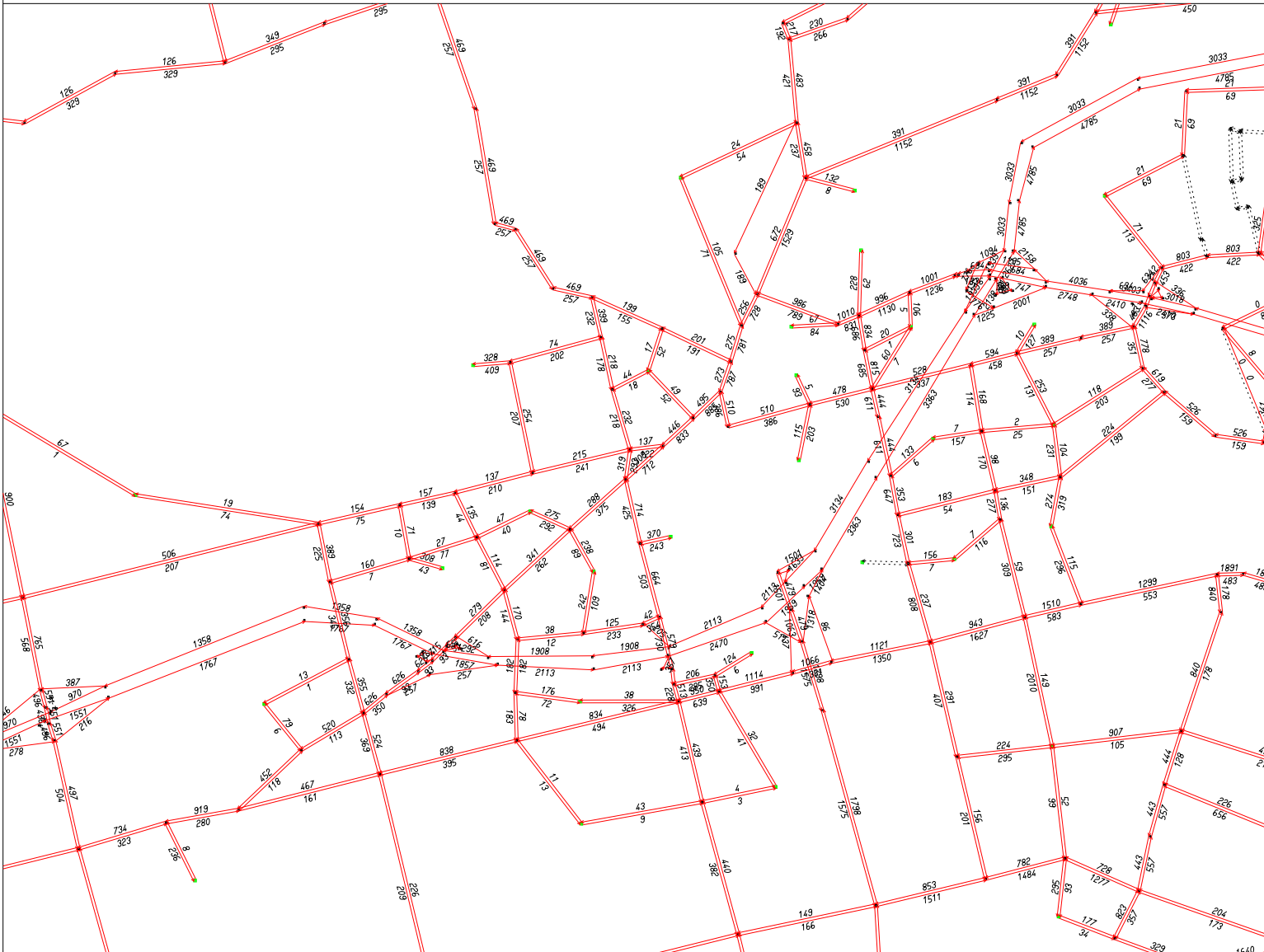


Exhibit 10:
2031
"Do Nothing"
V/C

AUTO VOLUMES

emme/2

Exhibit 11:
2031
HTMP
Improvements
Volumes



10-08-16 08:46
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

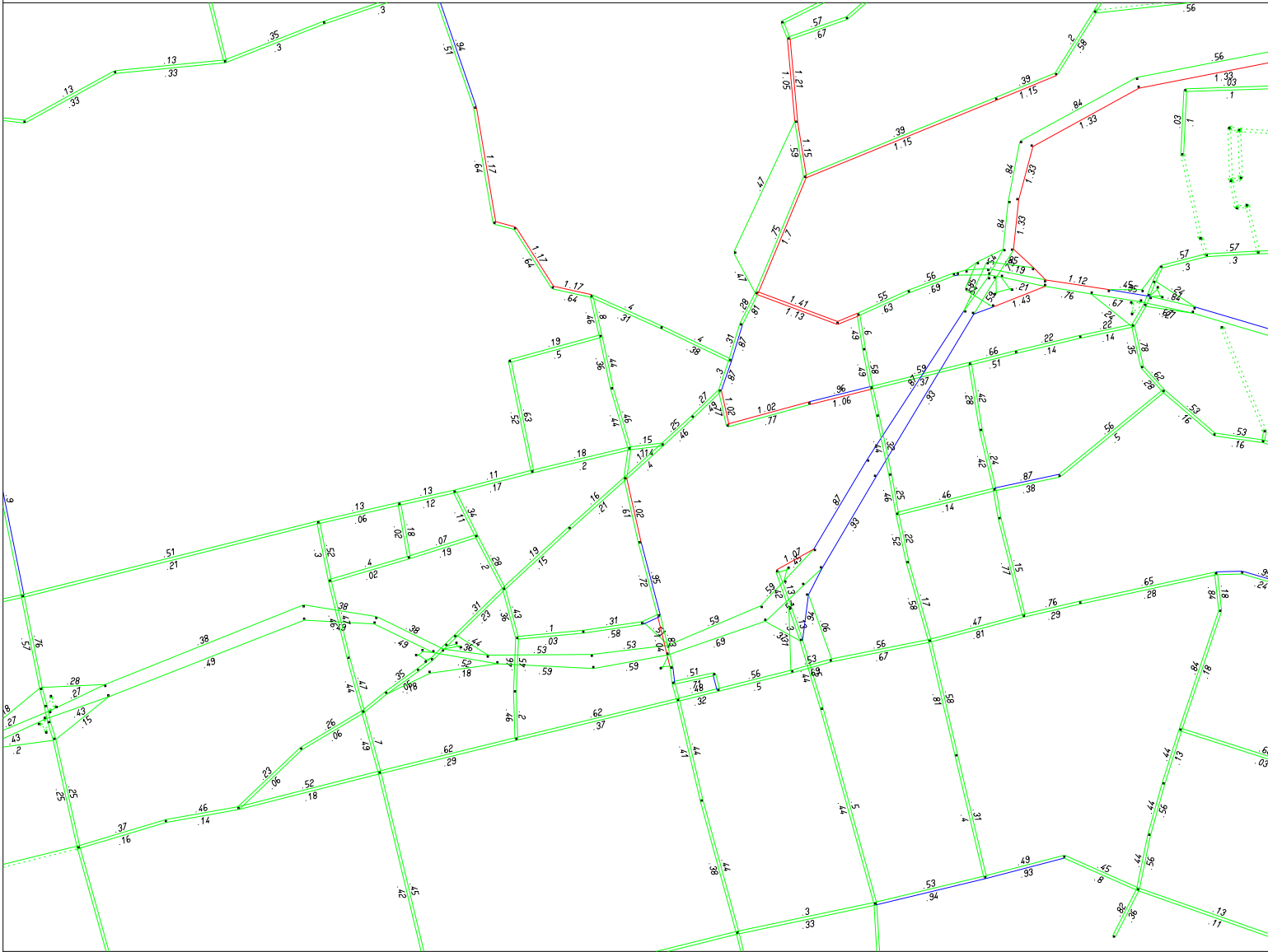


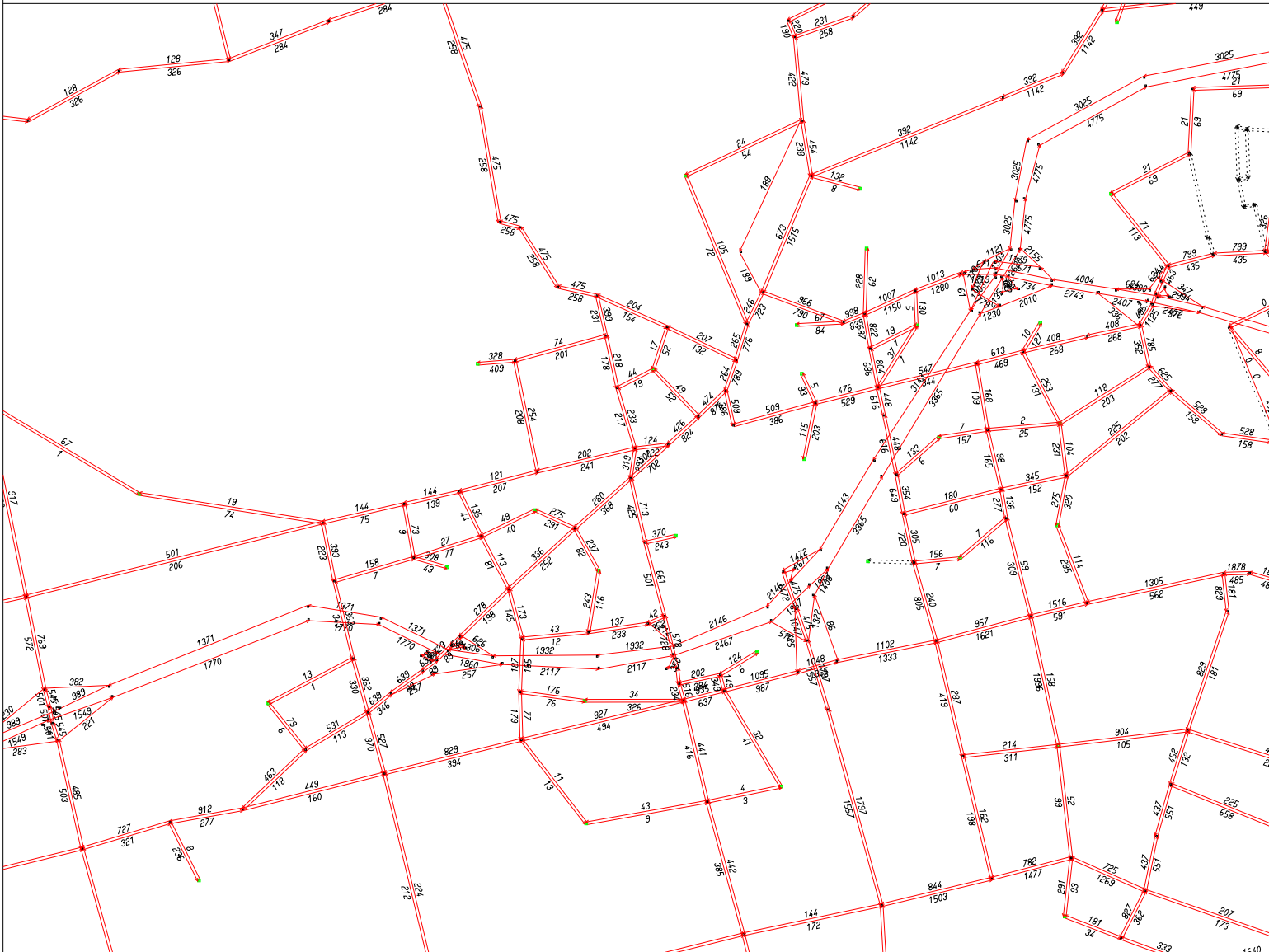
Exhibit 12:
2031
HTMP
Improvements
V/C

10-08-16 08:47
MODULE: 2.13
DMG.UTYU...j.dk

AUTO VOLUMES

emme/2

Exhibit 13:
2031
S2 Volumes

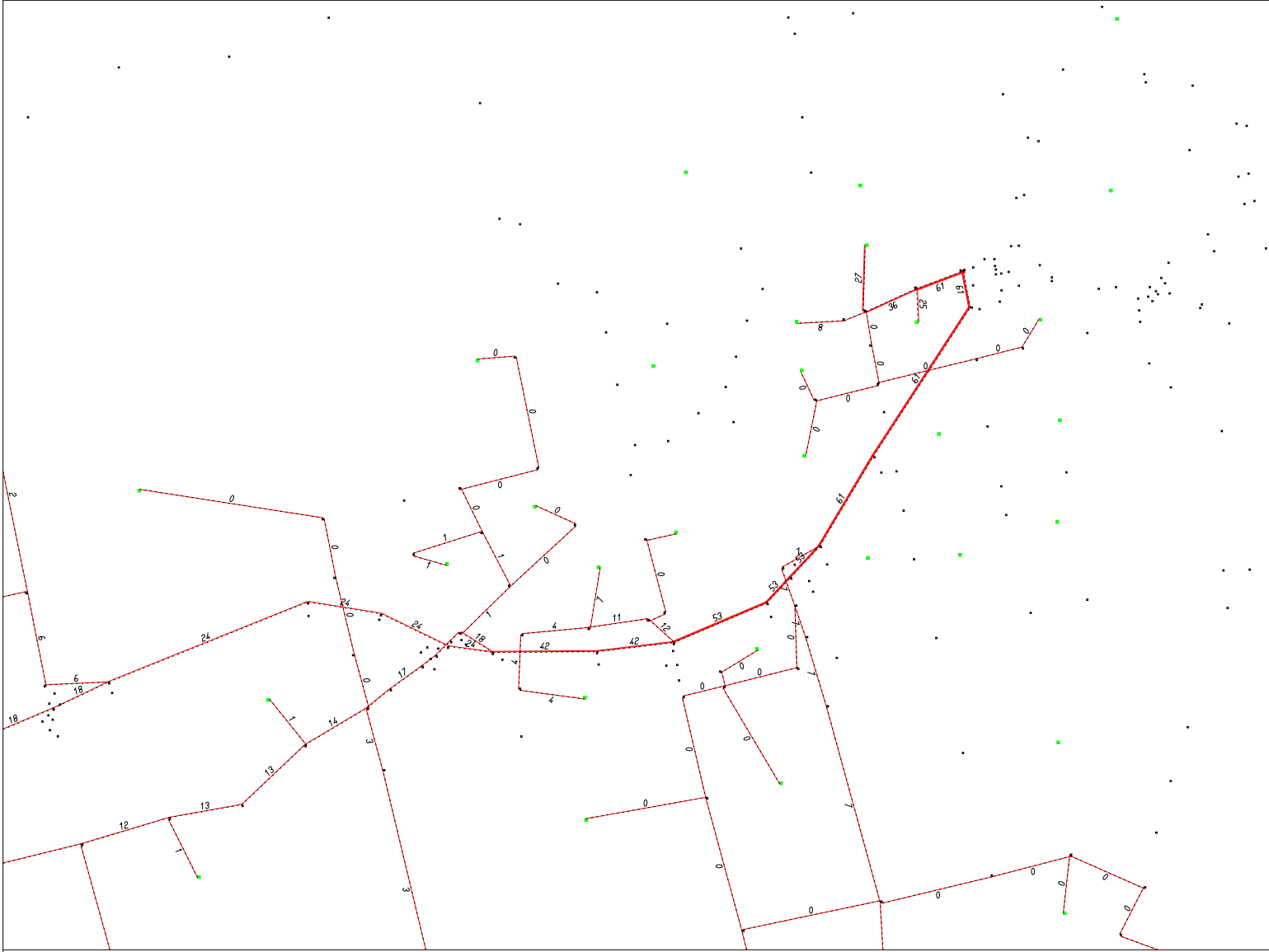


10-08-16 09:18
MODULE: 6.12
DMG.UTYU...j.dk

ADDITIONAL VOLUMES ON AUTO NETWORK

emme/2

Exhibit 14:
2031
S2 Select Link



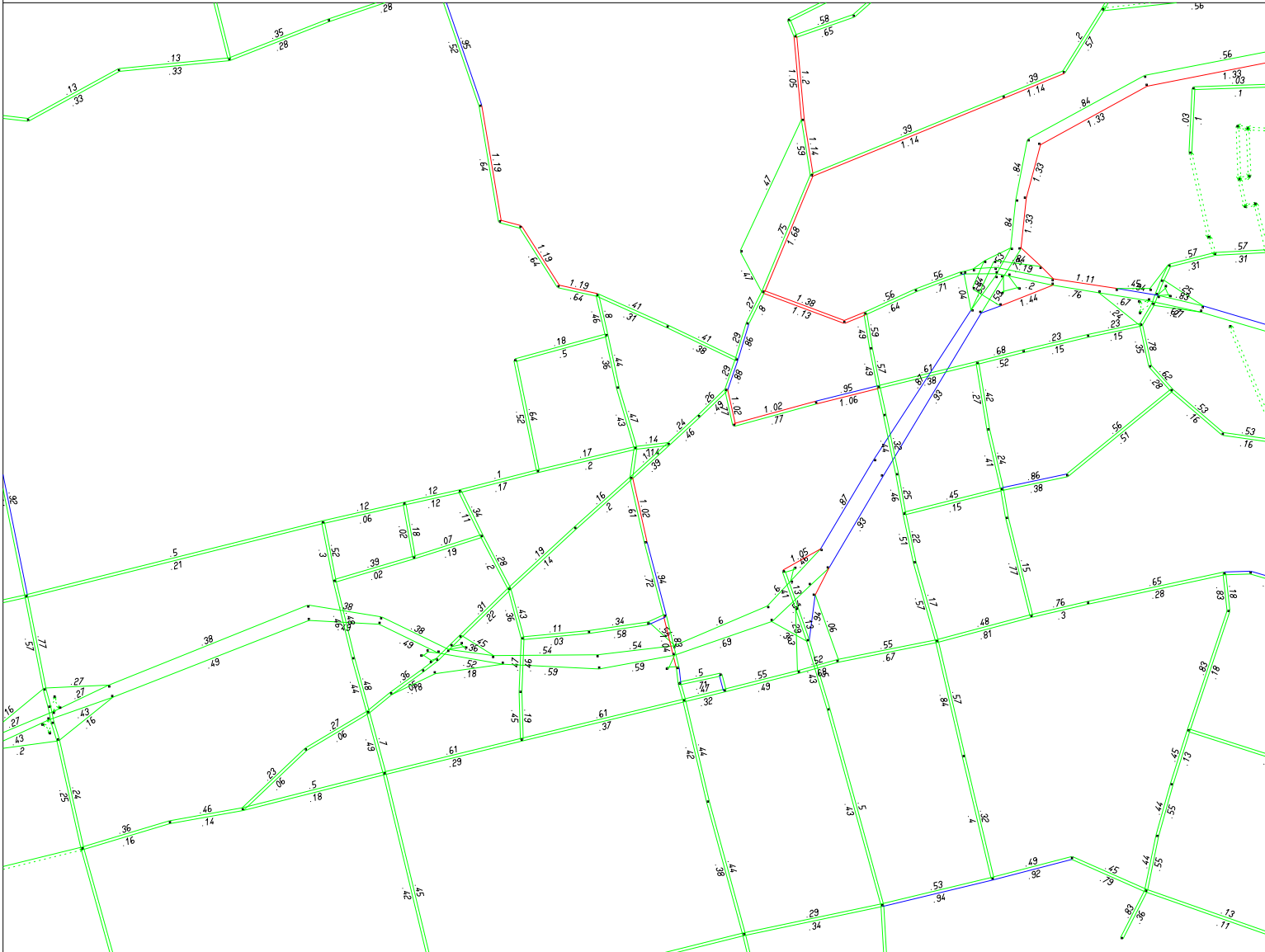
10-08-16 09:20
MODULE: 6.12
DMG.UTYU...jdk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 15:
2031
S2 V/C

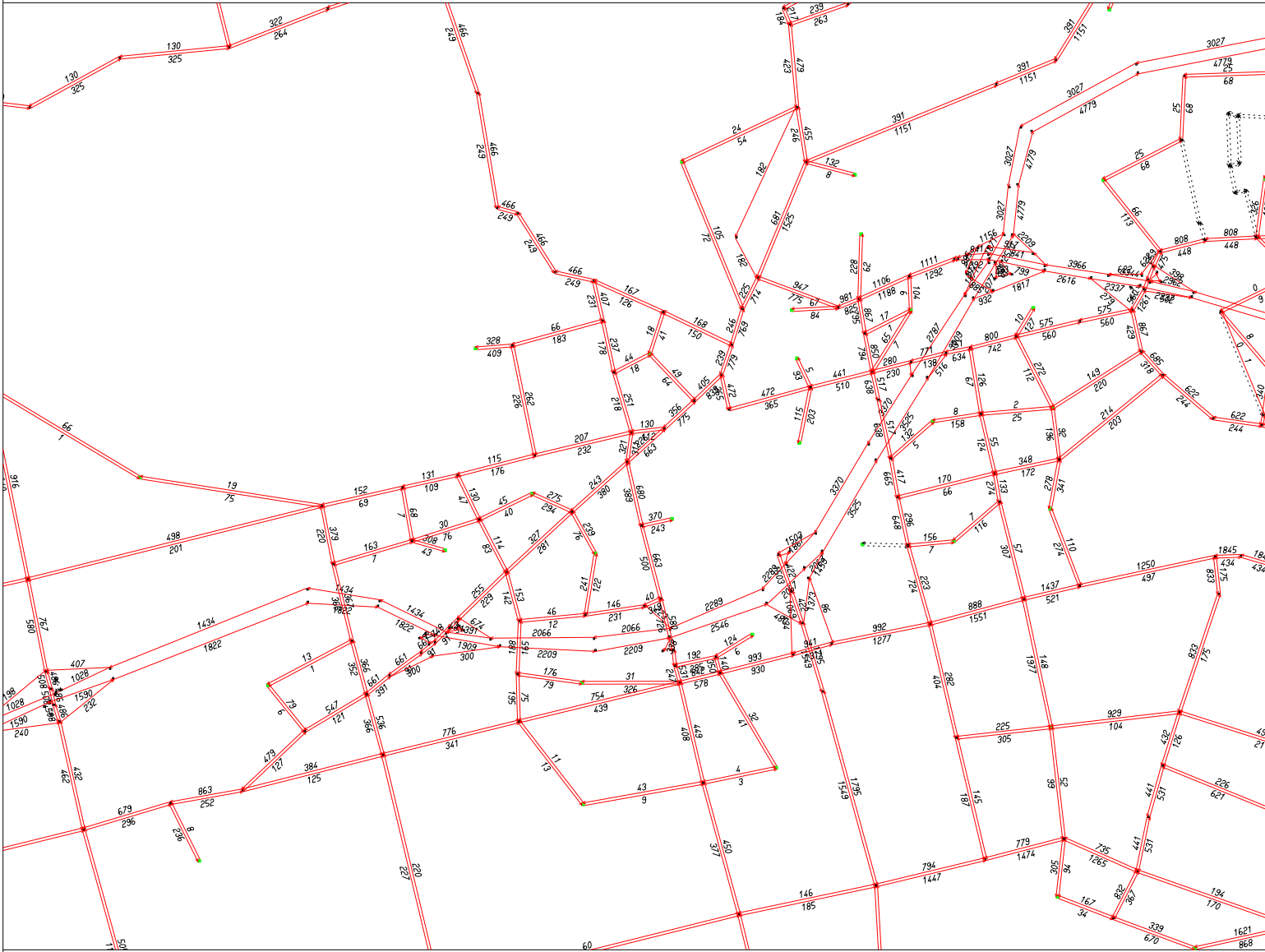


10-08-16 09:21
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 16:
2031
S3 Volumes

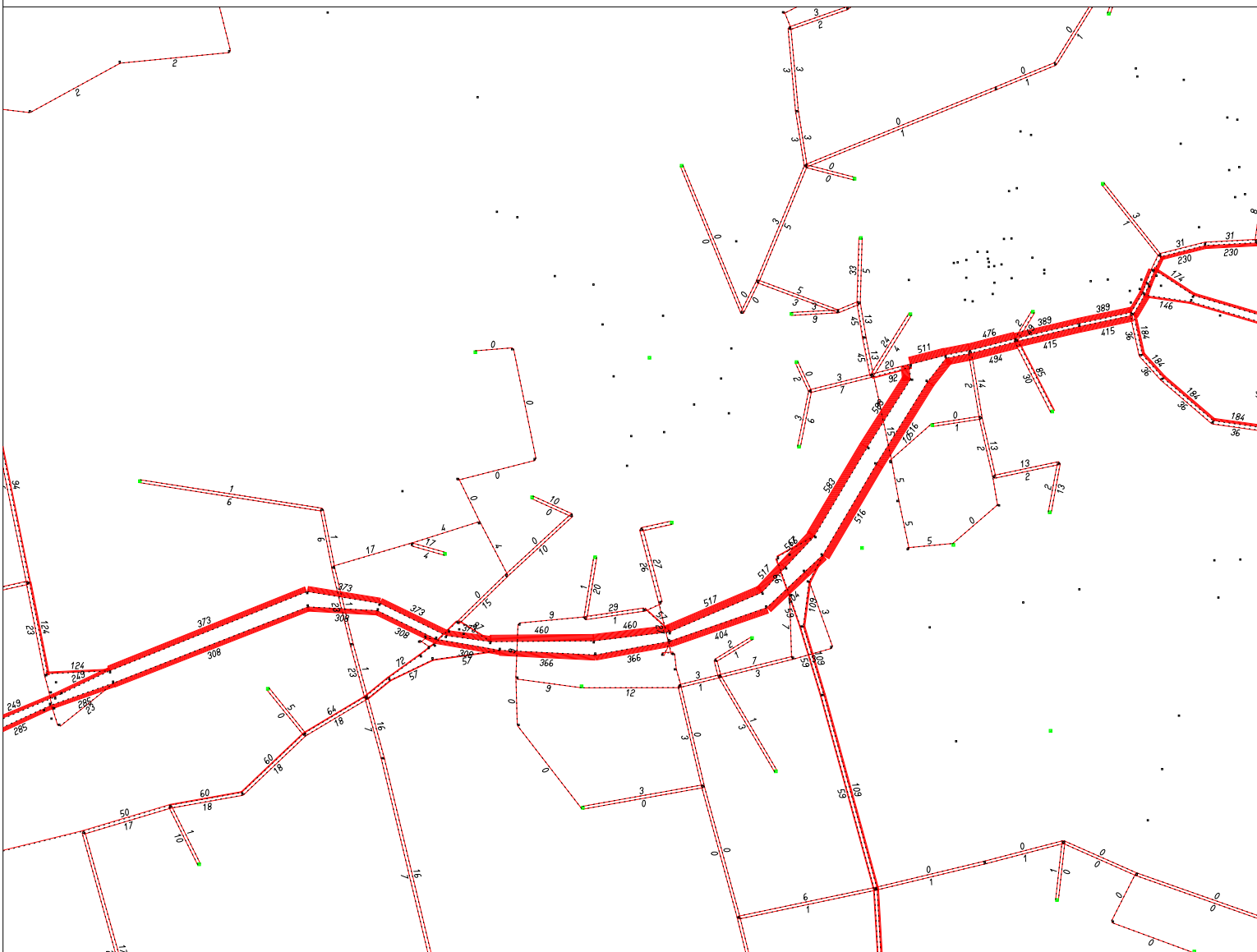


10-08-16 09:45
MODULE: 6.12
DMG.UTYU...j.dk

ADDITIONAL VOLUMES ON AUTO NETWORK

emme/2

Exhibit 17:
2031
S3 Select Link



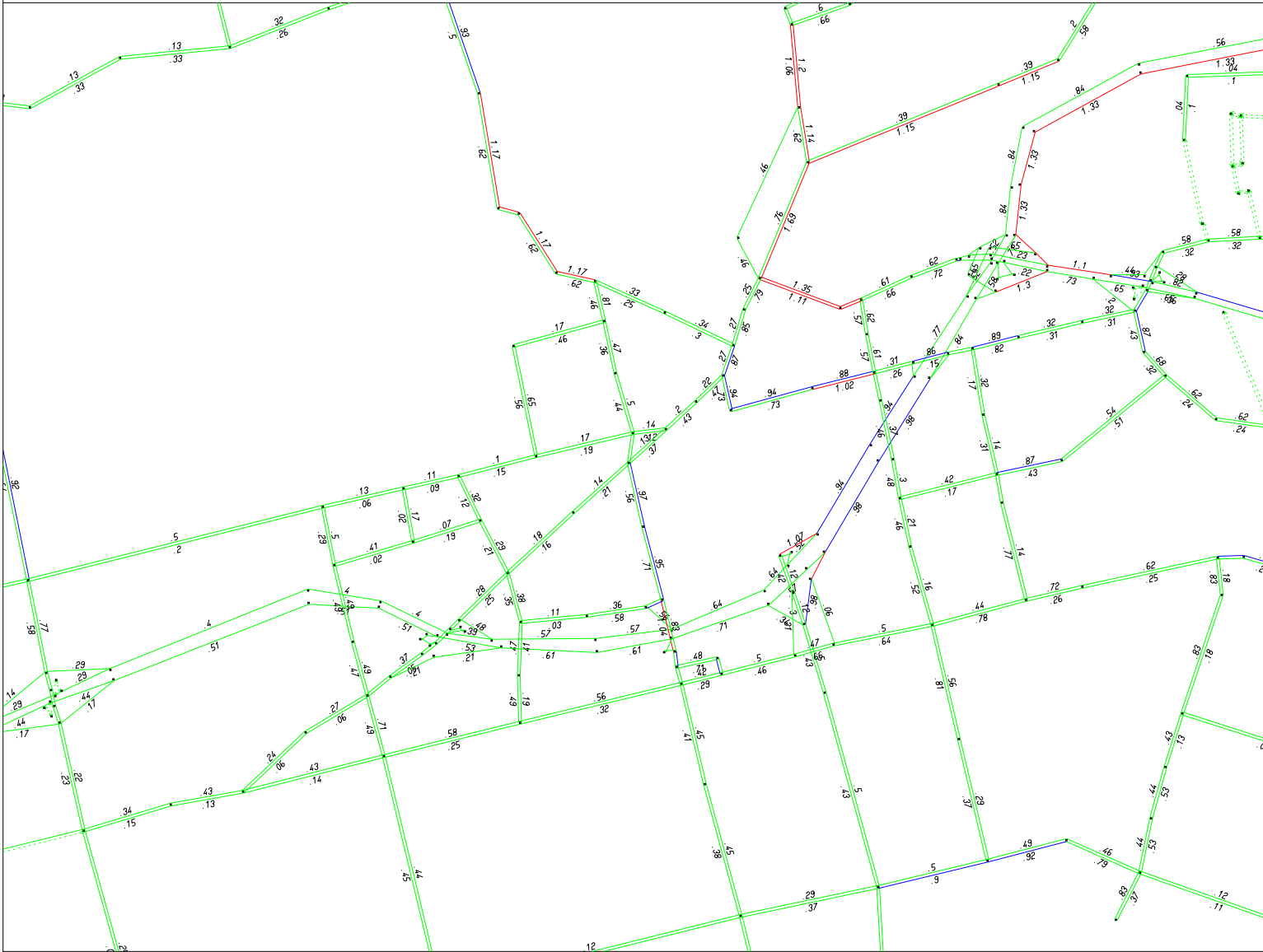
10-08-16 09:47
MODULE: 6.12
DMG.UTYU...jdk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 18:
2031
S3 V/C

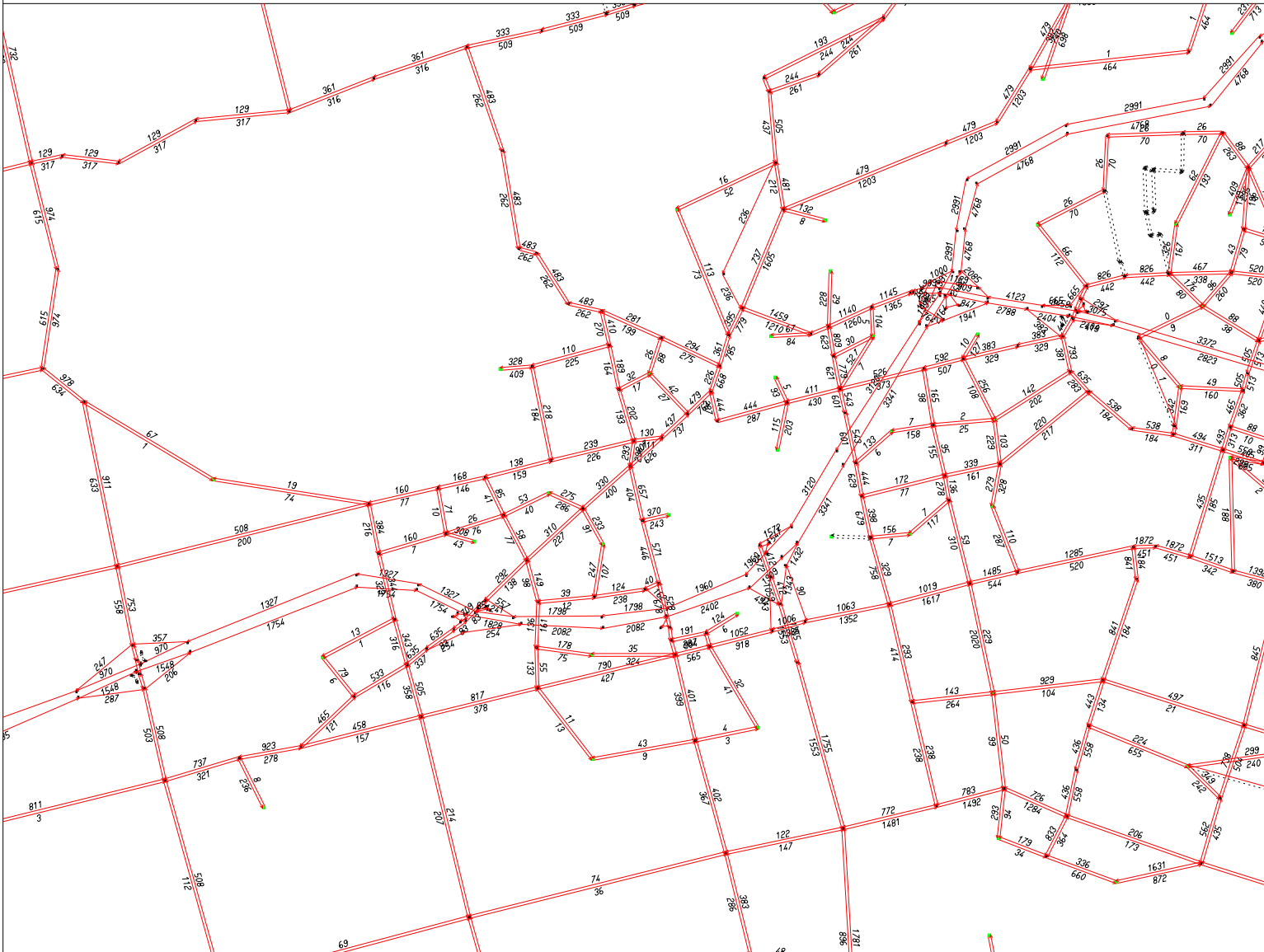


10-08-16 09:47
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 19:
2031
S4 Volumes

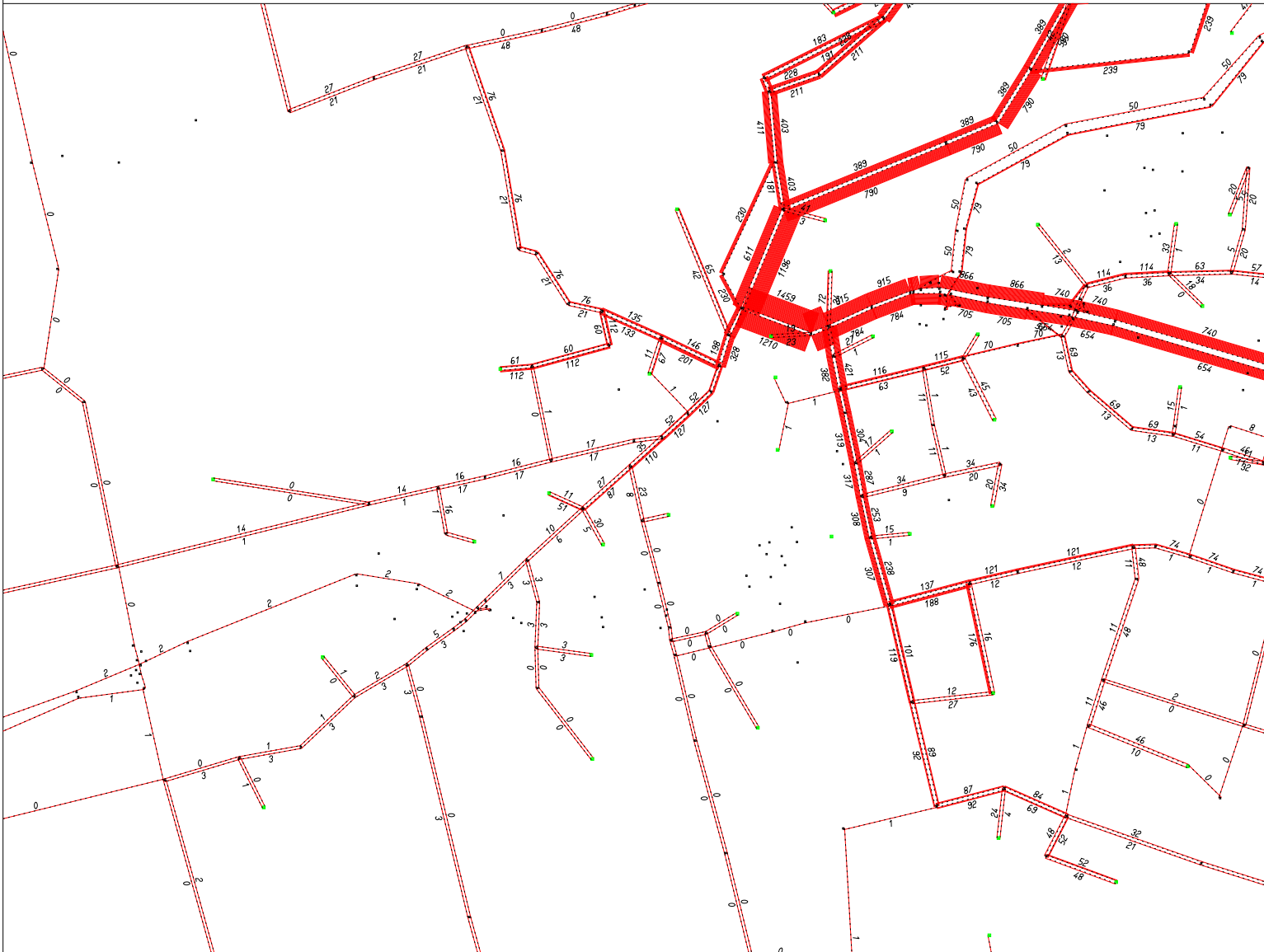


10-08-16 10:09
MODULE: 6.12
DMG.UTYU...jdk

ADDITIONAL VOLUMES ON AUTO NETWORK

emme/2

Exhibit 20:
2031
S4 Select Link



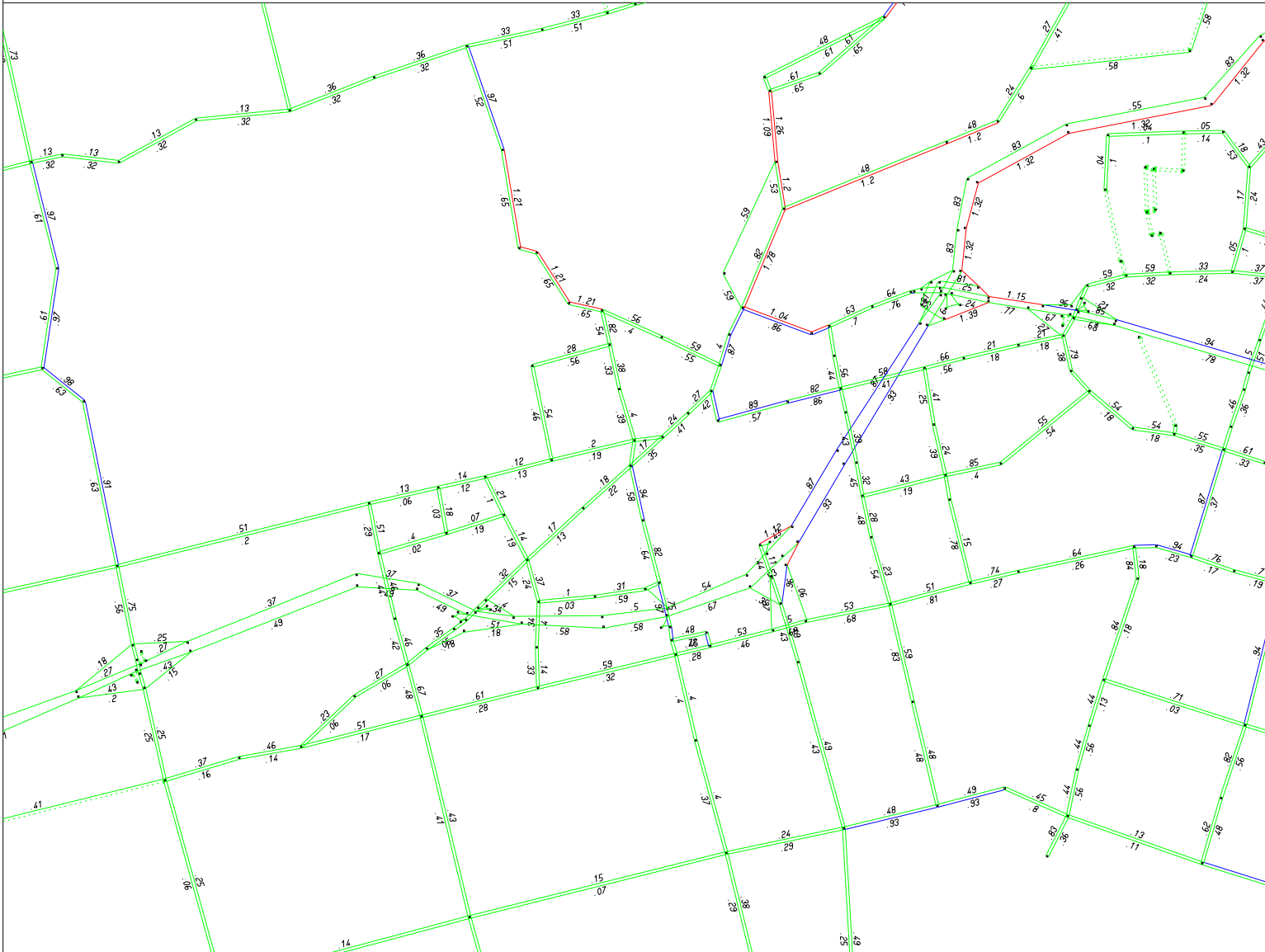
10-08-16 10:10
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 21:
2031
S4 V/C

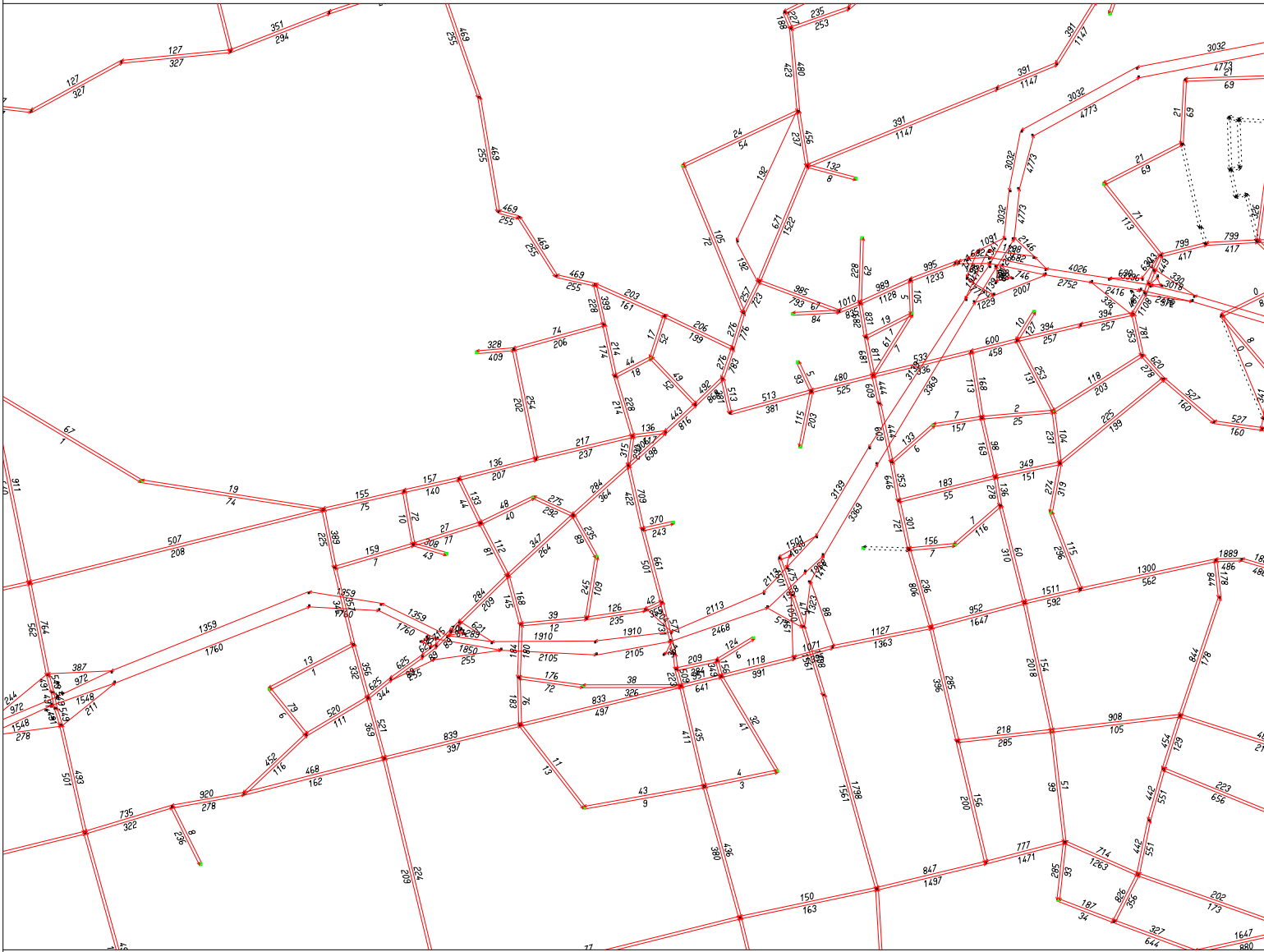


10-08-16 10:10
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 22:
2031
S5 Volumes



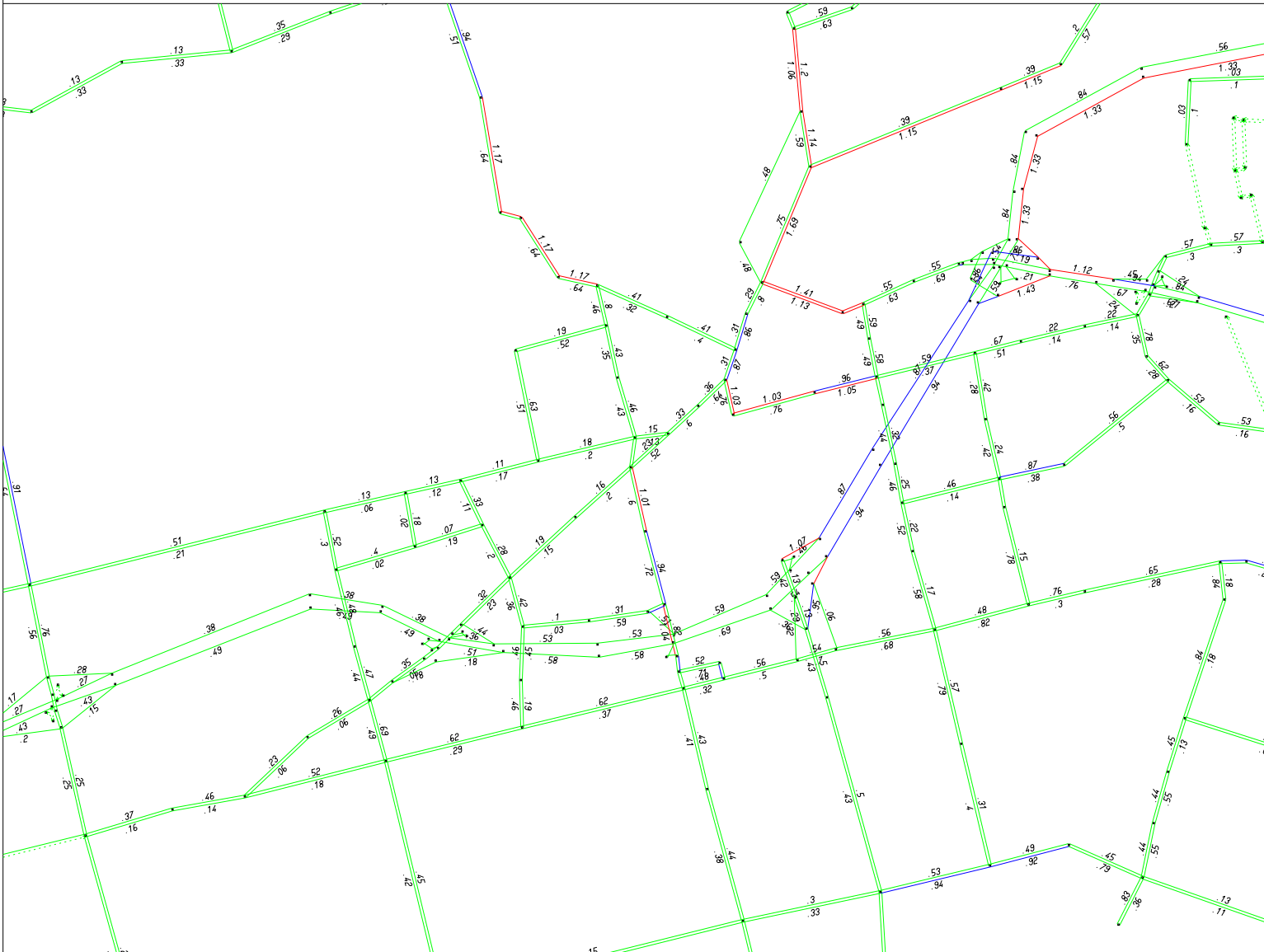
10-08-16 10:32
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme2

Exhibit 23:
2031
S5 V/C

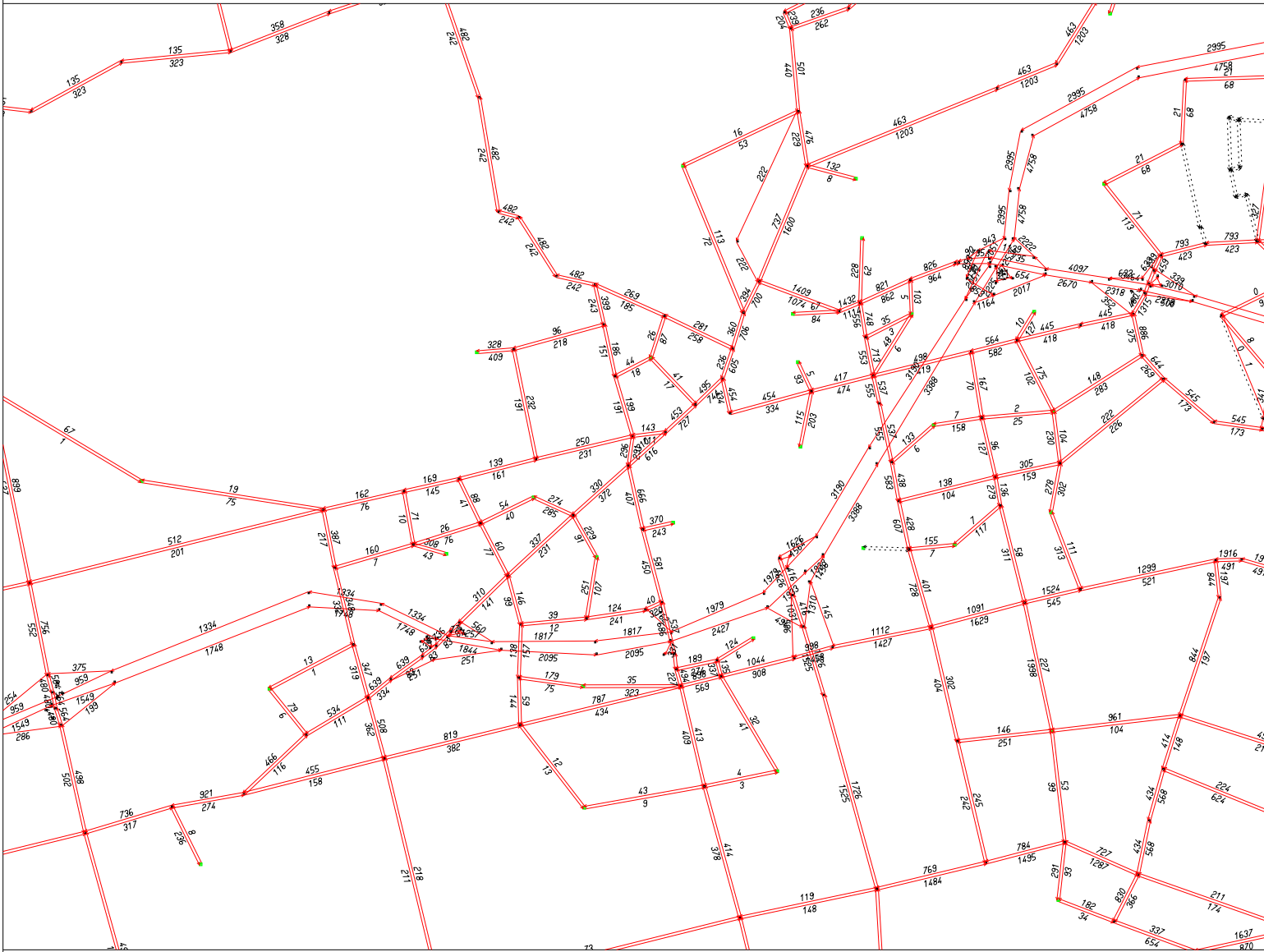


10-08-16 10:33
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 24:
2031
S6 Volumes



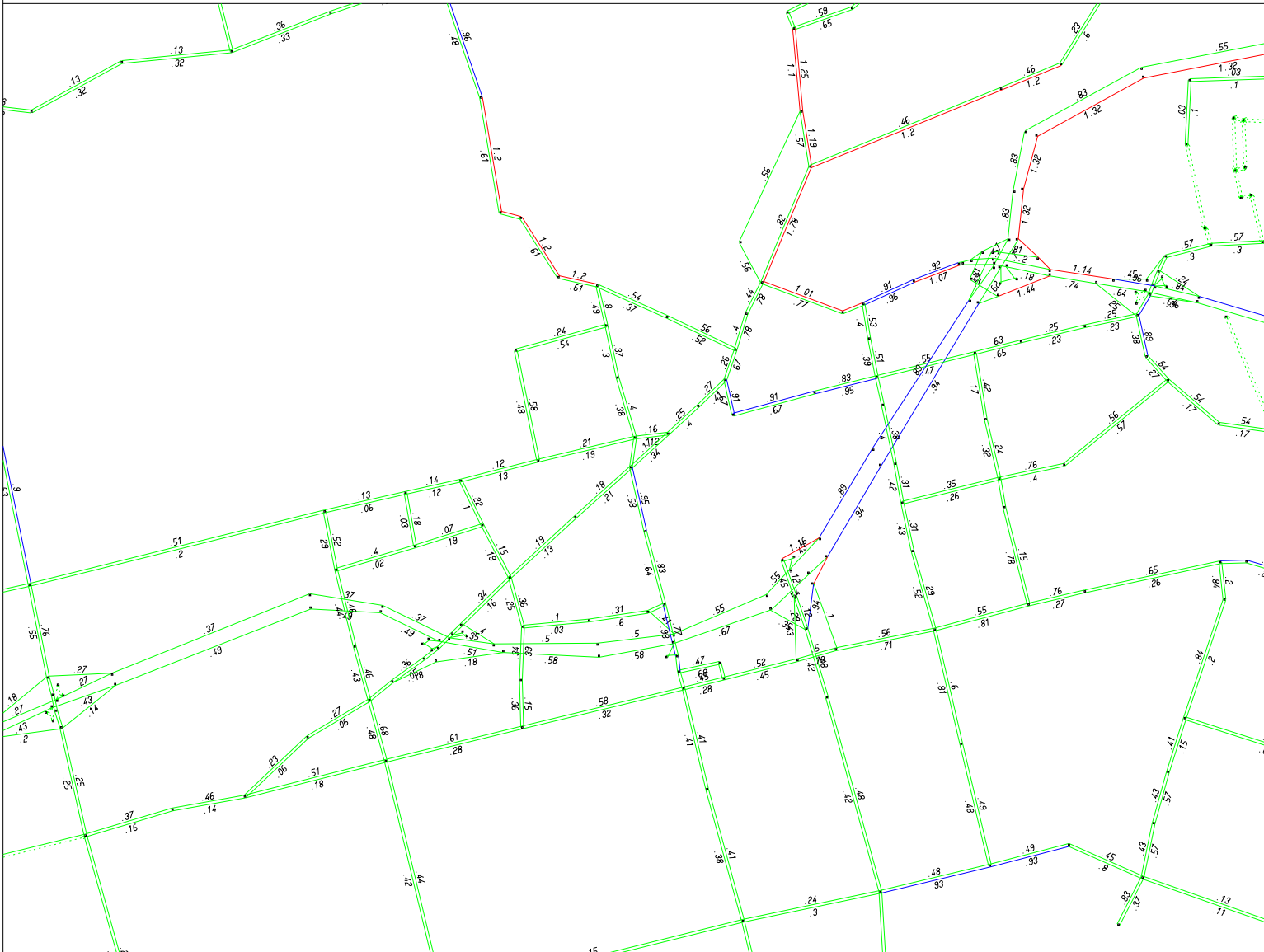
10-08-16 10:48
MODULE: 6.12
DMG.UTYU...jdx

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 25:
2031
S6 V/C

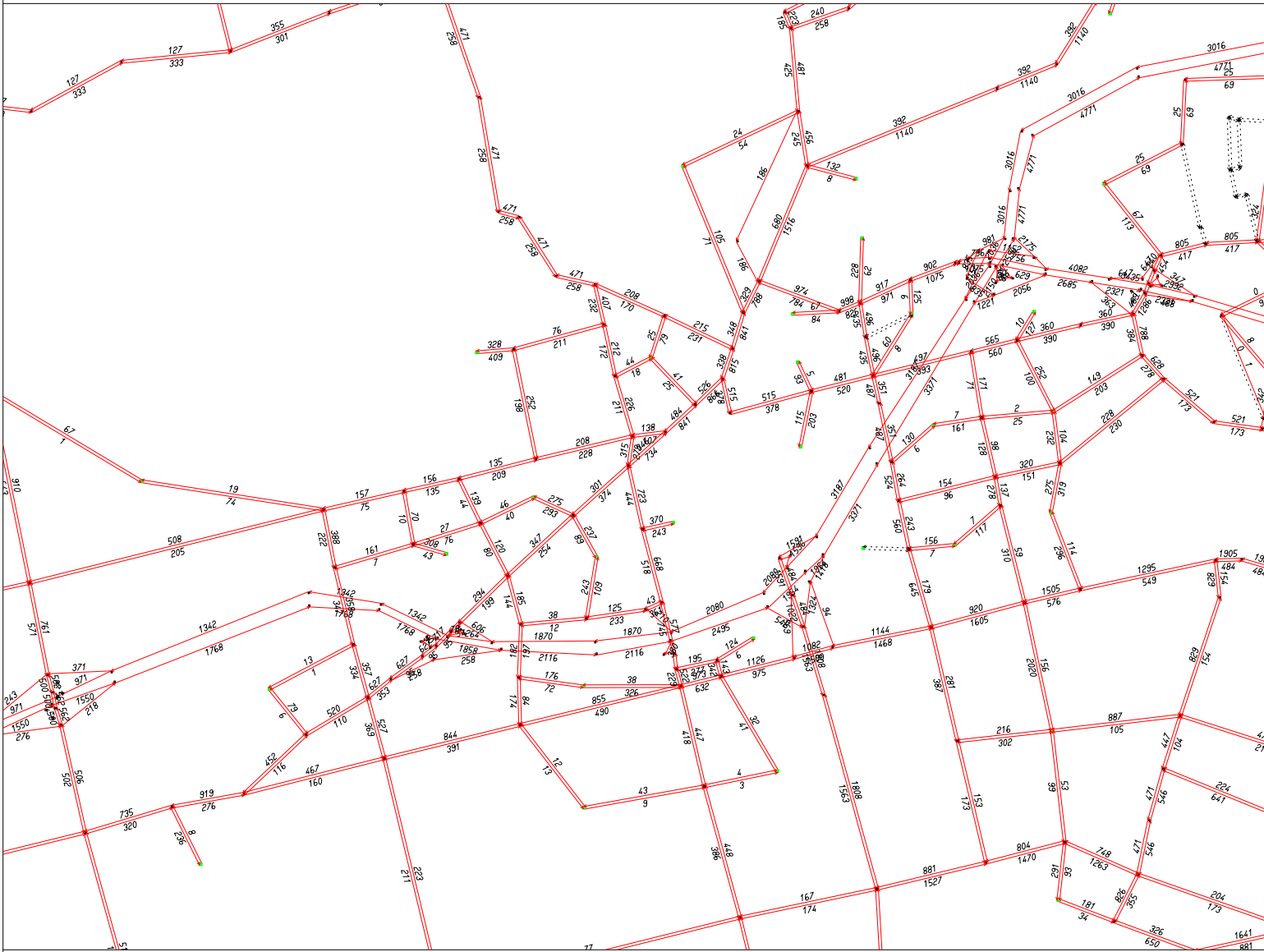


10-08-16 10:49
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 26:
2031
S7 Volumes



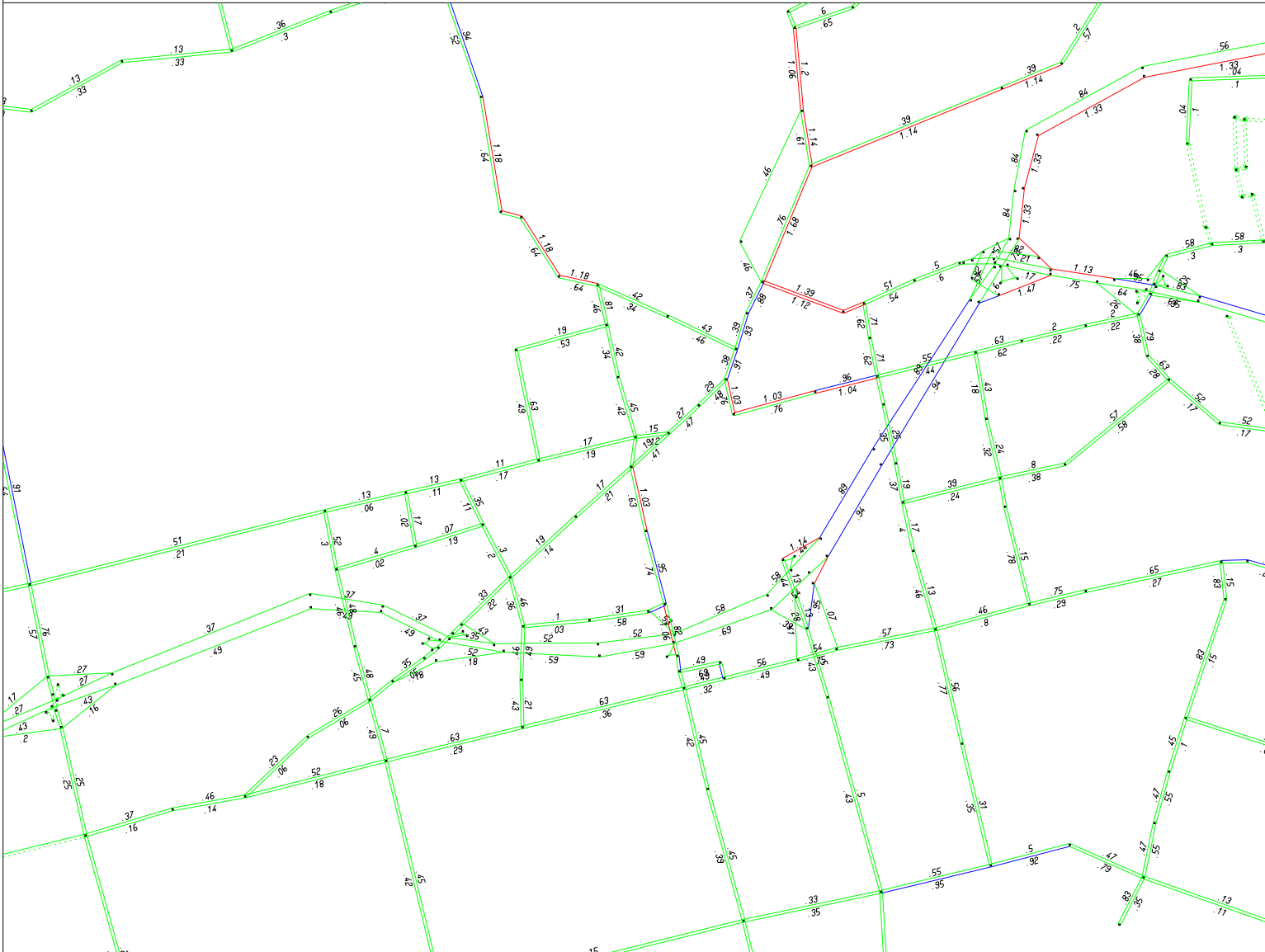
10-08-16 11:37
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 27:
2031
S7 VIC

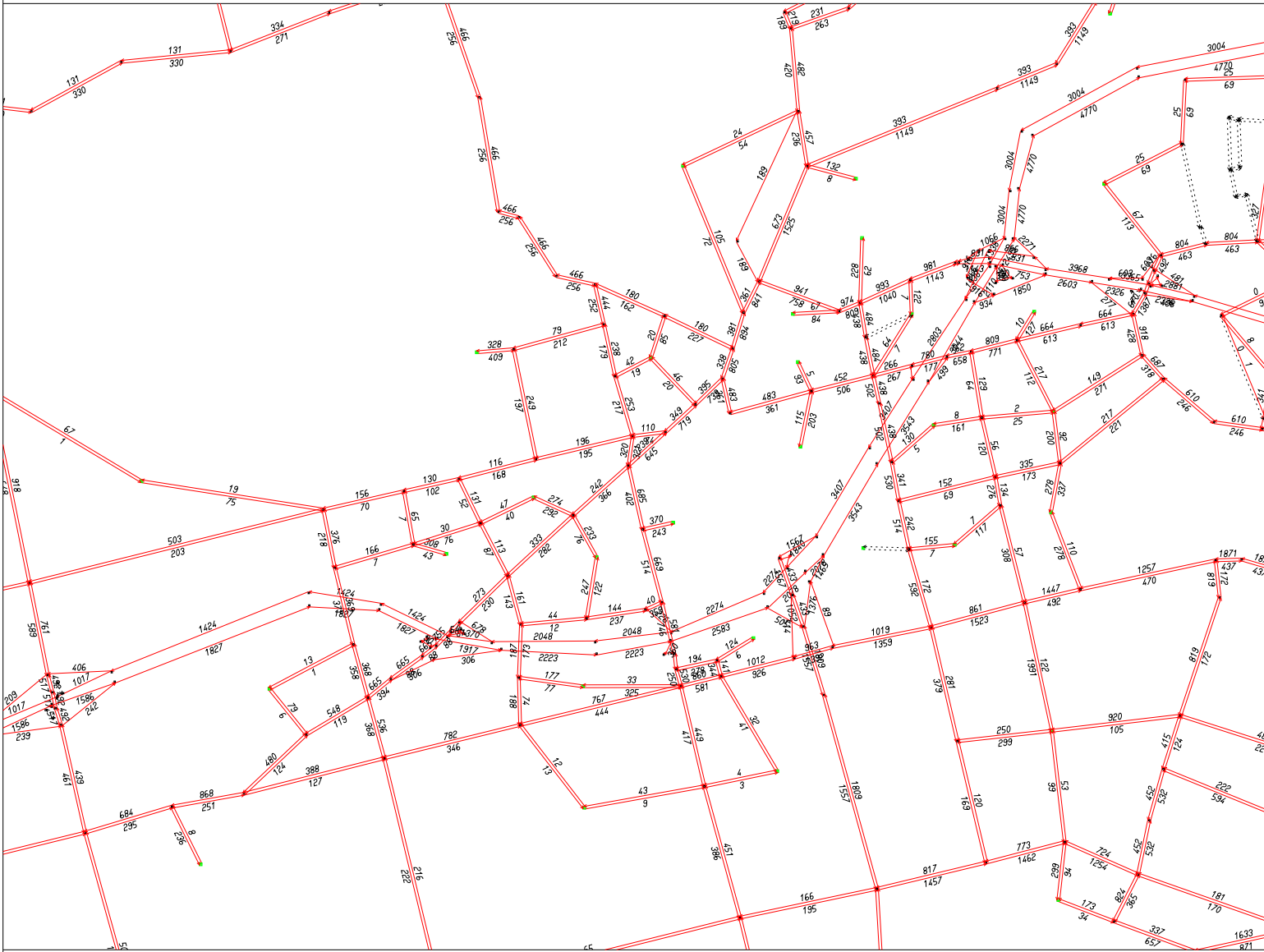


10-08-16 11:38
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 28:
2031
S8 Volumes

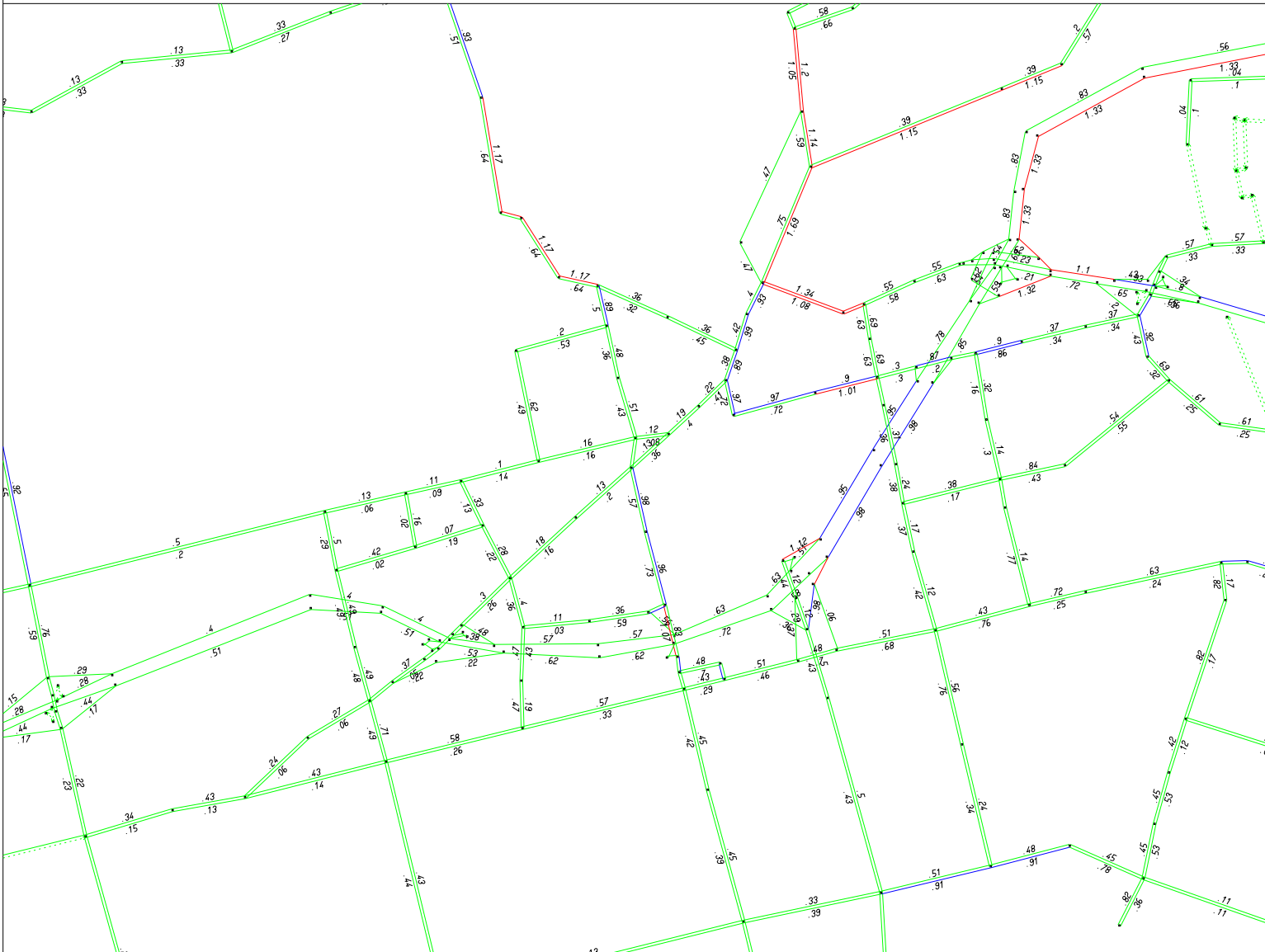


BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 29:
2031
S8 V/C

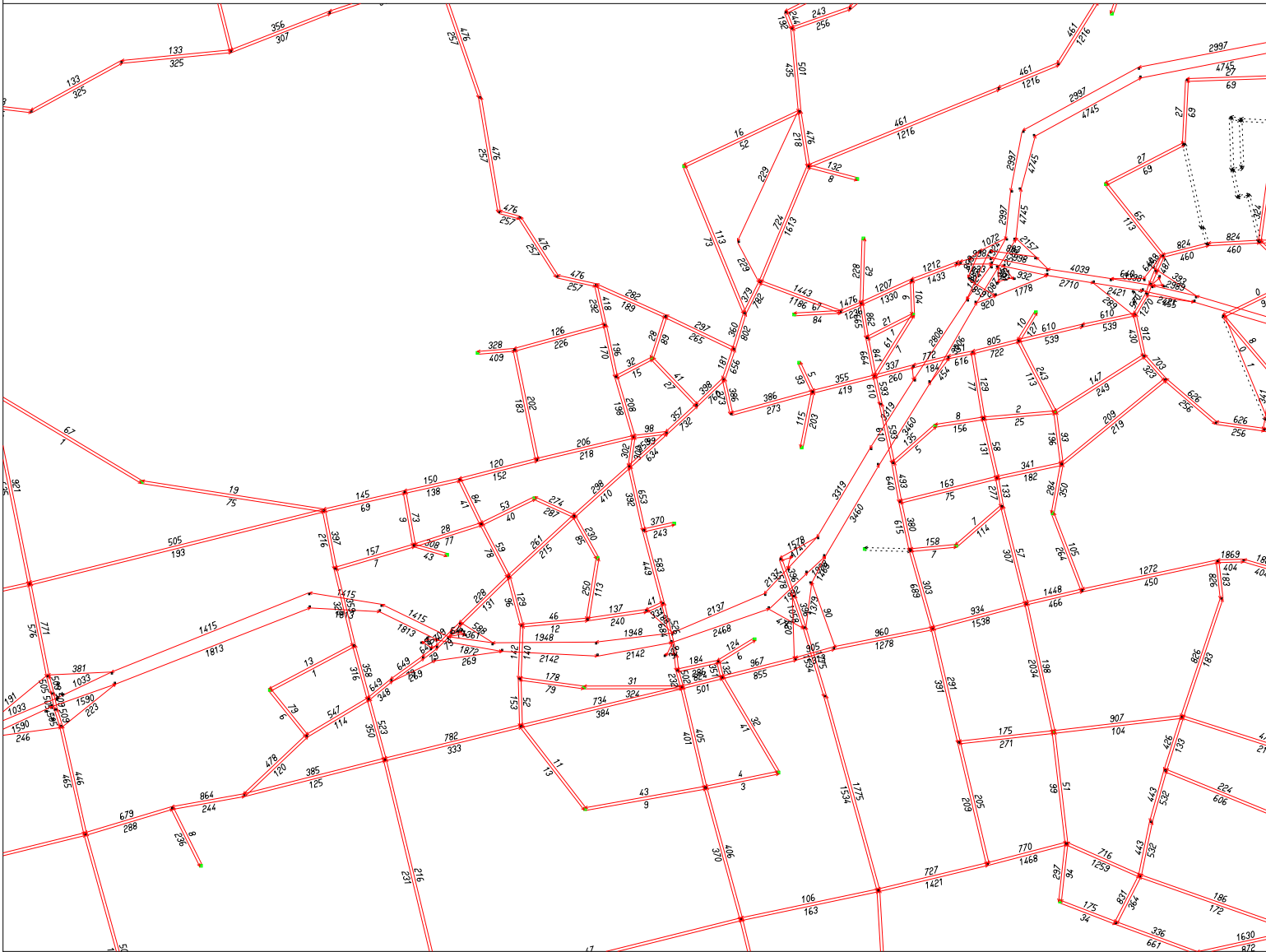


10-08-16 11:50
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 30:
2031
S9 Volumes



10-08-16 13:03
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

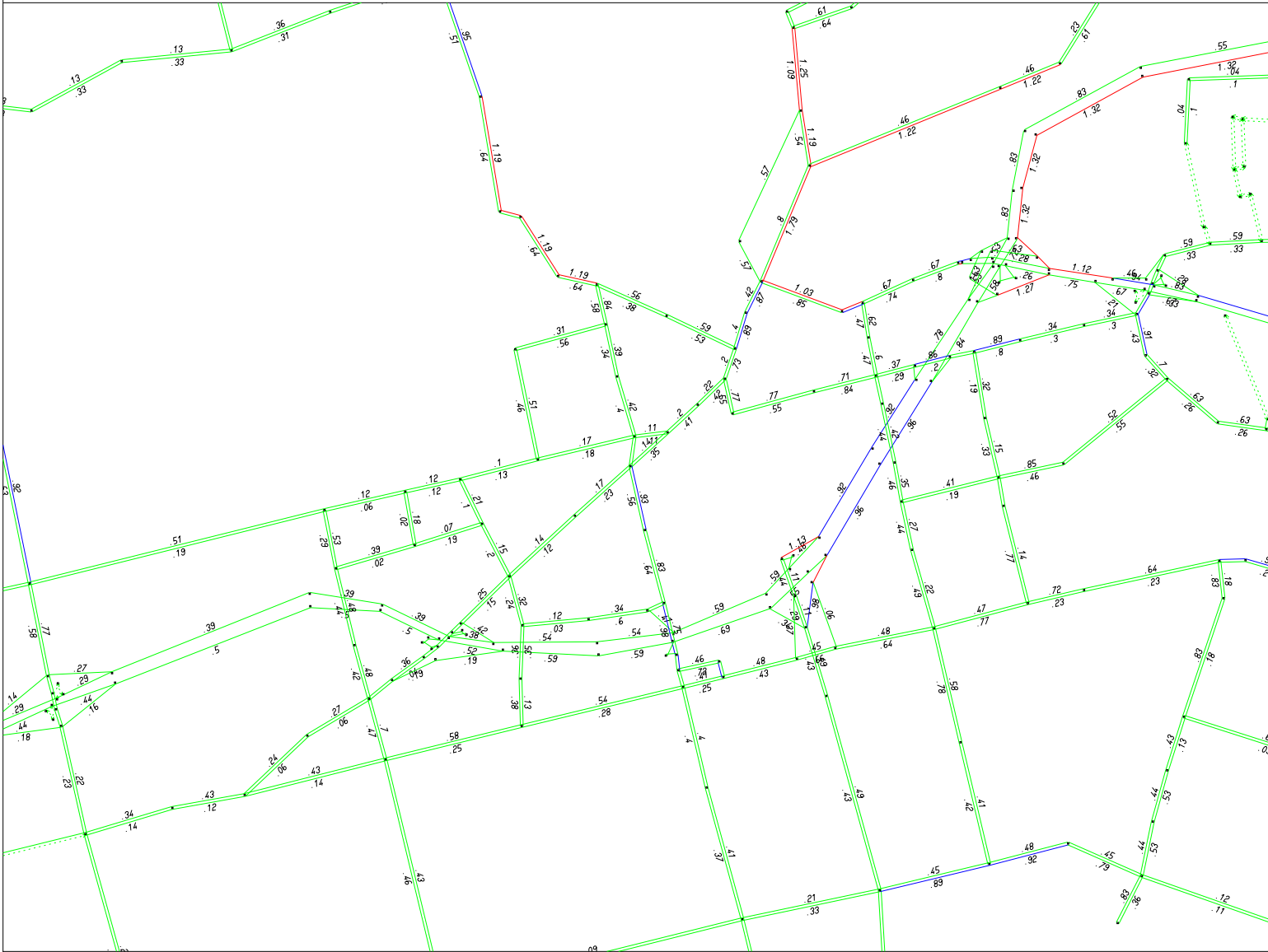


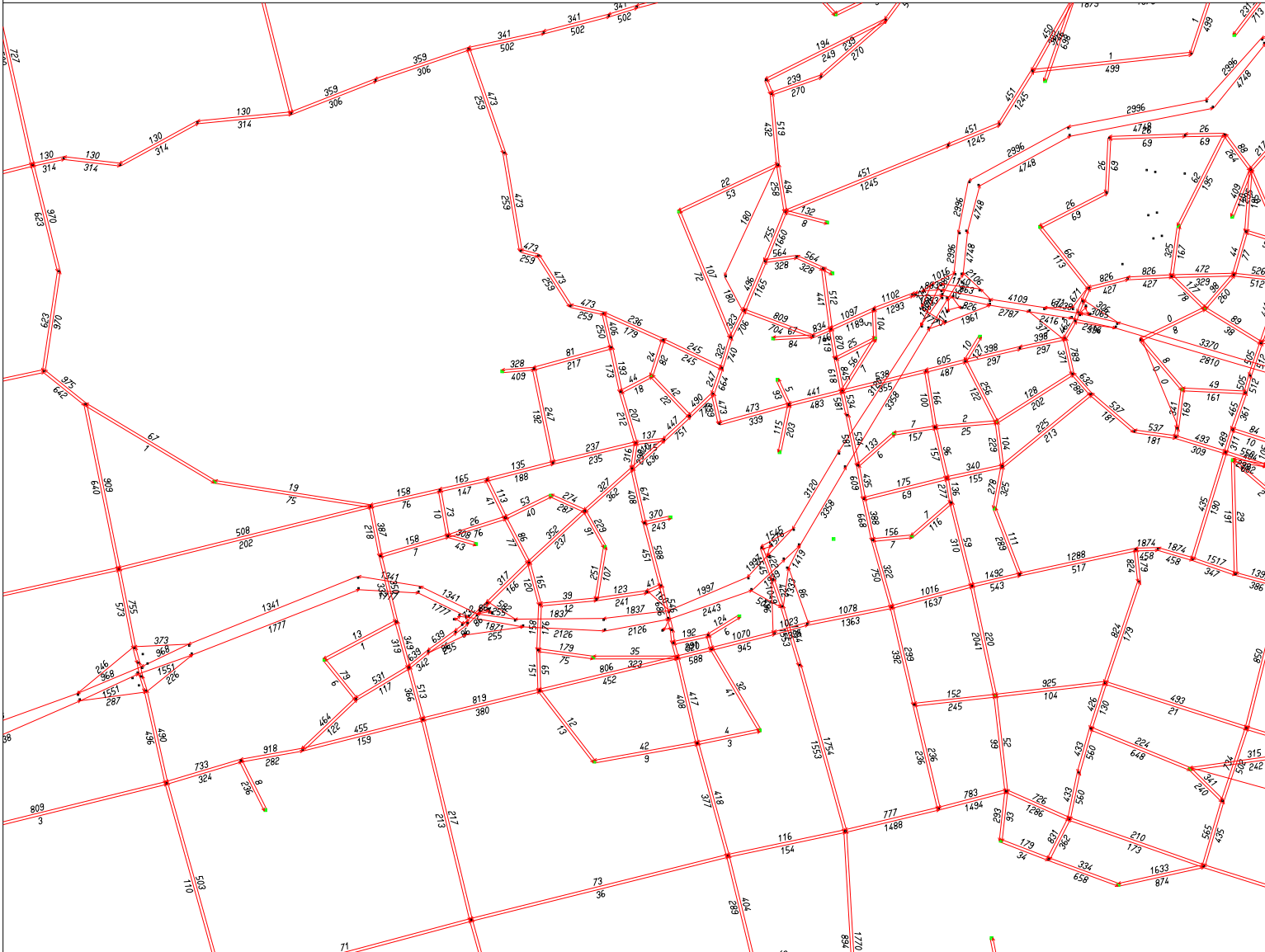
Exhibit 31:
2031
S9 V/C

10-08-16 13:03
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

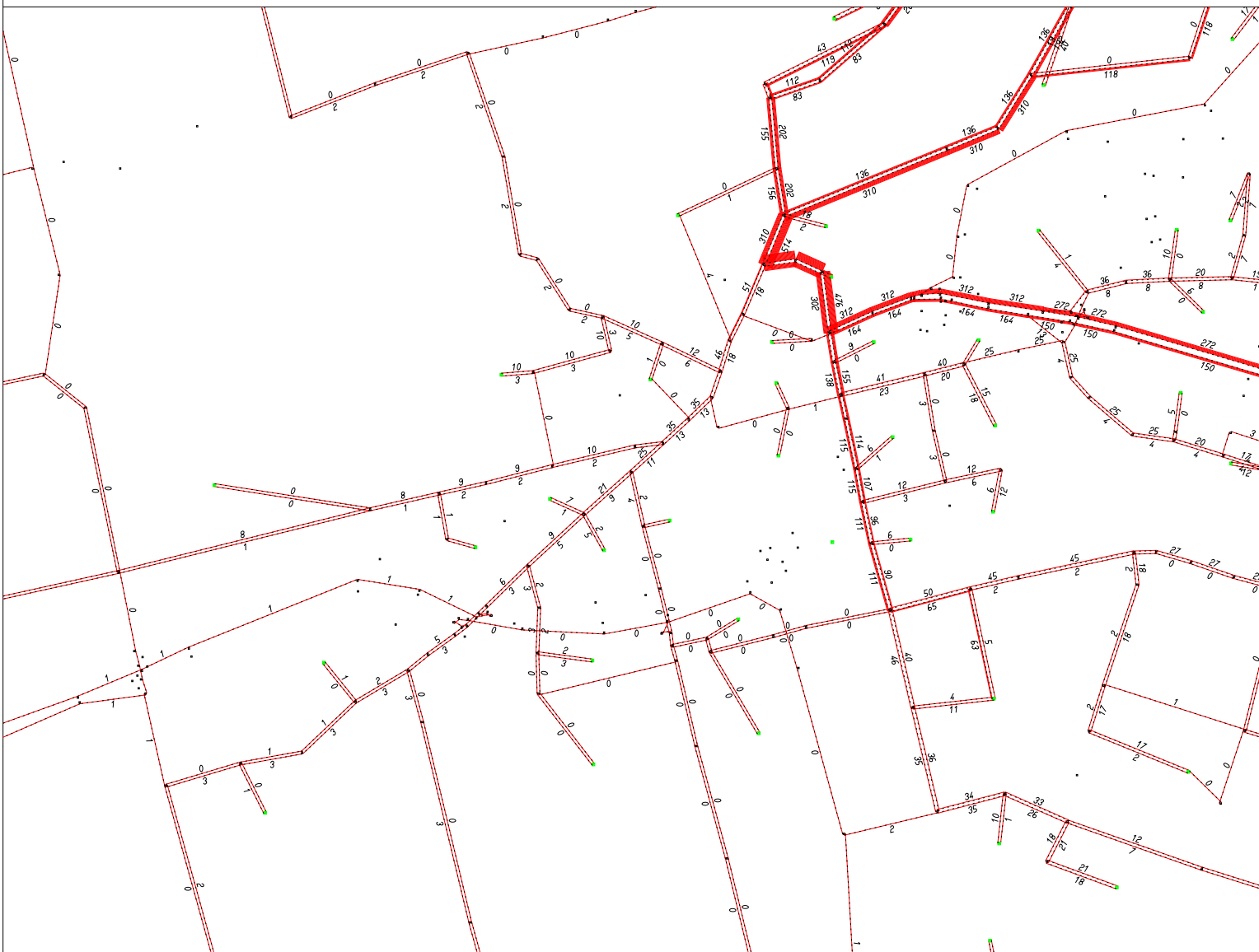
Exhibit 32: 2031 S10 Volumes



ADDITIONAL VOLUMES ON AUTO NETWORK

emme/2

Exhibit 33:
2031
S10 Select Link



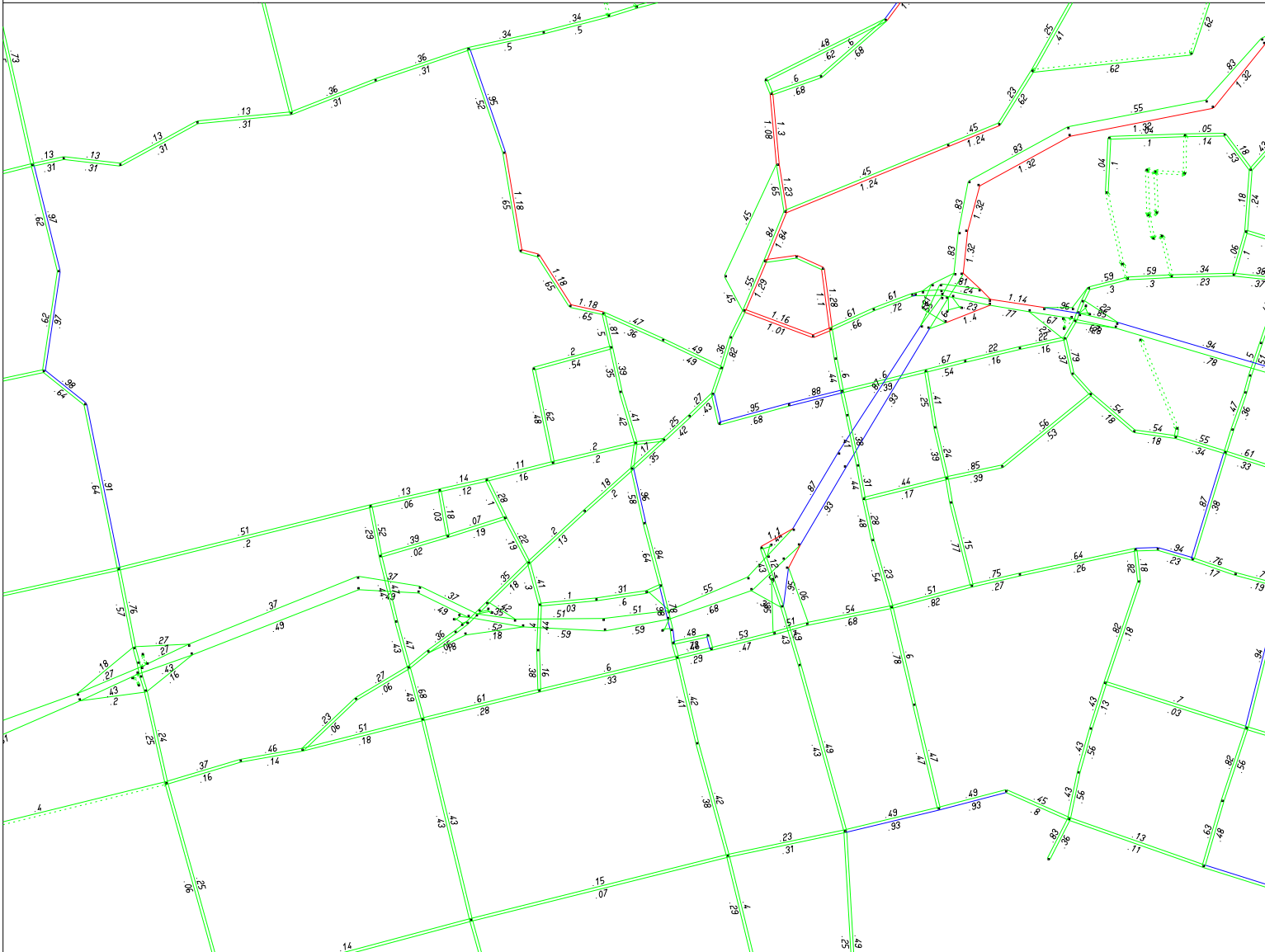
10-08-16 13:19
MODULE: 6.12
DMG.UTYU...jdk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 34:
2031
S10 V/C

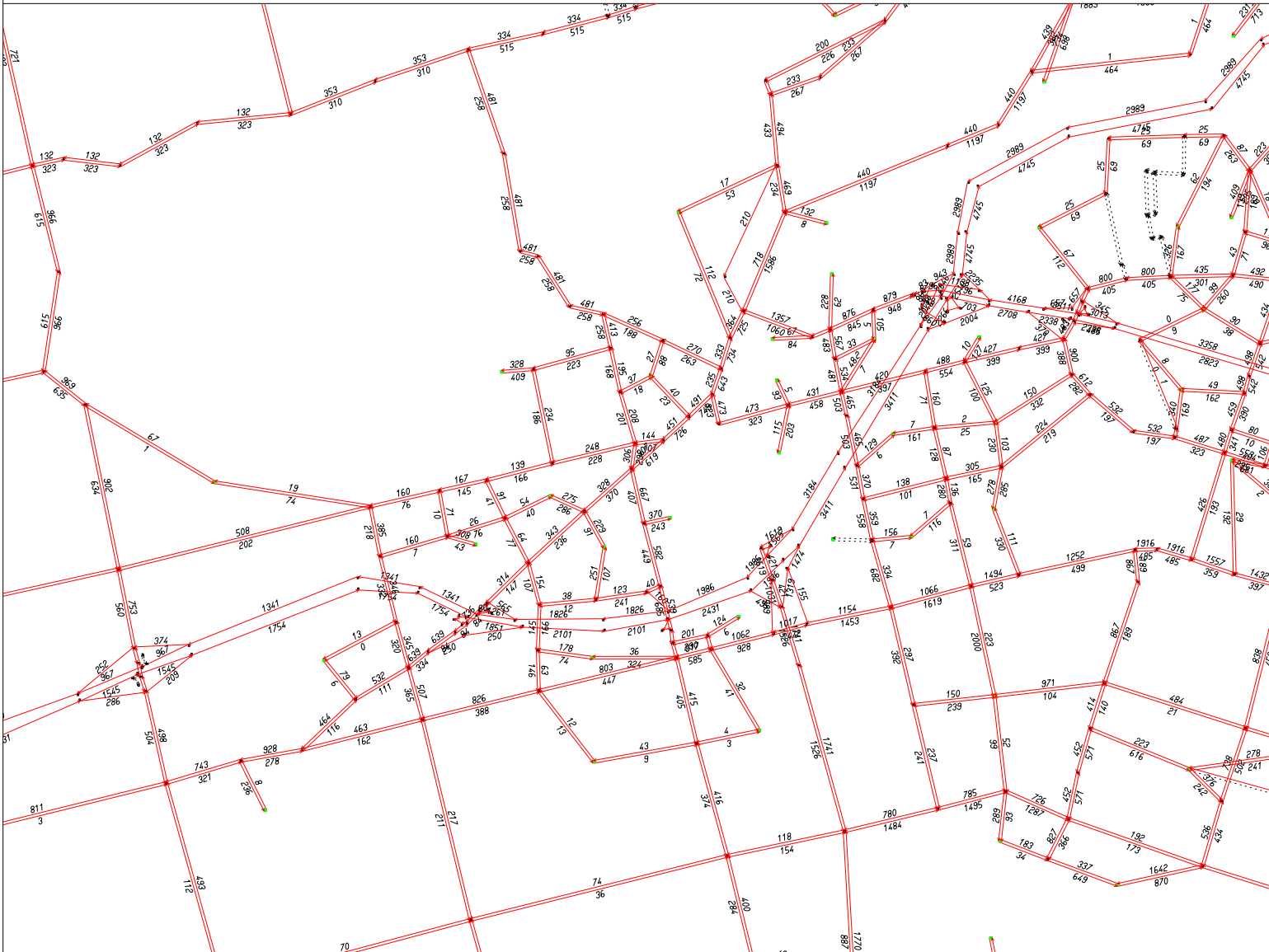


10-08-16 13:19
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 35:
2031
S11 Volumes



BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

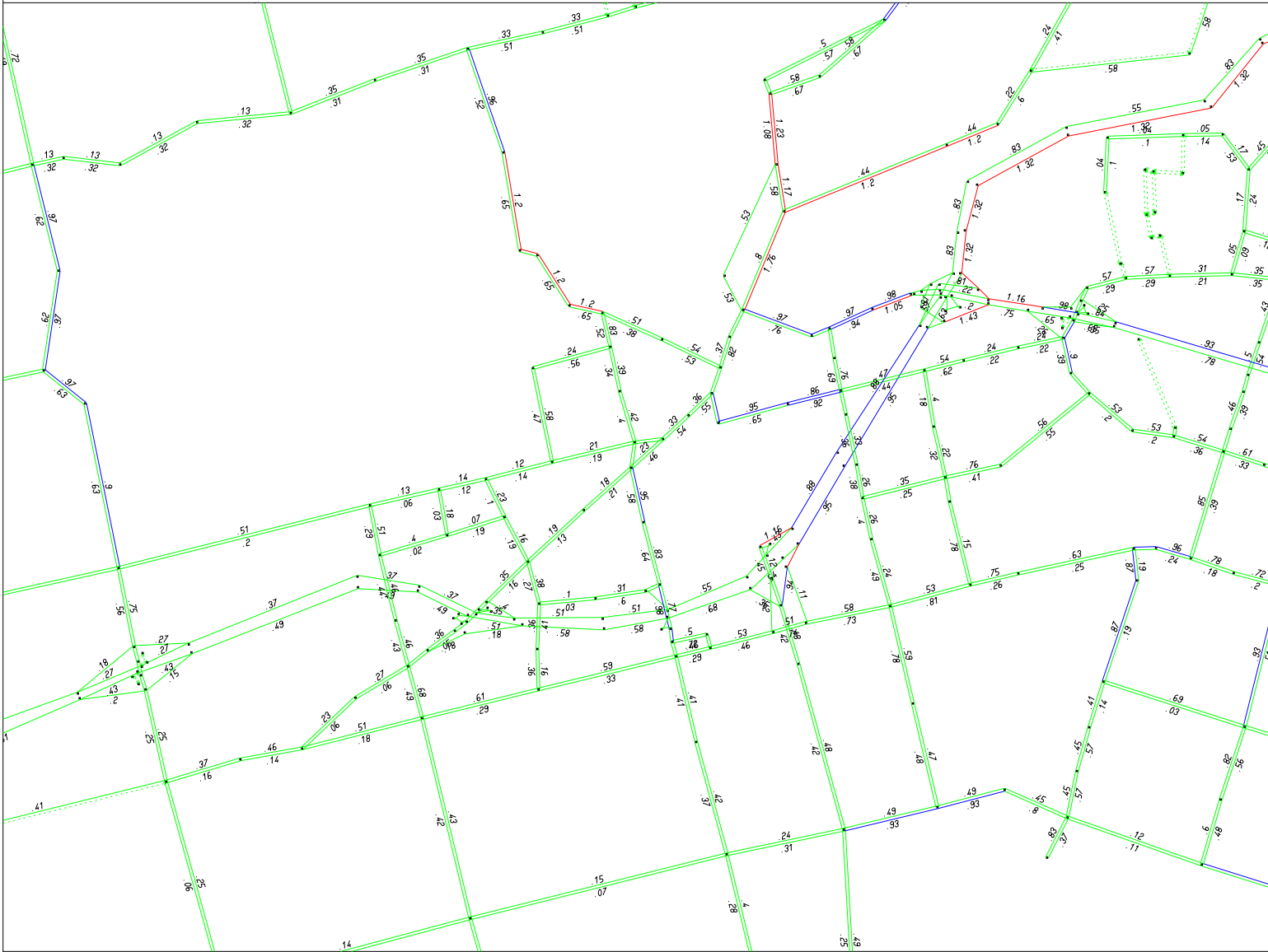


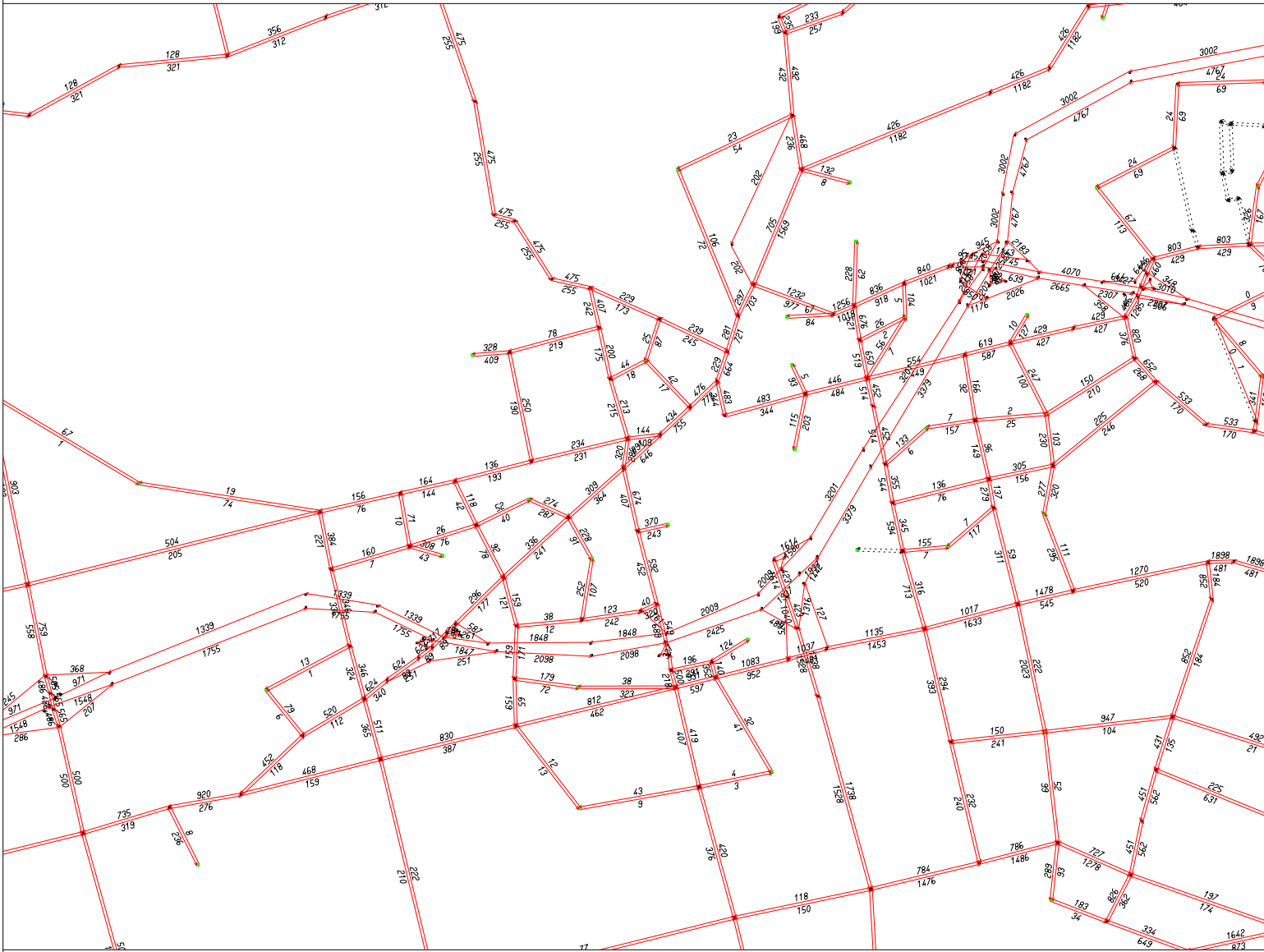
Exhibit 36:
2031
S11 V/C

10-08-16 13:33
MODULE: 2.13
DMG.UTYU...jdk

AUTO VOLUMES

emme/2

Exhibit 37:
2031
S12 Volumes



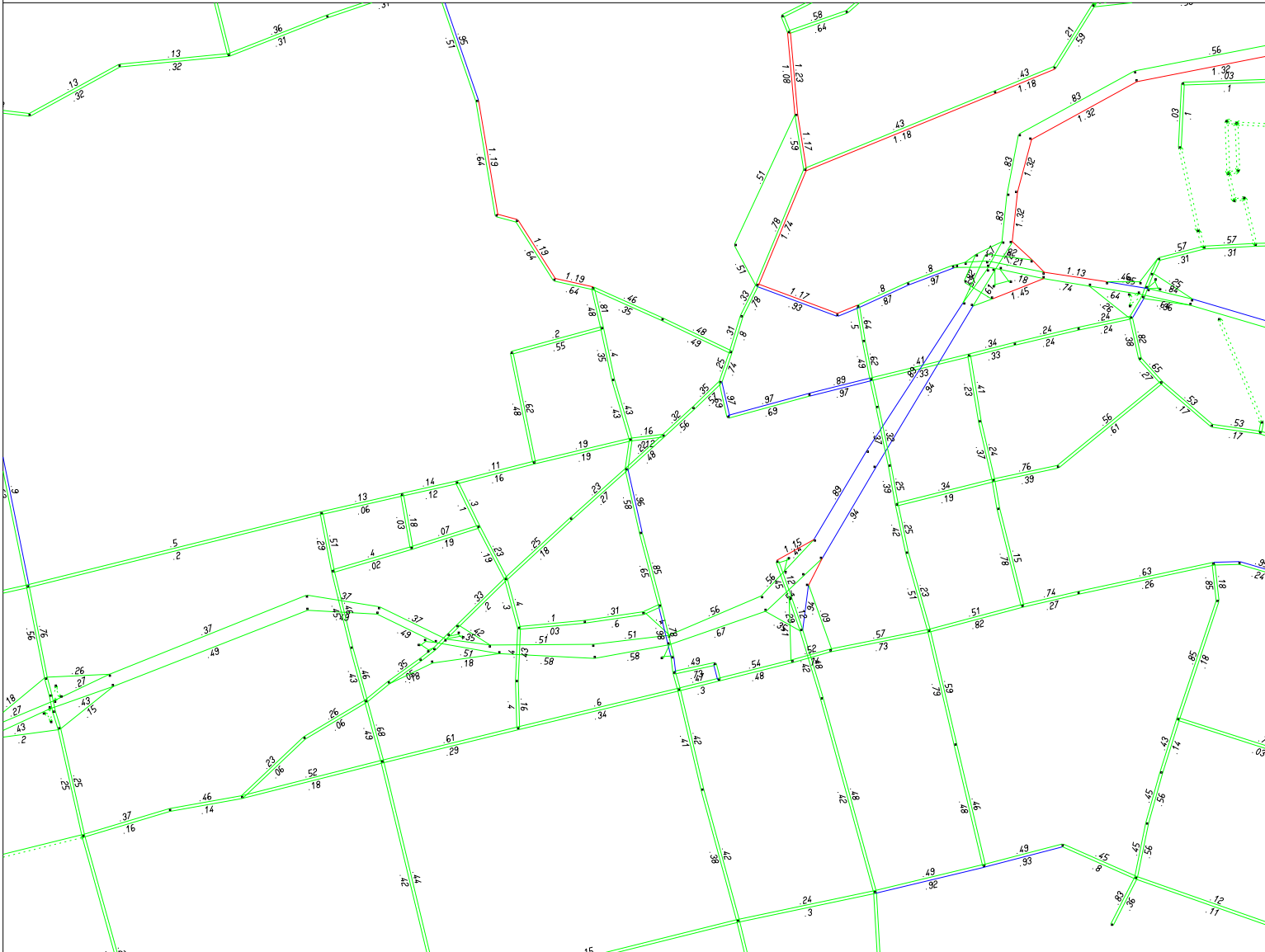
10-08-27 10:02
MODULE: 6.12
DMG.UTYU...j.dk

BASE NETWORK

ATTRIBUTE @VC: VOLUME TO CAPACITY RATIO

emme/2

Exhibit 38:
2031
S12 V/C



10-08-27 10:03
MODULE: 2.13
DMG.UTYU...jdk

Double Lane Roundabout Operation Analysis

FHWA Methodology

Wilson & Rousseaux Operations
Two-Lane Roundabout
2021 AM Peak

08-8952 Ancaster TMP
City of Hamilton
2010 Oct 20

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|---|-----------|---|---|-----------|---|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 369 | 813 | 729 | 212 | 0 | 0 | 0 | 0 | 132 | 0 | 813 |
| Peak hour factor | 0.95 | 0 | 388 | 856 | 767 | 223 | 0 | 0 | 0 | 0 | 139 | 0 | 856 |
| Heavy vehicle % | 2% | 0 | 396 | 873 | 782 | 227 | 0 | 0 | 0 | 0 | 142 | 0 | 873 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 1269 | 782 | 369 | 1009 | 142 | 1269 | 0 | 1151 | 0 | 1015 | 396 | 1655 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1848 | 2300 | 1588 | 2120 |
| Total Delay | 13,965 | 7,850 | 2,813 | 0 | 3,303 |
| v/c | - | 0.69 | 0.44 | 0.00 | 0.48 |
| Avg. Delay | 4.2 | 6.2 | 2.8 | 2.3 | 3.3 |
| Level of Service | A | A | A | A | A |

| | Northbound | Southbound | Eastbound | Westbound |
|------------------------|------------|------------|-----------|-----------|
| Avg Queue Length (veh) | 2.2 | 0.8 | 0.0 | 0.9 |
| Avg Queue Length (m) | 16.4 | 5.9 | 0.0 | 6.9 |
| 95% Queue (veh) | 6.4 | 2.3 | 0.0 | 2.7 |
| 95% Queue (m) | 48.2 | 17.5 | 0.0 | 20.6 |

Note: Assumes closure (i.e. cul-de-sac) of Old Dundas Road.

Double Lane Roundabout Operation Analysis

FHWA Methodology

Wilson & Rousseaux Operations
Two-Lane Roundabout
2021 PM Peak

08-8952 Ancaster TMP
City of Hamilton
2010 Oct 20

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|---|-----------|---|---|-----------|---|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 307 | 190 | 598 | 362 | 0 | 0 | 0 | 0 | 367 | 0 | 721 |
| Peak hour factor | 0.95 | 0 | 323 | 200 | 629 | 381 | 0 | 0 | 0 | 0 | 386 | 0 | 759 |
| Heavy vehicle % | 2% | 0 | 329 | 204 | 642 | 389 | 0 | 0 | 0 | 0 | 394 | 0 | 774 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 533 | 642 | 783 | 1031 | 394 | 1103 | 0 | 1425 | 0 | 1168 | 329 | 846 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1947 | 2122 | 1394 | 2168 |
| Total Delay | 8,957 | 1,357 | 3,400 | 0 | 4,201 |
| v/c | - | 0.27 | 0.49 | 0.00 | 0.54 |
| Avg. Delay | 3.3 | 2.5 | 3.3 | 2.6 | 3.6 |
| Level of Service | A | A | A | A | A |

| | Northbound | Southbound | Eastbound | Westbound |
|------------------------|------------|------------|-----------|-----------|
| Avg Queue Length (veh) | 0.4 | 0.9 | 0.0 | 1.2 |
| Avg Queue Length (m) | 2.8 | 7.1 | 0.0 | 8.8 |
| 95% Queue (veh) | 1.1 | 2.8 | 0.0 | 3.5 |
| 95% Queue (m) | 8.5 | 21.2 | 0.0 | 26.1 |

Note: Assumes closure (i.e. cul-de-sac) of Old Dundas Road.

Double Lane Roundabout Operation Analysis

FHWA Methodology

Wilson & Rousseaux Operations
Two-Lane Roundabout
2031 AM Peak

08-8952 Ancaster TMP
City of Hamilton
2010 Oct 20

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|---|-----------|---|---|-----------|---|------|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 393 | 310 | 957 | 349 | 0 | 0 | 0 | 0 | 111 | 0 | 957 |
| Peak hour factor | 0.95 | 0 | 414 | 326 | 1007 | 367 | 0 | 0 | 0 | 0 | 117 | 0 | 1007 |
| Heavy vehicle % | 2% | 0 | 422 | 333 | 1027 | 374 | 0 | 0 | 0 | 0 | 119 | 0 | 1027 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 755 | 1027 | 493 | 1401 | 119 | 1449 | 0 | 1520 | 0 | 1146 | 422 | 1360 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1675 | 2316 | 1327 | 2102 |
| Total Delay | 12,762 | 2,952 | 5,501 | 0 | 4,309 |
| v/c | - | 0.45 | 0.60 | 0.00 | 0.55 |
| Avg. Delay | 3.9 | 3.9 | 3.9 | 2.7 | 3.8 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|------|------|-----|------|
| Avg Queue Length (veh) | 0.8 | 1.5 | 0.0 | 1.2 |
| Avg Queue Length (m) | 6.1 | 11.5 | 0.0 | 9.0 |
| 95% Queue (veh) | 2.4 | 4.5 | 0.0 | 3.6 |
| 95% Queue (m) | 18.4 | 34.1 | 0.0 | 26.8 |

Note: Assumes closure (i.e. cul-de-sac) of Old Dundas Road.

Double Lane Roundabout Operation Analysis

FHWA Methodology

Wilson & Rousseaux Operations
Two-Lane Roundabout
2031 PM Peak

08-8952 Ancaster TMP
City of Hamilton
2010 Oct 20

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|---|-----------|---|---|-----------|---|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 427 | 160 | 667 | 379 | 0 | 0 | 0 | 0 | 315 | 0 | 795 |
| Peak hour factor | 0.95 | 0 | 449 | 168 | 702 | 399 | 0 | 0 | 0 | 0 | 332 | 0 | 837 |
| Heavy vehicle % | 2% | 0 | 458 | 171 | 716 | 407 | 0 | 0 | 0 | 0 | 339 | 0 | 854 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 629 | 716 | 746 | 1123 | 339 | 1312 | 0 | 1462 | 0 | 1193 | 458 | 887 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1895 | 2161 | 1368 | 2077 |
| Total Delay | 10,532 | 1,789 | 3,892 | 0 | 4,852 |
| v/c | - | 0.33 | 0.52 | 0.00 | 0.57 |
| Avg. Delay | 3.6 | 2.8 | 3.5 | 2.6 | 4.1 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|------|------|-----|------|
| Avg Queue Length (veh) | 0.5 | 1.1 | 0.0 | 1.3 |
| Avg Queue Length (m) | 3.7 | 8.1 | 0.0 | 10.1 |
| 95% Queue (veh) | 1.5 | 3.2 | 0.0 | 4.0 |
| 95% Queue (m) | 11.2 | 24.2 | 0.0 | 30.1 |

Note: Assumes closure (i.e. cul-de-sac) of Old Dundas Road.

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Wilson Street & Jerseyville Road (AM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|------|----|------------|-----|-----|-----------|---|---|-----------|---|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 1001 | 11 | 9 | 484 | 173 | 54 | 1 | 3 | 2 | 0 | 17 |
| Peak hour factor | 0.95 | 0 | 1054 | 12 | 9 | 509 | 182 | 57 | 1 | 3 | 2 | 0 | 18 |
| Heavy vehicle % | 2% | 0 | 1075 | 12 | 9 | 519 | 186 | 58 | 1 | 3 | 2 | 0 | 18 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 1087 | 68 | 524 | 714 | 2 | 1151 | 62 | 530 | 186 | 20 | 1133 | 22 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|-------------|-------------|-------------|-------------|-------------|
| Capacity | - | 1163 | 1199 | 915 | 590 |
| Total Delay | 46,167 | 40,497 | 5,282 | 262 | 126 |
| v/c | - | 0.93 | 0.60 | 0.07 | 0.03 |
| Avg. Delay | 24.5 | 37.3 | 7.4 | 4.2 | 6.3 |
| Level of Service | C | E | A | A | A |

| | | | | |
|------------------------|--------------|-------------|------------|------------|
| Avg Queue Length (veh) | 11.2 | 1.5 | 0.1 | 0.0 |
| Avg Queue Length (m) | 84.4 | 11.0 | 0.5 | 0.3 |
| 95% Queue (veh) | 25.6 | 4.3 | 0.2 | 0.1 |
| 95% Queue (m) | 191.8 | 32.5 | 1.6 | 0.8 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Wilson Street & Jerseyville Road (PM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|---|------------|------|-----|-----------|---|---|-----------|---|---|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 782 | 7 | 8 | 943 | 164 | 54 | 0 | 7 | 5 | 0 | 1 |
| Peak hour factor | 0.95 | 0 | 823 | 7 | 8 | 993 | 173 | 57 | 0 | 7 | 5 | 0 | 1 |
| Heavy vehicle % | 2% | 0 | 839 | 7 | 8 | 1013 | 176 | 58 | 0 | 7 | 5 | 0 | 1 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 846 | 66 | 1025 | 1197 | 5 | 898 | 65 | 1026 | 176 | 6 | 897 | 15 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1164 | 1197 | 648 | 717 |
| Total Delay | 101,255 | 9,451 | 91,371 | 402 | 30 |
| v/c | - | 0.73 | 1.00 | 0.10 | 0.01 |
| Avg. Delay | 47.9 | 11.2 | 76.3 | 6.2 | 5.1 |
| Level of Service | E | B | F | A | A |

| | | | | |
|------------------------|------|-------|-----|-----|
| Avg Queue Length (veh) | 2.6 | 25.4 | 0.1 | 0.0 |
| Avg Queue Length (m) | 19.7 | 190.4 | 0.8 | 0.1 |
| 95% Queue (veh) | 7.6 | 42.3 | 0.3 | 0.0 |
| 95% Queue (m) | 57.0 | 317.2 | 2.5 | 0.2 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Wilson Street & Shaver Road (AM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|----|-----|------------|----|-----|-----------|-----|----|-----------|------|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 86 | 44 | 93 | 15 | 31 | 172 | 84 | 743 | 33 | 32 | 936 | 15 |
| Peak hour factor | 0.95 | 91 | 46 | 98 | 16 | 33 | 181 | 88 | 782 | 35 | 34 | 985 | 16 |
| Heavy vehicle % | 2% | 93 | 47 | 100 | 16 | 34 | 185 | 90 | 798 | 36 | 35 | 1005 | 16 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 240 | 904 | 105 | 235 | 1133 | 153 | 924 | 85 | 1283 | 1056 | 230 | 914 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1762 | 1600 | 2340 | 2238 |
| Total Delay | 6,751 | 568 | 620 | 2,348 | 3,215 |
| v/c | - | 0.14 | 0.15 | 0.39 | 0.47 |
| Avg. Delay | 2.7 | 2.4 | 2.6 | 2.5 | 3.0 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-----|-----|------|------|
| Avg Queue Length (veh) | 0.2 | 0.2 | 0.7 | 0.9 |
| Avg Queue Length (m) | 1.2 | 1.3 | 4.9 | 6.7 |
| 95% Queue (veh) | 0.5 | 0.5 | 2.0 | 2.7 |
| 95% Queue (m) | 3.5 | 3.9 | 14.6 | 20.0 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Wilson Street & Shaver Road (PM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|----|----|------------|---|-----|-----------|------|----|-----------|------|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 42 | 26 | 51 | 7 | 9 | 195 | 238 | 1255 | 82 | 60 | 1144 | 24 |
| Peak hour factor | 0.95 | 44 | 27 | 54 | 7 | 9 | 205 | 251 | 1321 | 86 | 63 | 1204 | 25 |
| Heavy vehicle % | 2% | 45 | 28 | 55 | 7 | 9 | 209 | 256 | 1347 | 88 | 64 | 1228 | 26 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 128 | 1610 | 161 | 225 | 1337 | 310 | 1691 | 80 | 1482 | 1318 | 329 | 1409 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1264 | 1456 | 2344 | 2168 |
| Total Delay | 15,912 | 406 | 658 | 9,277 | 5,571 |
| v/c | - | 0.10 | 0.15 | 0.72 | 0.61 |
| Avg. Delay | 4.7 | 3.2 | 2.9 | 5.5 | 4.2 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-----|-----|------|------|
| Avg Queue Length (veh) | 0.1 | 0.2 | 2.6 | 1.5 |
| Avg Queue Length (m) | 0.8 | 1.4 | 19.3 | 11.6 |
| 95% Queue (veh) | 0.3 | 0.5 | 7.6 | 4.6 |
| 95% Queue (m) | 2.5 | 4.1 | 57.0 | 34.5 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Wilson Street & Halson Street (AM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|-----|------------|---|---|-----------|-----|-----|-----------|-----|---|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 233 | 1 | 195 | 2 | 2 | 1 | 1 | 662 | 252 | 113 | 545 | 2 |
| Peak hour factor | 0.95 | 245 | 1 | 205 | 2 | 2 | 1 | 1 | 697 | 265 | 119 | 574 | 2 |
| Heavy vehicle % | 2% | 250 | 1 | 209 | 2 | 2 | 1 | 1 | 711 | 270 | 121 | 585 | 2 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 460 | 714 | 393 | 5 | 956 | 4 | 982 | 125 | 836 | 708 | 252 | 922 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 816 | 685 | 1133 | 1064 |
| Total Delay | 33,719 | 4,639 | 26 | 21,952 | 7,101 |
| v/c | - | 0.56 | 0.01 | 0.87 | 0.67 |
| Avg. Delay | 15.6 | 10.1 | 5.3 | 22.4 | 10.0 |
| Level of Service | C | B | A | C | B |

| | | | | |
|------------------------|------|-----|-------|------|
| Avg Queue Length (veh) | 1.3 | 0.0 | 6.1 | 2.0 |
| Avg Queue Length (m) | 9.7 | 0.1 | 45.7 | 14.8 |
| 95% Queue (veh) | 3.8 | 0.0 | 16.1 | 5.8 |
| 95% Queue (m) | 28.5 | 0.2 | 120.8 | 43.3 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Wilson Street & Halson Street (PM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|-----|------------|---|---|-----------|-----|-----|-----------|-----|---|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 517 | 0 | 169 | 4 | 7 | 0 | 0 | 604 | 346 | 202 | 667 | 0 |
| Peak hour factor | 0.95 | 544 | 0 | 178 | 4 | 7 | 0 | 0 | 636 | 364 | 213 | 702 | 0 |
| Heavy vehicle % | 2% | 555 | 0 | 182 | 4 | 7 | 0 | 0 | 649 | 371 | 217 | 716 | 0 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 737 | 653 | 595 | 11 | 1488 | 0 | 1020 | 228 | 1271 | 933 | 555 | 835 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|-------------|-------------|-------------|-------------|--------------|
| Capacity | - | 848 | 312 | 1077 | 901 |
| Total Delay | 186,913 | 21,815 | 132 | 45,767 | 119,200 |
| v/c | - | 0.87 | 0.04 | 0.95 | 1.04 |
| Avg. Delay | 69.2 | 29.6 | 12.0 | 44.9 | 127.8 |
| Level of Service | F | D | B | E | F |

| | | | | |
|------------------------|-------|-----|-------|-------|
| Avg Queue Length (veh) | 6.1 | 0.0 | 12.7 | 33.1 |
| Avg Queue Length (m) | 45.4 | 0.3 | 95.3 | 248.3 |
| 95% Queue (veh) | 15.5 | 0.1 | 27.3 | 46.2 |
| 95% Queue (m) | 116.4 | 0.8 | 205.1 | 346.6 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Wilson Street & Halson Street (AM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|-----|------------|---|---|-----------|-----|-----|-----------|-----|---|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 233 | 1 | 195 | 2 | 2 | 1 | 1 | 662 | 252 | 113 | 545 | 2 |
| Peak hour factor | 0.95 | 245 | 1 | 205 | 2 | 2 | 1 | 1 | 697 | 265 | 119 | 574 | 2 |
| Heavy vehicle % | 2% | 250 | 1 | 209 | 2 | 2 | 1 | 1 | 711 | 270 | 121 | 585 | 2 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 460 | 714 | 393 | 5 | 956 | 4 | 982 | 125 | 836 | 708 | 252 | 922 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1896 | 1725 | 2312 | 2222 |
| Total Delay | 5,504 | 1,153 | 10 | 2,657 | 1,683 |
| v/c | - | 0.24 | 0.00 | 0.42 | 0.32 |
| Avg. Delay | 2.6 | 2.5 | 2.1 | 2.7 | 2.4 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-----|-----|------|------|
| Avg Queue Length (veh) | 0.3 | 0.0 | 0.7 | 0.5 |
| Avg Queue Length (m) | 2.4 | 0.0 | 5.5 | 3.5 |
| 95% Queue (veh) | 1.0 | 0.0 | 2.2 | 1.4 |
| 95% Queue (m) | 7.2 | 0.1 | 16.6 | 10.5 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Wilson Street & Halson Street (PM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|-----|------------|---|---|-----------|-----|-----|-----------|-----|---|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 517 | 0 | 169 | 4 | 7 | 0 | 0 | 604 | 346 | 202 | 667 | 0 |
| Peak hour factor | 0.95 | 544 | 0 | 178 | 4 | 7 | 0 | 0 | 636 | 364 | 213 | 702 | 0 |
| Heavy vehicle % | 2% | 555 | 0 | 182 | 4 | 7 | 0 | 0 | 649 | 371 | 217 | 716 | 0 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 737 | 653 | 595 | 11 | 1488 | 0 | 1020 | 228 | 1271 | 933 | 555 | 835 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|------------|-------------|-------------|-------------|-------------|
| Capacity | - | 1939 | 1350 | 2239 | 2008 |
| Total Delay | 8,368 | 2,206 | 30 | 3,010 | 3,121 |
| v/c | - | 0.38 | 0.01 | 0.46 | 0.46 |
| Avg. Delay | 3.1 | 3.0 | 2.7 | 3.0 | 3.3 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-------------|------------|-------------|-------------|
| Avg Queue Length (veh) | 0.6 | 0.0 | 0.8 | 0.9 |
| Avg Queue Length (m) | 4.6 | 0.1 | 6.3 | 6.5 |
| 95% Queue (veh) | 1.8 | 0.0 | 2.5 | 2.6 |
| 95% Queue (m) | 13.8 | 0.2 | 18.7 | 19.4 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Mohawk Road & McNiven Road (AM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|----|------|------------|----|----|-----------|-----|-----|-----------|-----|---|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 376 | 18 | 1268 | 39 | 40 | 18 | 4 | 755 | 782 | 698 | 722 | 7 |
| Peak hour factor | 0.95 | 396 | 19 | 1335 | 41 | 42 | 19 | 4 | 795 | 823 | 735 | 760 | 7 |
| Heavy vehicle % | 2% | 404 | 19 | 1362 | 42 | 43 | 19 | 4 | 811 | 839 | 750 | 775 | 7 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 1785 | 857 | 1632 | 104 | 1929 | 30 | 1654 | 835 | 1198 | 1532 | 427 | 2215 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|-------------|-------------|-------------|-------------|-------------|
| Capacity | - | 1795 | 1038 | 1811 | 2099 |
| Total Delay | 146,263 | 101,902 | 401 | 34,293 | 9,667 |
| v/c | - | 0.99 | 0.10 | 0.91 | 0.73 |
| Avg. Delay | 28.8 | 57.1 | 3.9 | 20.7 | 6.3 |
| Level of Service | D | F | A | C | A |

| | | | | |
|------------------------|-------|-----|-------|------|
| Avg Queue Length (veh) | 28.3 | 0.1 | 9.5 | 2.7 |
| Avg Queue Length (m) | 212.3 | 0.8 | 71.4 | 20.1 |
| 95% Queue (veh) | 49.3 | 0.3 | 24.2 | 7.9 |
| 95% Queue (m) | 369.7 | 2.5 | 181.5 | 59.2 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Mohawk Road & McNiven Road (PM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|----|-----|------------|----|---|-----------|-----|-----|-----------|-----|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 1392 | 57 | 774 | 18 | 27 | 7 | 15 | 740 | 427 | 1167 | 660 | 42 |
| Peak hour factor | 0.95 | 1465 | 60 | 815 | 19 | 28 | 7 | 16 | 779 | 449 | 1228 | 695 | 44 |
| Heavy vehicle % | 2% | 1494 | 61 | 831 | 19 | 29 | 7 | 16 | 795 | 458 | 1253 | 709 | 45 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 2386 | 830 | 1740 | 55 | 3456 | 122 | 1269 | 1301 | 2210 | 2007 | 1571 | 1645 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|--------------|------------|-------------|---------------|
| Capacity | - | 1814 | 0 | 1482 | 1291 |
| Total Delay | #DIV/0! | 1,378,102 | #DIV/0! | 20,553 | 2,024,488 |
| v/c | - | 1.32 | #DIV/0! | 0.86 | 1.55 |
| Avg. Delay | #DIV/0! | 577.6 | #DIV/0! | 16.2 | 1008.7 |
| Level of Service | #DIV/0! | F | #DIV/0! | C | F |

| | | | | |
|------------------------|---------------|---------|--------------|---------------|
| Avg Queue Length (veh) | 382.8 | #DIV/0! | 5.7 | 562.4 |
| Avg Queue Length (m) | 2871.0 | #DIV/0! | 42.8 | 4217.7 |
| 95% Queue (veh) | 298.0 | #DIV/0! | 15.6 | 366.2 |
| 95% Queue (m) | 2234.6 | #DIV/0! | 117.1 | 2746.4 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Wilson Street & Fiddler's Green Road (AM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|-----|-----------|-----|----|-----------|-----|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 141 | 125 | 222 | 162 | 179 | 149 | 61 | 419 | 83 | 76 | 326 | 26 |
| Peak hour factor | 0.95 | 148 | 132 | 234 | 171 | 188 | 157 | 64 | 441 | 87 | 80 | 343 | 27 |
| Heavy vehicle % | 2% | 151 | 135 | 239 | 174 | 192 | 160 | 65 | 450 | 89 | 82 | 350 | 28 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 525 | 689 | 363 | 526 | 583 | 228 | 604 | 448 | 661 | 460 | 351 | 863 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 829 | 886 | 959 | 1011 |
| Total Delay | 20,501 | 6,173 | 5,234 | 6,093 | 3,001 |
| v/c | - | 0.63 | 0.59 | 0.63 | 0.45 |
| Avg. Delay | 9.7 | 11.8 | 10.0 | 10.1 | 6.5 |
| Level of Service | A | B | A | B | A |

| | Northbound | Southbound | Eastbound | Westbound |
|------------------------|------------|------------|-----------|-----------|
| Avg Queue Length (veh) | 1.7 | 1.5 | 1.7 | 0.8 |
| Avg Queue Length (m) | 12.9 | 10.9 | 12.7 | 6.3 |
| 95% Queue (veh) | 5.0 | 4.3 | 5.0 | 2.5 |
| 95% Queue (m) | 37.6 | 32.1 | 37.3 | 18.6 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Wilson Street & Fiddler's Green Road (PM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|-----|-----------|-----|-----|-----------|-----|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 188 | 94 | 126 | 51 | 108 | 115 | 151 | 511 | 244 | 228 | 648 | 11 |
| Peak hour factor | 0.95 | 198 | 99 | 133 | 54 | 114 | 121 | 159 | 538 | 257 | 240 | 682 | 12 |
| Heavy vehicle % | 2% | 202 | 101 | 136 | 55 | 116 | 123 | 162 | 549 | 262 | 245 | 696 | 12 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 439 | 766 | 623 | 294 | 1143 | 275 | 973 | 416 | 1021 | 953 | 465 | 740 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 788 | 585 | 976 | 950 |
| Total Delay | 173,843 | 4,516 | 3,630 | 80,103 | 85,593 |
| v/c | - | 0.56 | 0.50 | 1.00 | 1.00 |
| Avg. Delay | 65.4 | 10.3 | 12.3 | 82.3 | 89.8 |
| Level of Service | F | B | B | F | F |

| | | | | |
|------------------------|------|------|-------|-------|
| Avg Queue Length (veh) | 1.3 | 1.0 | 22.3 | 23.8 |
| Avg Queue Length (m) | 9.4 | 7.6 | 166.9 | 178.3 |
| 95% Queue (veh) | 3.7 | 3.0 | 37.5 | 38.7 |
| 95% Queue (m) | 27.8 | 22.3 | 281.0 | 290.0 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Wilson Street & Fiddler's Green Road (AM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|-----|-----------|-----|----|-----------|-----|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 141 | 125 | 222 | 162 | 179 | 149 | 61 | 419 | 83 | 76 | 326 | 26 |
| Peak hour factor | 0.95 | 148 | 132 | 234 | 171 | 188 | 157 | 64 | 441 | 87 | 80 | 343 | 27 |
| Heavy vehicle % | 2% | 151 | 135 | 239 | 174 | 192 | 160 | 65 | 450 | 89 | 82 | 350 | 28 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 525 | 689 | 363 | 526 | 583 | 228 | 604 | 448 | 661 | 460 | 351 | 863 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1914 | 1988 | 2084 | 2152 |
| Total Delay | 5,103 | 1,361 | 1,295 | 1,469 | 979 |
| v/c | - | 0.27 | 0.26 | 0.29 | 0.21 |
| Avg. Delay | 2.4 | 2.6 | 2.5 | 2.4 | 2.1 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-----|-----|-----|-----|
| Avg Queue Length (veh) | 0.4 | 0.4 | 0.4 | 0.3 |
| Avg Queue Length (m) | 2.8 | 2.7 | 3.1 | 2.0 |
| 95% Queue (veh) | 1.1 | 1.1 | 1.2 | 0.8 |
| 95% Queue (m) | 8.5 | 8.1 | 9.2 | 6.1 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Wilson Street & Fiddler's Green Road (PM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|-----|-----------|-----|-----|-----------|-----|----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 188 | 94 | 126 | 51 | 108 | 115 | 151 | 511 | 244 | 228 | 648 | 11 |
| Peak hour factor | 0.95 | 198 | 99 | 133 | 54 | 114 | 121 | 159 | 538 | 257 | 240 | 682 | 12 |
| Heavy vehicle % | 2% | 202 | 101 | 136 | 55 | 116 | 123 | 162 | 549 | 262 | 245 | 696 | 12 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 439 | 766 | 623 | 294 | 1143 | 275 | 973 | 416 | 1021 | 953 | 465 | 740 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|------------|-------------|-------------|-------------|-------------|
| Capacity | - | 1859 | 1593 | 2106 | 2072 |
| Total Delay | 8,080 | 1,113 | 815 | 3,088 | 3,064 |
| v/c | - | 0.24 | 0.18 | 0.46 | 0.46 |
| Avg. Delay | 3.0 | 2.5 | 2.8 | 3.2 | 3.2 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|------------|------------|-------------|-------------|
| Avg Queue Length (veh) | 0.3 | 0.2 | 0.9 | 0.9 |
| Avg Queue Length (m) | 2.3 | 1.7 | 6.4 | 6.4 |
| 95% Queue (veh) | 0.9 | 0.7 | 2.6 | 2.5 |
| 95% Queue (m) | 6.9 | 5.1 | 19.2 | 19.1 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Golf Links Road & Southcote Road (AM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|----|-----------|-----|-----|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 66 | 418 | 139 | 365 | 685 | 38 | 281 | 187 | 207 | 82 | 376 | 534 |
| Peak hour factor | 0.95 | 69 | 440 | 146 | 384 | 721 | 40 | 296 | 197 | 218 | 86 | 396 | 562 |
| Heavy vehicle % | 2% | 70 | 449 | 149 | 392 | 735 | 41 | 302 | 201 | 222 | 88 | 404 | 573 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 668 | 895 | 1045 | 1168 | 562 | 1324 | 725 | 1215 | 515 | 1065 | 821 | 742 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|--------------|-------------|--------------|--------------|--------------|
| Capacity | - | 718 | 897 | 546 | 758 |
| Total Delay | 1,944,706 | 35,610 | 658,302 | 451,887 | 798,907 |
| v/c | - | 0.93 | 1.30 | 1.33 | 1.41 |
| Avg. Delay | 536.3 | 53.3 | 563.6 | 623.3 | 750.1 |
| Level of Service | F | F | F | F | F |

| | | | | |
|------------------------|-------|--------|-------|--------|
| Avg Queue Length (veh) | 9.9 | 182.9 | 125.5 | 221.9 |
| Avg Queue Length (m) | 74.2 | 1371.5 | 941.4 | 1664.4 |
| 95% Queue (veh) | 21.5 | 147.2 | 100.4 | 163.3 |
| 95% Queue (m) | 161.4 | 1104.1 | 753.3 | 1224.9 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Golf Links Road & Southcote Road (PM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|-----|-----------|-----|-----|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 297 | 756 | 128 | 739 | 443 | 220 | 41 | 538 | 107 | 213 | 284 | 663 |
| Peak hour factor | 0.95 | 313 | 796 | 135 | 778 | 466 | 232 | 43 | 566 | 113 | 224 | 299 | 698 |
| Heavy vehicle % | 2% | 319 | 812 | 138 | 794 | 475 | 237 | 44 | 577 | 115 | 228 | 305 | 712 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 1269 | 1415 | 818 | 1506 | 852 | 1568 | 736 | 1497 | 861 | 1245 | 1175 | 1509 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|----------|-------------|-------------|-------------|-------------|
| Capacity | - | 385 | 741 | 303 | 567 |
| Total Delay | ##### | 5,273,605 | 2,818,528 | 1,916,689 | 2,699,382 |
| v/c | - | 3.30 | 2.03 | 2.43 | 2.19 |
| Avg. Delay | 2672.0 | 4155.7 | 1871.5 | 2604.2 | 2168.2 |
| Level of Service | F | F | F | F | F |

| | | | | |
|------------------------|---------|--------|--------|--------|
| Avg Queue Length (veh) | 1464.9 | 782.9 | 532.4 | 749.8 |
| Avg Queue Length (m) | 10986.7 | 5871.9 | 3993.1 | 5623.7 |
| 95% Queue (veh) | 446.3 | 388.2 | 221.5 | 344.3 |
| 95% Queue (m) | 3347.0 | 2911.5 | 1661.1 | 2582.0 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Golf Links Road & Southcote Road (AM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|----|-----------|-----|-----|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 66 | 418 | 139 | 365 | 685 | 38 | 281 | 187 | 207 | 82 | 376 | 534 |
| Peak hour factor | 0.95 | 69 | 440 | 146 | 384 | 721 | 40 | 296 | 197 | 218 | 86 | 396 | 562 |
| Heavy vehicle % | 2% | 70 | 449 | 149 | 392 | 735 | 41 | 302 | 201 | 222 | 88 | 404 | 573 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 668 | 895 | 1045 | 1168 | 562 | 1324 | 725 | 1215 | 515 | 1065 | 821 | 742 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1768 | 2003 | 1542 | 1820 |
| Total Delay | 15,463 | 2,185 | 5,024 | 3,190 | 5,064 |
| v/c | - | 0.38 | 0.58 | 0.47 | 0.59 |
| Avg. Delay | 4.3 | 3.3 | 4.3 | 4.4 | 4.8 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|------|------|------|------|
| Avg Queue Length (veh) | 0.6 | 1.4 | 0.9 | 1.4 |
| Avg Queue Length (m) | 4.6 | 10.5 | 6.6 | 10.5 |
| 95% Queue (veh) | 1.8 | 4.2 | 2.6 | 4.2 |
| 95% Queue (m) | 13.6 | 31.2 | 19.8 | 31.4 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Golf Links Road & Southcote Road (PM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|-----|-----|------------|-----|-----|-----------|-----|-----|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 297 | 756 | 128 | 739 | 443 | 220 | 41 | 538 | 107 | 213 | 284 | 663 |
| Peak hour factor | 0.95 | 313 | 796 | 135 | 778 | 466 | 232 | 43 | 566 | 113 | 224 | 299 | 698 |
| Heavy vehicle % | 2% | 319 | 812 | 138 | 794 | 475 | 237 | 44 | 577 | 115 | 228 | 305 | 712 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 1269 | 1415 | 818 | 1506 | 852 | 1568 | 736 | 1497 | 861 | 1245 | 1175 | 1509 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|-------------|-------------|-------------|-------------|-------------|
| Capacity | - | 1401 | 1799 | 1343 | 1571 |
| Total Delay | 66,887 | 30,993 | 18,019 | 4,353 | 13,521 |
| v/c | - | 0.91 | 0.84 | 0.55 | 0.79 |
| Avg. Delay | 14.1 | 24.4 | 12.0 | 5.9 | 10.9 |
| Level of Service | B | C | B | A | B |

| | Northbound | Southbound | Eastbound | Westbound |
|------------------------|--------------|--------------|-------------|-------------|
| Avg Queue Length (veh) | 8.6 | 5.0 | 1.2 | 3.8 |
| Avg Queue Length (m) | 64.6 | 37.5 | 9.1 | 28.2 |
| 95% Queue (veh) | 21.7 | 14.1 | 3.6 | 10.8 |
| 95% Queue (m) | 162.6 | 105.6 | 26.9 | 80.7 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Garner Road & Hamilton Drive (AM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|---|------------|---|----|-----------|-----|---|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 0 | 0 | 177 | 0 | 50 | 48 | 633 | 0 | 0 | 740 | 301 |
| Peak hour factor | 0.95 | 0 | 0 | 0 | 186 | 0 | 53 | 51 | 666 | 0 | 0 | 779 | 317 |
| Heavy vehicle % | 2% | 0 | 0 | 0 | 190 | 0 | 54 | 52 | 679 | 0 | 0 | 795 | 323 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 0 | 921 | 0 | 244 | 795 | 375 | 731 | 190 | 849 | 1118 | 52 | 869 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 704 | 772 | 1098 | 1172 |
| Total Delay | 59,359 | 0 | 1,663 | 7,126 | 50,571 |
| v/c | - | 0.00 | 0.32 | 0.67 | 0.95 |
| Avg. Delay | 28.4 | 5.1 | 6.8 | 9.7 | 45.2 |
| Level of Service | D | A | A | A | E |

| | | | | |
|------------------------|-----|------|------|-------|
| Avg Queue Length (veh) | 0.0 | 0.5 | 2.0 | 14.0 |
| Avg Queue Length (m) | 0.0 | 3.5 | 14.8 | 105.4 |
| 95% Queue (veh) | 0.0 | 1.4 | 5.8 | 29.6 |
| 95% Queue (m) | 0.0 | 10.3 | 43.5 | 222.1 |

Single Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
 One-Lane Roundabout
 Garner Road & Hamilton Drive (PM)

08-8952 Ancaster TMP
 City of Hamilton
 2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|---|------------|---|----|-----------|-----|---|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 0 | 0 | 138 | 0 | 78 | 50 | 817 | 0 | 0 | 694 | 101 |
| Peak hour factor | 0.95 | 0 | 0 | 0 | 145 | 0 | 82 | 53 | 860 | 0 | 0 | 731 | 106 |
| Heavy vehicle % | 2% | 0 | 0 | 0 | 148 | 0 | 84 | 54 | 877 | 0 | 0 | 746 | 108 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 0 | 1079 | 0 | 232 | 746 | 162 | 931 | 148 | 830 | 854 | 54 | 1025 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 619 | 798 | 1120 | 1171 |
| Total Delay | 28,069 | 0 | 1,474 | 17,010 | 9,584 |
| v/c | - | 0.00 | 0.29 | 0.83 | 0.73 |
| Avg. Delay | 13.9 | 5.8 | 6.4 | 18.3 | 11.2 |
| Level of Service | B | A | A | C | B |

| | | | | |
|------------------------|-----|-----|------|------|
| Avg Queue Length (veh) | 0.0 | 0.4 | 4.7 | 2.7 |
| Avg Queue Length (m) | 0.0 | 3.1 | 35.4 | 20.0 |
| 95% Queue (veh) | 0.0 | 1.2 | 13.0 | 7.7 |
| 95% Queue (m) | 0.0 | 9.2 | 97.3 | 57.8 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Garner Road & Hamilton Drive (AM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|---|------------|---|----|-----------|-----|---|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 0 | 0 | 177 | 0 | 50 | 48 | 633 | 0 | 0 | 740 | 301 |
| Peak hour factor | 0.95 | 0 | 0 | 0 | 186 | 0 | 53 | 51 | 666 | 0 | 0 | 779 | 317 |
| Heavy vehicle % | 2% | 0 | 0 | 0 | 190 | 0 | 54 | 52 | 679 | 0 | 0 | 795 | 323 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 0 | 921 | 0 | 244 | 795 | 375 | 731 | 190 | 849 | 1118 | 52 | 869 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1750 | 1839 | 2266 | 2363 |
| Total Delay | 5,495 | 0 | 551 | 1,714 | 3,230 |
| v/c | - | 0.00 | 0.13 | 0.32 | 0.47 |
| Avg. Delay | 2.6 | 2.1 | 2.3 | 2.3 | 2.9 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-----|-----|------|------|
| Avg Queue Length (veh) | 0.0 | 0.2 | 0.5 | 0.9 |
| Avg Queue Length (m) | 0.0 | 1.1 | 3.6 | 6.7 |
| 95% Queue (veh) | 0.0 | 0.5 | 1.4 | 2.7 |
| 95% Queue (m) | 0.0 | 3.4 | 10.7 | 20.1 |

Double Lane Roundabout Operation Analysis

FHWA Methodology

2031 Horizon
Two-Lane Roundabout
Garner Road & Hamilton Drive (PM)

08-8952 Ancaster TMP
City of Hamilton
2010 Nov 09

| | Adj | Northbound | | | Southbound | | | Eastbound | | | Westbound | | |
|------------------|------|------------|---|---|------------|---|----|-----------|-----|---|-----------|-----|-----|
| | | L | T | R | L | T | R | L | T | R | L | T | R |
| Base volume | - | 0 | 0 | 0 | 138 | 0 | 78 | 50 | 817 | 0 | 0 | 694 | 101 |
| Peak hour factor | 0.95 | 0 | 0 | 0 | 145 | 0 | 82 | 53 | 860 | 0 | 0 | 731 | 106 |
| Heavy vehicle % | 2% | 0 | 0 | 0 | 148 | 0 | 84 | 54 | 877 | 0 | 0 | 746 | 108 |

| | Entering | Circ | Exit SB | Entering | Circ | Exit NB | Entering | Circ | Exit WB | Entering | Circ | Exit EB |
|-----------|----------|------|---------|----------|------|---------|----------|------|---------|----------|------|---------|
| Flow Rate | 0 | 1079 | 0 | 232 | 746 | 162 | 931 | 148 | 830 | 854 | 54 | 1025 |

| | Overall | Northbound | Southbound | Eastbound | Westbound |
|------------------|---------|------------|------------|-----------|-----------|
| Capacity | - | 1638 | 1873 | 2296 | 2362 |
| Total Delay | 5,002 | 0 | 509 | 2,455 | 2,038 |
| v/c | - | 0.00 | 0.12 | 0.41 | 0.36 |
| Avg. Delay | 2.5 | 2.2 | 2.2 | 2.6 | 2.4 |
| Level of Service | A | A | A | A | A |

| | | | | |
|------------------------|-----|-----|------|------|
| Avg Queue Length (veh) | 0.0 | 0.1 | 0.7 | 0.6 |
| Avg Queue Length (m) | 0.0 | 1.1 | 5.1 | 4.2 |
| 95% Queue (veh) | 0.0 | 0.4 | 2.0 | 1.7 |
| 95% Queue (m) | 0.0 | 3.2 | 15.3 | 12.7 |

HCM Signalized Intersection Capacity Analysis

31: Mohawk/Rosseaux & McNiven

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|------|------|-------|-------|-------|------|------|------|
| Lane Configurations | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1750 | 1842 | 1566 | 1750 | 1842 | 1566 | 1711 | 1842 | 1531 | 1711 | 1736 | 1736 |
| Fl _t Permitted | 0.30 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.63 | 1.00 | 1.00 | 0.75 | 1.00 | 1.00 |
| Satd. Flow (perm) | 554 | 1842 | 1566 | 153 | 1842 | 1566 | 1131 | 1842 | 1531 | 1345 | 1736 | 1736 |
| Volume (vph) | 4 | 825 | 368 | 212 | 592 | 6 | 319 | 15 | 1133 | 38 | 29 | 18 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 4 | 897 | 400 | 230 | 643 | 7 | 347 | 16 | 1232 | 41 | 32 | 20 |
| RTOR Reduction (vph) | 0 | 0 | 84 | 0 | 0 | 4 | 0 | 0 | 255 | 0 | 16 | 0 |
| Lane Group Flow (vph) | 4 | 897 | 316 | 230 | 643 | 3 | 347 | 16 | 977 | 41 | 36 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | pm+pt | | Perm | Perm | | |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 42.2 | 42.2 | 42.2 | 61.9 | 61.9 | 61.9 | 55.6 | 55.6 | 55.6 | 24.7 | 24.7 | |
| Effective Green, g (s) | 44.1 | 44.1 | 44.1 | 63.8 | 63.8 | 63.8 | 57.3 | 57.3 | 57.3 | 26.4 | 26.4 | |
| Actuated g/C Ratio | 0.34 | 0.34 | 0.34 | 0.49 | 0.49 | 0.49 | 0.44 | 0.44 | 0.44 | 0.20 | 0.20 | |
| Clearance Time (s) | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 | 5.9 | 4.0 | 5.7 | 5.7 | 5.7 | 5.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | 3.5 | 2.0 | 3.5 | 3.5 | 3.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 189 | 629 | 535 | 270 | 910 | 774 | 623 | 818 | 680 | 275 | 355 | |
| v/s Ratio Prot | | c0.49 | | c0.10 | 0.35 | | 0.12 | 0.01 | | | 0.02 | |
| v/s Ratio Perm | 0.01 | | 0.20 | 0.32 | | 0.00 | 0.13 | | c0.64 | 0.03 | | |
| v/c Ratio | 0.02 | 1.43 | 0.59 | 0.85 | 0.71 | 0.00 | 0.56 | 0.02 | 1.44 | 0.15 | 0.10 | |
| Uniform Delay, d ₁ | 28.2 | 42.5 | 35.1 | 37.5 | 25.4 | 16.6 | 25.1 | 20.1 | 35.9 | 42.1 | 41.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.1 | 200.9 | 1.9 | 21.2 | 2.6 | 0.0 | 1.1 | 0.0 | 205.1 | 0.1 | 0.0 | |
| Delay (s) | 28.2 | 243.4 | 36.9 | 58.7 | 28.0 | 16.6 | 26.2 | 20.1 | 241.0 | 42.2 | 41.8 | |
| Level of Service | C | F | D | E | C | B | C | C | F | D | D | |
| Approach Delay (s) | | 179.2 | | | 35.9 | | | 192.0 | | | 42.0 | |
| Approach LOS | | F | | | D | | | F | | | D | |













Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|------|
| HCM Average Control Delay | 148.6 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.36 | | |
| Actuated Cycle Length (s) | 129.1 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 131.9% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
52: Golf Links & Stone Church

11/12/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑ | | ↑ | | ↑ | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.91 | 0.91 | 1.00 |
| Flt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.98 | 1.00 |
| Satd. Flow (prot) | | 4916 | 1531 | 1711 | 3421 | | 1711 | | 1531 | 1628 | 3348 | 1601 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.39 | | 1.00 | 0.95 | 0.98 | 1.00 |
| Satd. Flow (perm) | | 4916 | 1531 | 1711 | 3421 | | 700 | | 1531 | 1628 | 3348 | 1601 |
| Volume (vph) | 0 | 845 | 112 | 243 | 1202 | 0 | 301 | 0 | 327 | 313 | 173 | 236 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 918 | 122 | 264 | 1307 | 0 | 327 | 0 | 355 | 340 | 188 | 257 |
| RTOR Reduction (vph) | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 37 |
| Lane Group Flow (vph) | 0 | 918 | 37 | 264 | 1307 | 0 | 327 | 0 | 350 | 170 | 358 | 220 |
| Turn Type | | | Perm | Prot | | | custom | | custom | Perm | | Perm |
| Protected Phases | | 6 | | 5 | 2 | | 3 | | 5 | 8 | | 4 |
| Permitted Phases | | | 6 | | | | 8 | | 3 | 4 | 4 | 4 |
| Actuated Green, G (s) | | 25.3 | 25.3 | 13.0 | 43.3 | | 34.7 | | 53.7 | 23.7 | 23.7 | 23.7 |
| Effective Green, g (s) | | 27.3 | 27.3 | 14.0 | 45.3 | | 36.7 | | 54.7 | 25.7 | 25.7 | 25.7 |
| Actuated g/C Ratio | | 0.30 | 0.30 | 0.16 | 0.50 | | 0.41 | | 0.61 | 0.29 | 0.29 | 0.29 |
| Clearance Time (s) | | 6.0 | 6.0 | 5.0 | 6.0 | | 3.0 | | | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | 1.0 | 2.0 | | 1.0 | | | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | | 1491 | 464 | 266 | 1722 | | 364 | | 931 | 465 | 956 | 457 |
| v/s Ratio Prot | | 0.19 | | c0.15 | c0.38 | | c0.07 | | 0.23 | | | |
| v/s Ratio Perm | | | 0.02 | | | | c0.30 | | | 0.10 | 0.11 | 0.14 |
| v/c Ratio | | 0.62 | 0.08 | 0.99 | 0.76 | | 0.90 | | 0.38 | 0.37 | 0.37 | 0.48 |
| Uniform Delay, d1 | | 26.9 | 22.4 | 37.9 | 18.0 | | 24.1 | | 9.0 | 25.6 | 25.7 | 26.6 |
| Progression Factor | | 1.15 | 1.61 | 1.04 | 1.28 | | 1.09 | | 1.13 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.7 | 0.3 | 41.5 | 2.0 | | 23.2 | | 0.1 | 0.2 | 0.1 | 0.3 |
| Delay (s) | | 32.6 | 36.4 | 81.2 | 25.0 | | 49.6 | | 10.2 | 25.8 | 25.8 | 26.9 |
| Level of Service | | C | D | F | C | | D | | B | C | C | C |
| Approach Delay (s) | | 33.1 | | | 34.4 | | | 29.1 | | | 26.2 | |
| Approach LOS | | C | | | C | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 31.6 | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | | 0.84 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 74.5% | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

75: Golf Links Rd & Neville

11/12/2010

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
|-----------------------------------|-------|------|-------|-------|----------------------|------|------|------|------|-------|------|------|--|
| Lane Configurations | | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | | 1.00 | 0.93 | | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1629 | | 3319 | 1715 | | |
| Fl _t Permitted | 0.07 | 1.00 | 1.00 | 0.31 | 1.00 | 1.00 | 0.63 | 1.00 | | 0.40 | 1.00 | | |
| Satd. Flow (perm) | 134 | 3500 | 1531 | 565 | 3500 | 1531 | 1136 | 1629 | | 1410 | 1715 | | |
| Volume (vph) | 53 | 690 | 22 | 125 | 1525 | 148 | 115 | 50 | 167 | 279 | 63 | 53 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Adj. Flow (vph) | 58 | 750 | 24 | 136 | 1658 | 161 | 125 | 54 | 182 | 303 | 68 | 58 | |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 55 | 0 | 143 | 0 | 0 | 42 | 0 | |
| Lane Group Flow (vph) | 58 | 750 | 14 | 136 | 1658 | 106 | 125 | 93 | 0 | 303 | 84 | 0 | |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | Perm | | | |
| Protected Phases | 1 | 6 | | 5 | 2 | | | 8 | | | 4 | | |
| Permitted Phases | 6 | | 6 | 2 | | 2 | 8 | | | 4 | | | |
| Actuated Green, G (s) | 55.7 | 51.6 | 51.6 | 59.3 | 53.4 | 53.4 | 17.5 | 17.5 | | 17.5 | 17.5 | | |
| Effective Green, g (s) | 56.7 | 53.6 | 53.6 | 60.3 | 55.4 | 55.4 | 19.5 | 19.5 | | 19.5 | 19.5 | | |
| Actuated g/C Ratio | 0.63 | 0.60 | 0.60 | 0.67 | 0.62 | 0.62 | 0.22 | 0.22 | | 0.22 | 0.22 | | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | |
| Lane Grp Cap (vph) | 139 | 2084 | 912 | 441 | 2154 | 942 | 246 | 353 | | 306 | 372 | | |
| v/s Ratio Prot | 0.01 | 0.21 | | c0.02 | c0.47 | | | 0.06 | | | 0.05 | | |
| v/s Ratio Perm | 0.25 | | 0.01 | 0.19 | | 0.07 | 0.11 | | | c0.21 | | | |
| v/c Ratio | 0.42 | 0.36 | 0.02 | 0.31 | 0.77 | 0.11 | 0.51 | 0.26 | | 0.99 | 0.23 | | |
| Uniform Delay, d ₁ | 11.5 | 9.4 | 7.4 | 5.8 | 12.6 | 7.1 | 31.0 | 29.3 | | 35.2 | 29.0 | | |
| Progression Factor | 0.99 | 0.66 | 0.33 | 0.67 | 0.95 | 0.65 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d ₂ | 0.7 | 0.5 | 0.0 | 0.1 | 1.8 | 0.2 | 0.6 | 0.1 | | 48.6 | 0.1 | | |
| Delay (s) | 12.0 | 6.6 | 2.5 | 4.0 | 13.9 | 4.8 | 31.6 | 29.4 | | 83.7 | 29.2 | | |
| Level of Service | B | A | A | A | B | A | C | C | | F | C | | |
| Approach Delay (s) | | 6.9 | | | 12.4 | | | 30.2 | | | 67.7 | | |
| Approach LOS | | A | | | B | | | C | | | E | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM Average Control Delay | | | 19.6 | | HCM Level of Service | | | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.81 | | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | | | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 80.9% | | ICU Level of Service | | | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

78: Golf Links & McNiven

11/12/2010

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|------|------|----------------------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 | 1711 | 3249 | | 1711 | 1726 | |
| Flt Permitted | 0.40 | 1.00 | 1.00 | 0.68 | 1.00 | 1.00 | 0.62 | 1.00 | | 0.27 | 1.00 | |
| Satd. Flow (perm) | 724 | 1801 | 1531 | 1232 | 1801 | 1531 | 1111 | 3249 | | 489 | 1726 | |
| Volume (vph) | 325 | 104 | 82 | 82 | 177 | 491 | 88 | 276 | 139 | 258 | 151 | 58 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 353 | 113 | 89 | 89 | 192 | 534 | 96 | 300 | 151 | 280 | 164 | 63 |
| RTOR Reduction (vph) | 0 | 0 | 49 | 0 | 0 | 395 | 0 | 55 | 0 | 0 | 13 | 0 |
| Lane Group Flow (vph) | 353 | 113 | 40 | 89 | 192 | 139 | 96 | 396 | 0 | 280 | 214 | 0 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | pm+pt | | | pm+pt | | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 37.6 | 37.6 | 37.6 | 16.6 | 16.6 | 16.6 | 20.2 | 17.2 | | 38.7 | 31.7 | |
| Effective Green, g (s) | 39.7 | 39.7 | 39.7 | 18.7 | 18.7 | 18.7 | 22.5 | 19.5 | | 41.0 | 34.0 | |
| Actuated g/C Ratio | 0.45 | 0.45 | 0.45 | 0.21 | 0.21 | 0.21 | 0.25 | 0.22 | | 0.46 | 0.38 | |
| Clearance Time (s) | 4.0 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 4.0 | 6.3 | | 4.0 | 6.3 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 513 | 806 | 685 | 260 | 380 | 323 | 302 | 714 | | 467 | 662 | |
| v/s Ratio Prot | c0.13 | 0.06 | | | 0.11 | | 0.01 | 0.12 | | c0.12 | 0.12 | |
| v/s Ratio Perm | c0.18 | | 0.03 | 0.07 | | 0.09 | 0.07 | | | c0.16 | | |
| v/c Ratio | 0.69 | 0.14 | 0.06 | 0.34 | 0.51 | 0.43 | 0.32 | 0.55 | | 0.60 | 0.32 | |
| Uniform Delay, d1 | 17.6 | 14.4 | 13.9 | 29.8 | 30.9 | 30.4 | 26.2 | 30.7 | | 16.2 | 19.3 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 3.8 | 0.1 | 0.0 | 0.8 | 1.1 | 0.9 | 0.6 | 0.9 | | 2.1 | 0.3 | |
| Delay (s) | 21.5 | 14.5 | 13.9 | 30.6 | 32.0 | 31.3 | 26.8 | 31.7 | | 18.3 | 19.5 | |
| Level of Service | C | B | B | C | C | C | C | C | | B | B | |
| Approach Delay (s) | | 18.8 | | | 31.4 | | | 30.8 | | | 18.9 | |
| Approach LOS | | B | | | C | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 25.8 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.63 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 88.7 | | | | Sum of lost time (s) | | 8.0 | | | |
| Intersection Capacity Utilization | | | 70.5% | | | | ICU Level of Service | | C | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

91: Garner & Kitty Murray

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|------|-------|------|------|-------|------|------|------|------|
| Lane Configurations | ↘ | ↗↗ | ↘ | ↘ | ↗↗ | ↘ | ↘ | ↗ | ↘ | ↘ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3421 | 1531 | 1711 | 3421 | 1531 | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 |
| Flt Permitted | 0.24 | 1.00 | 1.00 | 0.46 | 1.00 | 1.00 | 0.66 | 1.00 | 1.00 | 0.64 | 1.00 | 1.00 |
| Satd. Flow (perm) | 424 | 3421 | 1531 | 832 | 3421 | 1531 | 1188 | 1801 | 1531 | 1150 | 1801 | 1531 |
| Volume (vph) | 73 | 474 | 23 | 37 | 529 | 46 | 12 | 174 | 78 | 57 | 141 | 105 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 79 | 515 | 25 | 40 | 575 | 50 | 13 | 189 | 85 | 62 | 153 | 114 |
| RTOR Reduction (vph) | 0 | 0 | 16 | 0 | 0 | 37 | 0 | 0 | 44 | 0 | 0 | 59 |
| Lane Group Flow (vph) | 79 | 515 | 9 | 40 | 575 | 13 | 13 | 189 | 41 | 62 | 153 | 55 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 20.1 | 20.1 | 20.1 | 13.9 | 13.9 | 13.9 | 26.5 | 26.5 | 26.5 | 26.5 | 26.5 | 26.5 |
| Effective Green, g (s) | 20.1 | 20.1 | 20.1 | 13.9 | 13.9 | 13.9 | 26.5 | 26.5 | 26.5 | 26.5 | 26.5 | 26.5 |
| Actuated g/C Ratio | 0.37 | 0.37 | 0.37 | 0.25 | 0.25 | 0.25 | 0.49 | 0.49 | 0.49 | 0.49 | 0.49 | 0.49 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 208 | 1259 | 564 | 212 | 871 | 390 | 577 | 874 | 743 | 558 | 874 | 743 |
| v/s Ratio Prot | 0.02 | c0.15 | | | c0.17 | | | c0.10 | | | 0.08 | |
| v/s Ratio Perm | 0.12 | | 0.01 | 0.05 | | 0.01 | 0.01 | | 0.03 | 0.05 | | 0.04 |
| v/c Ratio | 0.38 | 0.41 | 0.02 | 0.19 | 0.66 | 0.03 | 0.02 | 0.22 | 0.06 | 0.11 | 0.18 | 0.07 |
| Uniform Delay, d1 | 12.1 | 12.8 | 11.0 | 15.9 | 18.2 | 15.3 | 7.3 | 8.1 | 7.4 | 7.6 | 7.9 | 7.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.2 | 0.2 | 0.0 | 0.4 | 1.9 | 0.0 | 0.1 | 0.6 | 0.1 | 0.4 | 0.4 | 0.2 |
| Delay (s) | 13.3 | 13.0 | 11.0 | 16.4 | 20.1 | 15.3 | 7.4 | 8.6 | 7.6 | 8.0 | 8.3 | 7.7 |
| Level of Service | B | B | B | B | C | B | A | A | A | A | A | A |
| Approach Delay (s) | | 13.0 | | | 19.5 | | | 8.3 | | | 8.1 | |
| Approach LOS | | B | | | B | | | A | | | A | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 13.7 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.39 | | |
| Actuated Cycle Length (s) | 54.6 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 44.5% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

31: Mohawk/Rosseaux & McNiven

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|-------|------|-------|-------|------|------|------|------|
| Lane Configurations | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1750 | 1842 | 1566 | 1750 | 1842 | 1566 | 1711 | 1842 | 1531 | 1711 | 1775 | |
| Fl _t Permitted | 0.37 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 | 0.74 | 1.00 | 1.00 | 0.73 | 1.00 | |
| Satd. Flow (perm) | 679 | 1842 | 1566 | 167 | 1842 | 1566 | 1325 | 1842 | 1531 | 1310 | 1775 | |
| Volume (vph) | 15 | 607 | 362 | 1043 | 721 | 41 | 654 | 41 | 235 | 15 | 23 | 7 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 16 | 660 | 393 | 1134 | 784 | 45 | 711 | 45 | 255 | 16 | 25 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 109 | 0 | 0 | 15 | 0 | 0 | 167 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 16 | 660 | 284 | 1134 | 784 | 30 | 711 | 45 | 88 | 16 | 28 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 38.1 | 38.1 | 38.1 | 88.1 | 88.1 | 88.1 | 50.3 | 50.3 | 50.3 | 50.3 | 50.3 | |
| Effective Green, g (s) | 40.0 | 40.0 | 40.0 | 90.0 | 90.0 | 90.0 | 52.0 | 52.0 | 52.0 | 52.0 | 52.0 | |
| Actuated g/C Ratio | 0.27 | 0.27 | 0.27 | 0.60 | 0.60 | 0.60 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | |
| Clearance Time (s) | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 | 5.9 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | 3.5 | 2.0 | 3.5 | 3.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 181 | 491 | 418 | 586 | 1105 | 940 | 459 | 639 | 531 | 454 | 615 | |
| v/s Ratio Prot | | 0.36 | | c0.59 | 0.43 | | | 0.02 | | | 0.02 | |
| v/s Ratio Perm | 0.02 | | 0.18 | c0.57 | | 0.02 | c0.54 | | 0.06 | 0.01 | | |
| v/c Ratio | 0.09 | 1.34 | 0.68 | 1.94 | 0.71 | 0.03 | 1.55 | 0.07 | 0.17 | 0.04 | 0.05 | |
| Uniform Delay, d ₁ | 41.3 | 55.0 | 49.3 | 54.2 | 20.9 | 12.2 | 49.0 | 32.8 | 34.0 | 32.4 | 32.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.3 | 168.1 | 4.7 | 427.1 | 2.2 | 0.0 | 257.7 | 0.0 | 0.1 | 0.0 | 0.0 | |
| Delay (s) | 41.6 | 223.1 | 54.0 | 481.3 | 23.1 | 12.2 | 306.7 | 32.8 | 34.0 | 32.4 | 32.5 | |
| Level of Service | D | F | D | F | C | B | F | C | C | C | C | |
| Approach Delay (s) | | 158.2 | | | 287.5 | | | 225.7 | | | 32.5 | |
| Approach LOS | | F | | | F | | | F | | | C | |













Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 235.4 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.78 | | |
| Actuated Cycle Length (s) | 150.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 142.6% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
52: Golf Links & Stone Church

11/12/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑ | | ↑ | | ↑ | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.91 | 0.91 | 1.00 |
| Flt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.99 | 1.00 |
| Satd. Flow (prot) | | 4916 | 1531 | 1711 | 3421 | | 1711 | | 1531 | 1628 | 3403 | 1601 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.25 | | 1.00 | 0.95 | 0.99 | 1.00 |
| Satd. Flow (perm) | | 4916 | 1531 | 1711 | 3421 | | 459 | | 1531 | 1628 | 3403 | 1601 |
| Volume (vph) | 0 | 2377 | 284 | 106 | 741 | 0 | 282 | 0 | 433 | 294 | 402 | 351 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 2584 | 309 | 115 | 805 | 0 | 307 | 0 | 471 | 320 | 437 | 382 |
| RTOR Reduction (vph) | 0 | 0 | 173 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 |
| Lane Group Flow (vph) | 0 | 2584 | 136 | 115 | 805 | 0 | 307 | 0 | 471 | 244 | 513 | 282 |
| Turn Type | | | Perm | Prot | | | custom | | custom | Perm | | Perm |
| Protected Phases | | 6 | | 5 | 2 | | 3 | | 5 | 8 | | 4 |
| Permitted Phases | | | 6 | | | | 8 | | 3 | 4 | 4 | 4 |
| Actuated Green, G (s) | | 42.0 | 42.0 | 4.0 | 51.0 | | 37.0 | | 47.0 | 25.0 | 25.0 | 25.0 |
| Effective Green, g (s) | | 44.0 | 44.0 | 5.0 | 53.0 | | 39.0 | | 48.0 | 27.0 | 27.0 | 27.0 |
| Actuated g/C Ratio | | 0.44 | 0.44 | 0.05 | 0.53 | | 0.39 | | 0.48 | 0.27 | 0.27 | 0.27 |
| Clearance Time (s) | | 6.0 | 6.0 | 5.0 | 6.0 | | 3.0 | | | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | 1.0 | 2.0 | | 1.0 | | | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | | 2163 | 674 | 86 | 1813 | | 279 | | 735 | 440 | 919 | 432 |
| v/s Ratio Prot | | c0.53 | | c0.07 | 0.24 | | c0.09 | | 0.31 | | | |
| v/s Ratio Perm | | | 0.09 | | | | c0.34 | | | 0.15 | 0.15 | 0.18 |
| v/c Ratio | | 1.19 | 0.20 | 1.34 | 0.44 | | 1.10 | | 0.64 | 0.55 | 0.56 | 0.65 |
| Uniform Delay, d1 | | 28.0 | 17.2 | 47.5 | 14.4 | | 28.4 | | 19.5 | 31.3 | 31.4 | 32.3 |
| Progression Factor | | 0.99 | 1.62 | 1.05 | 0.96 | | 1.60 | | 1.59 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 88.0 | 0.1 | 190.3 | 0.5 | | 71.8 | | 0.9 | 0.9 | 0.4 | 2.7 |
| Delay (s) | | 115.9 | 28.0 | 240.3 | 14.4 | | 117.1 | | 32.0 | 32.2 | 31.8 | 35.0 |
| Level of Service | | F | C | F | B | | F | | C | C | C | D |
| Approach Delay (s) | | 106.5 | | | 42.6 | | | 65.6 | | | 33.0 | |
| Approach LOS | | F | | | D | | | E | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 76.1 | | | | HCM Level of Service | | | E | | |
| HCM Volume to Capacity ratio | | | 1.15 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | | Sum of lost time (s) | | 12.0 | | | |
| Intersection Capacity Utilization | | | 107.4% | | | | ICU Level of Service | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

75: Golf Links Rd & Neville

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|------|------|------|------|------|--------|--------|------|
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘ | ↑↑ | ↗ | ↘ | ↑ | | ↗↘ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 0.94 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1655 | | 3319 | 1740 | |
| Fl _t Permitted | 0.23 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.34 | 1.00 | | 0.25 | 1.00 | |
| Satd. Flow (perm) | 409 | 3500 | 1531 | 148 | 3500 | 1531 | 619 | 1655 | | 882 | 1740 | |
| Volume (vph) | 238 | 2342 | 165 | 227 | 808 | 188 | 140 | 118 | 246 | 1124 | 190 | 112 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 259 | 2546 | 179 | 247 | 878 | 204 | 152 | 128 | 267 | 1222 | 207 | 122 |
| RTOR Reduction (vph) | 0 | 0 | 53 | 0 | 0 | 104 | 0 | 75 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 259 | 2546 | 126 | 247 | 878 | 100 | 152 | 320 | 0 | 1222 | 308 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | Perm | | |
| Protected Phases | 1 | 6 | | 5 | 2 | | | 8 | | | 4 | |
| Permitted Phases | 6 | | 6 | 2 | | 2 | 8 | | | 4 | | |
| Actuated Green, G (s) | 58.2 | 48.0 | 48.0 | 55.8 | 46.8 | 46.8 | 28.0 | 28.0 | | 28.0 | 28.0 | |
| Effective Green, g (s) | 59.2 | 50.0 | 50.0 | 56.8 | 48.8 | 48.8 | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Actuated g/C Ratio | 0.59 | 0.50 | 0.50 | 0.57 | 0.49 | 0.49 | 0.30 | 0.30 | | 0.30 | 0.30 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 362 | 1750 | 766 | 209 | 1708 | 747 | 186 | 497 | | 265 | 522 | |
| v/s Ratio Prot | 0.07 | c0.73 | | c0.09 | 0.25 | | | 0.19 | | | 0.18 | |
| v/s Ratio Perm | 0.36 | | 0.08 | 0.58 | | 0.07 | 0.25 | | | c1.39 | | |
| v/c Ratio | 0.72 | 1.45 | 0.16 | 1.18 | 0.51 | 0.13 | 0.82 | 0.64 | | 4.61 | 0.59 | |
| Uniform Delay, d ₁ | 11.8 | 25.0 | 13.6 | 48.2 | 17.5 | 14.0 | 32.5 | 30.4 | | 35.0 | 29.8 | |
| Progression Factor | 1.05 | 0.96 | 0.82 | 1.15 | 1.00 | 1.56 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.5 | 205.0 | 0.0 | 112.6 | 0.8 | 0.3 | 22.4 | 2.1 | | 1633.7 | 1.2 | |
| Delay (s) | 12.9 | 229.0 | 11.3 | 168.0 | 18.4 | 22.1 | 54.8 | 32.5 | | 1668.7 | 31.0 | |
| Level of Service | B | F | B | F | B | C | D | C | | F | C | |
| Approach Delay (s) | | 197.2 | | | 46.8 | | | 38.7 | | | 1321.3 | |
| Approach LOS | | F | | | D | | | D | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 424.4 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 2.40 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 144.0% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

78: Golf Links & McNiven

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|-------|------|------|-------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 0.93 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 | 1711 | 3199 | | 1711 | 1675 | |
| Flt Permitted | 0.65 | 1.00 | 1.00 | 0.28 | 1.00 | 1.00 | 0.44 | 1.00 | | 0.37 | 1.00 | |
| Satd. Flow (perm) | 1168 | 1801 | 1531 | 498 | 1801 | 1531 | 793 | 3199 | | 668 | 1675 | |
| Volume (vph) | 64 | 253 | 142 | 213 | 158 | 469 | 117 | 167 | 128 | 681 | 292 | 255 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 70 | 275 | 154 | 232 | 172 | 510 | 127 | 182 | 139 | 740 | 317 | 277 |
| RTOR Reduction (vph) | 0 | 0 | 120 | 0 | 0 | 333 | 0 | 110 | 0 | 0 | 23 | 0 |
| Lane Group Flow (vph) | 70 | 275 | 34 | 232 | 172 | 177 | 127 | 211 | 0 | 740 | 571 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | pm+pt | | | pm+pt | | |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 19.6 | 19.6 | 19.6 | 31.7 | 31.7 | 31.7 | 25.5 | 17.7 | | 53.3 | 41.5 | |
| Effective Green, g (s) | 21.7 | 21.7 | 21.7 | 33.8 | 33.8 | 33.8 | 27.8 | 20.0 | | 55.6 | 43.8 | |
| Actuated g/C Ratio | 0.22 | 0.22 | 0.22 | 0.35 | 0.35 | 0.35 | 0.29 | 0.21 | | 0.57 | 0.45 | |
| Clearance Time (s) | 6.1 | 6.1 | 6.1 | 4.0 | 6.1 | 6.1 | 4.0 | 6.3 | | 4.0 | 6.3 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 260 | 401 | 341 | 274 | 625 | 531 | 300 | 657 | | 720 | 753 | |
| v/s Ratio Prot | | 0.15 | | c0.07 | 0.10 | | 0.03 | 0.07 | | c0.33 | 0.34 | |
| v/s Ratio Perm | 0.06 | | 0.02 | c0.22 | | 0.12 | 0.09 | | | c0.25 | | |
| v/c Ratio | 0.27 | 0.69 | 0.10 | 0.85 | 0.28 | 0.33 | 0.42 | 0.32 | | 1.03 | 0.76 | |
| Uniform Delay, d1 | 31.3 | 34.7 | 30.1 | 27.5 | 23.0 | 23.5 | 26.9 | 32.9 | | 17.9 | 22.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.6 | 4.8 | 0.1 | 20.8 | 0.2 | 0.4 | 1.0 | 0.3 | | 40.8 | 4.4 | |
| Delay (s) | 31.9 | 39.5 | 30.2 | 48.2 | 23.2 | 23.9 | 27.8 | 33.2 | | 58.7 | 26.8 | |
| Level of Service | C | D | C | D | C | C | C | C | | E | C | |
| Approach Delay (s) | | 35.6 | | | 29.9 | | | 31.7 | | | 44.5 | |
| Approach LOS | | D | | | C | | | C | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 37.1 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.94 | | |
| Actuated Cycle Length (s) | 97.4 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 84.9% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

91: Garner & Kitty Murray

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|------|-------|------|------|------|------|------|-------|------|
| Lane Configurations | ↘ | ↗↗ | ↘ | ↘ | ↗↗ | ↘ | ↘ | ↗ | ↘ | ↘ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3421 | 1531 | 1711 | 3421 | 1531 | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 |
| Flt Permitted | 0.26 | 1.00 | 1.00 | 0.37 | 1.00 | 1.00 | 0.64 | 1.00 | 1.00 | 0.65 | 1.00 | 1.00 |
| Satd. Flow (perm) | 471 | 3421 | 1531 | 658 | 3421 | 1531 | 1159 | 1801 | 1531 | 1165 | 1801 | 1531 |
| Volume (vph) | 96 | 695 | 27 | 40 | 508 | 81 | 32 | 161 | 46 | 40 | 166 | 57 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 104 | 755 | 29 | 43 | 552 | 88 | 35 | 175 | 50 | 43 | 180 | 62 |
| RTOR Reduction (vph) | 0 | 0 | 16 | 0 | 0 | 64 | 0 | 0 | 29 | 0 | 0 | 33 |
| Lane Group Flow (vph) | 104 | 755 | 13 | 43 | 552 | 24 | 35 | 175 | 21 | 43 | 180 | 29 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 25.1 | 25.1 | 25.1 | 15.3 | 15.3 | 15.3 | 23.6 | 23.6 | 23.6 | 23.6 | 23.6 | 23.6 |
| Effective Green, g (s) | 25.1 | 25.1 | 25.1 | 15.3 | 15.3 | 15.3 | 23.6 | 23.6 | 23.6 | 23.6 | 23.6 | 23.6 |
| Actuated g/C Ratio | 0.44 | 0.44 | 0.44 | 0.27 | 0.27 | 0.27 | 0.42 | 0.42 | 0.42 | 0.42 | 0.42 | 0.42 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 335 | 1514 | 678 | 178 | 923 | 413 | 482 | 750 | 637 | 485 | 750 | 637 |
| v/s Ratio Prot | 0.03 | c0.22 | | | c0.16 | | | 0.10 | | | c0.10 | |
| v/s Ratio Perm | 0.11 | | 0.01 | 0.07 | | 0.02 | 0.03 | | 0.01 | 0.04 | | 0.02 |
| v/c Ratio | 0.31 | 0.50 | 0.02 | 0.24 | 0.60 | 0.06 | 0.07 | 0.23 | 0.03 | 0.09 | 0.24 | 0.05 |
| Uniform Delay, d1 | 10.0 | 11.3 | 8.9 | 16.2 | 18.0 | 15.4 | 10.0 | 10.7 | 9.8 | 10.0 | 10.7 | 9.8 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.5 | 0.3 | 0.0 | 0.7 | 1.1 | 0.1 | 0.3 | 0.7 | 0.1 | 0.4 | 0.8 | 0.1 |
| Delay (s) | 10.6 | 11.6 | 8.9 | 16.9 | 19.1 | 15.4 | 10.3 | 11.4 | 9.9 | 10.4 | 11.5 | 10.0 |
| Level of Service | B | B | A | B | B | B | B | B | A | B | B | A |
| Approach Delay (s) | | 11.4 | | | 18.5 | | | 11.0 | | | 11.0 | |
| Approach LOS | | B | | | B | | | B | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 13.6 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.41 | | |
| Actuated Cycle Length (s) | 56.7 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 47.9% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

1: Wilson & Highway 52

11/12/2010

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|------|-------|------|----------------------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 4.0 | 3.3 | 3.3 | 4.0 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1946 | 1531 | 1711 | 1946 | 1531 |
| Flt Permitted | 0.15 | 1.00 | 1.00 | 0.62 | 1.00 | 1.00 | 0.60 | 1.00 | 1.00 | 0.69 | 1.00 | 1.00 |
| Satd. Flow (perm) | 265 | 3500 | 1531 | 1118 | 3500 | 1531 | 1085 | 1946 | 1531 | 1237 | 1946 | 1531 |
| Volume (vph) | 25 | 192 | 105 | 170 | 1070 | 30 | 456 | 100 | 60 | 17 | 204 | 136 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 27 | 209 | 114 | 185 | 1163 | 33 | 496 | 109 | 65 | 18 | 222 | 148 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 0 | 20 | 0 | 0 | 33 | 0 | 0 | 8 |
| Lane Group Flow (vph) | 27 | 209 | 44 | 185 | 1163 | 13 | 496 | 109 | 32 | 18 | 222 | 140 |
| Turn Type | Perm | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 25.2 | 25.2 | 25.2 | 25.2 | 25.2 | 25.2 | 31.8 | 31.8 | 31.8 | 31.8 | 31.8 | 31.8 |
| Effective Green, g (s) | 27.2 | 27.2 | 27.2 | 27.2 | 27.2 | 27.2 | 34.8 | 34.8 | 34.8 | 34.8 | 34.8 | 34.8 |
| Actuated g/C Ratio | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Grp Cap (vph) | 103 | 1360 | 595 | 434 | 1360 | 595 | 539 | 967 | 761 | 615 | 967 | 761 |
| v/s Ratio Prot | | 0.06 | | | c0.33 | | | 0.06 | | | 0.11 | |
| v/s Ratio Perm | 0.10 | | 0.03 | 0.17 | | 0.01 | c0.46 | | 0.02 | 0.01 | | 0.09 |
| v/c Ratio | 0.26 | 0.15 | 0.07 | 0.43 | 0.86 | 0.02 | 0.92 | 0.11 | 0.04 | 0.03 | 0.23 | 0.18 |
| Uniform Delay, d1 | 14.6 | 13.9 | 13.5 | 15.7 | 19.6 | 13.2 | 16.3 | 9.4 | 9.0 | 9.0 | 10.0 | 9.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.81 | 0.88 | 0.59 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 6.1 | 0.2 | 0.2 | 3.0 | 7.0 | 0.1 | 21.4 | 0.1 | 0.0 | 0.0 | 0.2 | 0.2 |
| Delay (s) | 20.7 | 14.2 | 13.7 | 15.7 | 24.2 | 7.8 | 37.7 | 9.4 | 9.1 | 9.0 | 10.2 | 9.9 |
| Level of Service | C | B | B | B | C | A | D | A | A | A | B | A |
| Approach Delay (s) | | 14.5 | | | 22.7 | | | 30.4 | | | 10.0 | |
| Approach LOS | | B | | | C | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.7 | | | | HCM Level of Service | | | | C | |
| HCM Volume to Capacity ratio | | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | | | | Sum of lost time (s) | | | 8.0 | | |
| Intersection Capacity Utilization | | | 87.2% | | | | ICU Level of Service | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

31: Mohawk/Rosseaux & McNiven

11/12/2010













| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | |
|-----------------------------------|------|-------|--------|-------|-------|------|-------|-------|-------|------|------|----------------------|----------------------|---|
| Lane Configurations | | | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | | |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | 1.00 | | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | |
| Satd. Flow (prot) | 1750 | 1842 | 1566 | 1750 | 1842 | 1566 | 1711 | 1842 | 1531 | 1711 | 1742 | 1742 | | |
| Fl _t Permitted | 0.22 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.64 | 1.00 | 1.00 | 0.75 | 1.00 | 1.00 | | |
| Satd. Flow (perm) | 401 | 1842 | 1566 | 139 | 1842 | 1566 | 1147 | 1842 | 1531 | 1343 | 1742 | 1742 | | |
| Volume (vph) | 4 | 831 | 425 | 215 | 568 | 7 | 399 | 17 | 1213 | 40 | 32 | 18 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | |
| Adj. Flow (vph) | 4 | 903 | 462 | 234 | 617 | 8 | 434 | 18 | 1318 | 43 | 35 | 20 | | |
| RTOR Reduction (vph) | 0 | 0 | 100 | 0 | 0 | 4 | 0 | 0 | 109 | 0 | 16 | 0 | | |
| Lane Group Flow (vph) | 4 | 903 | 362 | 234 | 617 | 4 | 434 | 18 | 1209 | 43 | 39 | 0 | | |
| Turn Type | Perm | | Perm | pm+pt | | Perm | pm+pt | | Perm | Perm | | | | |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 8 | | | | 4 | | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | | | |
| Actuated Green, G (s) | 47.1 | 47.1 | 47.1 | 60.1 | 60.1 | 60.1 | 69.4 | 69.4 | 69.4 | 28.5 | 28.5 | | | |
| Effective Green, g (s) | 49.0 | 49.0 | 49.0 | 62.0 | 62.0 | 62.0 | 71.1 | 71.1 | 71.1 | 30.2 | 30.2 | | | |
| Actuated g/C Ratio | 0.35 | 0.35 | 0.35 | 0.44 | 0.44 | 0.44 | 0.50 | 0.50 | 0.50 | 0.21 | 0.21 | | | |
| Clearance Time (s) | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 | 5.9 | 4.0 | 5.7 | 5.7 | 5.7 | 5.7 | | | |
| Vehicle Extension (s) | 3.5 | 3.5 | 3.5 | 2.0 | 3.5 | 3.5 | 3.0 | 2.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | 139 | 640 | 544 | 164 | 809 | 688 | 725 | 928 | 771 | 287 | 373 | | | |
| v/s Ratio Prot | | 0.49 | | c0.09 | 0.33 | | 0.16 | 0.01 | | | 0.02 | | | |
| v/s Ratio Perm | 0.01 | | 0.23 | c0.54 | | 0.00 | 0.15 | | c0.79 | 0.03 | | | | |
| v/c Ratio | 0.03 | 1.41 | 0.67 | 1.43 | 0.76 | 0.01 | 0.60 | 0.02 | 1.57 | 0.15 | 0.11 | | | |
| Uniform Delay, d ₁ | 30.4 | 46.0 | 39.1 | 68.2 | 33.3 | 22.2 | 23.4 | 17.5 | 35.0 | 45.0 | 44.6 | | | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d ₂ | 0.1 | 194.1 | 3.2 | 223.6 | 4.4 | 0.0 | 1.3 | 0.0 | 262.1 | 0.1 | 0.0 | | | |
| Delay (s) | 30.5 | 240.2 | 42.3 | 291.8 | 37.8 | 22.2 | 24.7 | 17.5 | 297.1 | 45.1 | 44.6 | | | |
| Level of Service | C | F | D | F | D | C | C | B | F | D | D | | | |
| Approach Delay (s) | | 172.8 | | | 106.8 | | | 227.5 | | | 44.8 | | | |
| Approach LOS | | F | | | F | | | F | | | D | | | |
| Intersection Summary | | | | | | | | | | | | | | |
| HCM Average Control Delay | | | 179.5 | | | | | | | | | HCM Level of Service | F | |
| HCM Volume to Capacity ratio | | | 1.49 | | | | | | | | | | | |
| Actuated Cycle Length (s) | | | 141.1 | | | | | | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 137.2% | | | | | | | | | | ICU Level of Service | H |
| Analysis Period (min) | | | 15 | | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

52: Golf Links & Stone Church

11/12/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑ | | ↑ | | ↑ | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.91 | 0.91 | 1.00 |
| Flt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.98 | 1.00 |
| Satd. Flow (prot) | | 4916 | 1531 | 1711 | 3421 | | 1711 | | 1531 | 1628 | 3348 | 1601 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.39 | | 1.00 | 0.95 | 0.98 | 1.00 |
| Satd. Flow (perm) | | 4916 | 1531 | 1711 | 3421 | | 700 | | 1531 | 1628 | 3348 | 1601 |
| Volume (vph) | 0 | 845 | 112 | 243 | 1202 | 0 | 301 | 0 | 327 | 313 | 173 | 236 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 918 | 122 | 264 | 1307 | 0 | 327 | 0 | 355 | 340 | 188 | 257 |
| RTOR Reduction (vph) | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 37 |
| Lane Group Flow (vph) | 0 | 918 | 37 | 264 | 1307 | 0 | 327 | 0 | 350 | 170 | 358 | 220 |
| Turn Type | | | Perm | Prot | | custom | | custom | | Perm | | Perm |
| Protected Phases | | 6 | | 5 | 2 | | 3 | | 5 | | 4 | |
| Permitted Phases | | | 6 | | | | 8 | | 3 | 4 | 4 | 4 |
| Actuated Green, G (s) | | 25.3 | 25.3 | 13.0 | 43.3 | | 34.7 | | 53.7 | 23.7 | 23.7 | 23.7 |
| Effective Green, g (s) | | 27.3 | 27.3 | 14.0 | 45.3 | | 36.7 | | 54.7 | 25.7 | 25.7 | 25.7 |
| Actuated g/C Ratio | | 0.30 | 0.30 | 0.16 | 0.50 | | 0.41 | | 0.61 | 0.29 | 0.29 | 0.29 |
| Clearance Time (s) | | 6.0 | 6.0 | 5.0 | 6.0 | | 3.0 | | | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | 1.0 | 2.0 | | 1.0 | | | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | | 1491 | 464 | 266 | 1722 | | 364 | | 931 | 465 | 956 | 457 |
| v/s Ratio Prot | | 0.19 | | c0.15 | c0.38 | | c0.07 | | 0.23 | | | |
| v/s Ratio Perm | | | 0.02 | | | | c0.30 | | | 0.10 | 0.11 | 0.14 |
| v/c Ratio | | 0.62 | 0.08 | 0.99 | 0.76 | | 0.90 | | 0.38 | 0.37 | 0.37 | 0.48 |
| Uniform Delay, d1 | | 26.9 | 22.4 | 37.9 | 18.0 | | 24.1 | | 9.0 | 25.6 | 25.7 | 26.6 |
| Progression Factor | | 1.23 | 1.87 | 1.04 | 1.28 | | 1.09 | | 1.13 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.7 | 0.3 | 41.5 | 2.0 | | 23.2 | | 0.1 | 0.2 | 0.1 | 0.3 |
| Delay (s) | | 34.7 | 42.2 | 81.2 | 25.0 | | 49.6 | | 10.2 | 25.8 | 25.8 | 26.9 |
| Level of Service | | C | D | F | C | | D | | B | C | C | C |
| Approach Delay (s) | | 35.6 | | | 34.4 | | | 29.1 | | | 26.2 | |
| Approach LOS | | D | | | C | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 32.3 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.84 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 74.5% | | | ICU Level of Service | | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

75: Golf Links Rd & Neville

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|-------|-------|------|------|------|------|-------|------|------|
| Lane Configurations | ↙ | ↑↑ | ↗ | ↙ | ↑↑ | ↗ | ↙ | ↑ | | ↗↘ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Flt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | | 1.00 | 0.93 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1629 | | 3319 | 1715 | |
| Flt Permitted | 0.07 | 1.00 | 1.00 | 0.31 | 1.00 | 1.00 | 0.63 | 1.00 | | 0.40 | 1.00 | |
| Satd. Flow (perm) | 134 | 3500 | 1531 | 565 | 3500 | 1531 | 1136 | 1629 | | 1410 | 1715 | |
| Volume (vph) | 53 | 690 | 22 | 125 | 1525 | 148 | 115 | 50 | 167 | 279 | 63 | 53 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 58 | 750 | 24 | 136 | 1658 | 161 | 125 | 54 | 182 | 303 | 68 | 58 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 55 | 0 | 143 | 0 | 0 | 42 | 0 |
| Lane Group Flow (vph) | 58 | 750 | 14 | 136 | 1658 | 106 | 125 | 93 | 0 | 303 | 84 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | Perm | | |
| Protected Phases | 1 | 6 | | 5 | 2 | | | 8 | | | 4 | |
| Permitted Phases | 6 | | 6 | 2 | | 2 | 8 | | | 4 | | |
| Actuated Green, G (s) | 55.7 | 51.6 | 51.6 | 59.3 | 53.4 | 53.4 | 17.5 | 17.5 | | 17.5 | 17.5 | |
| Effective Green, g (s) | 56.7 | 53.6 | 53.6 | 60.3 | 55.4 | 55.4 | 19.5 | 19.5 | | 19.5 | 19.5 | |
| Actuated g/C Ratio | 0.63 | 0.60 | 0.60 | 0.67 | 0.62 | 0.62 | 0.22 | 0.22 | | 0.22 | 0.22 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 139 | 2084 | 912 | 441 | 2154 | 942 | 246 | 353 | | 306 | 372 | |
| v/s Ratio Prot | 0.01 | 0.21 | | c0.02 | c0.47 | | | 0.06 | | | 0.05 | |
| v/s Ratio Perm | 0.25 | | 0.01 | 0.19 | | 0.07 | 0.11 | | | c0.21 | | |
| v/c Ratio | 0.42 | 0.36 | 0.02 | 0.31 | 0.77 | 0.11 | 0.51 | 0.26 | | 0.99 | 0.23 | |
| Uniform Delay, d1 | 11.5 | 9.4 | 7.4 | 5.8 | 12.6 | 7.1 | 31.0 | 29.3 | | 35.2 | 29.0 | |
| Progression Factor | 1.15 | 0.99 | 0.92 | 0.67 | 0.95 | 0.65 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.7 | 0.5 | 0.0 | 0.1 | 1.8 | 0.2 | 0.6 | 0.1 | | 48.6 | 0.1 | |
| Delay (s) | 13.8 | 9.7 | 6.9 | 4.0 | 13.9 | 4.8 | 31.6 | 29.4 | | 83.7 | 29.2 | |
| Level of Service | B | A | A | A | B | A | C | C | | F | C | |
| Approach Delay (s) | | 9.9 | | | 12.4 | | | 30.2 | | | 67.7 | |
| Approach LOS | | A | | | B | | | C | | | E | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 20.3 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.81 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 80.9% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

78: Golf Links & McNiven

11/12/2010

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|------|------|----------------------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 | 1711 | 3285 | | 1711 | 1747 | |
| Flt Permitted | 0.29 | 1.00 | 1.00 | 0.66 | 1.00 | 1.00 | 0.60 | 1.00 | | 0.20 | 1.00 | |
| Satd. Flow (perm) | 514 | 1801 | 1531 | 1197 | 1801 | 1531 | 1082 | 3285 | | 368 | 1747 | |
| Volume (vph) | 302 | 133 | 125 | 82 | 244 | 543 | 80 | 385 | 139 | 331 | 189 | 47 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 328 | 145 | 136 | 89 | 265 | 590 | 87 | 418 | 151 | 360 | 205 | 51 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 0 | 349 | 0 | 31 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 328 | 145 | 58 | 89 | 265 | 241 | 87 | 538 | 0 | 360 | 249 | 0 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | pm+pt | | | pm+pt | | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 41.5 | 41.5 | 41.5 | 20.4 | 20.4 | 20.4 | 25.7 | 22.7 | | 48.6 | 41.6 | |
| Effective Green, g (s) | 43.6 | 43.6 | 43.6 | 22.5 | 22.5 | 22.5 | 28.0 | 25.0 | | 50.9 | 43.9 | |
| Actuated g/C Ratio | 0.43 | 0.43 | 0.43 | 0.22 | 0.22 | 0.22 | 0.27 | 0.24 | | 0.50 | 0.43 | |
| Clearance Time (s) | 4.0 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 4.0 | 6.3 | | 4.0 | 6.3 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 418 | 766 | 651 | 263 | 395 | 336 | 314 | 801 | | 470 | 748 | |
| v/s Ratio Prot | c0.13 | 0.08 | | | 0.15 | | 0.01 | 0.16 | | c0.16 | 0.14 | |
| v/s Ratio Perm | c0.20 | | 0.04 | 0.07 | | 0.16 | 0.07 | | | c0.22 | | |
| v/c Ratio | 0.78 | 0.19 | 0.09 | 0.34 | 0.67 | 0.72 | 0.28 | 0.67 | | 0.77 | 0.33 | |
| Uniform Delay, d1 | 22.3 | 18.4 | 17.6 | 33.7 | 36.6 | 37.1 | 28.6 | 35.0 | | 18.6 | 19.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 9.3 | 0.1 | 0.1 | 0.8 | 4.4 | 7.1 | 0.5 | 2.2 | | 7.3 | 0.3 | |
| Delay (s) | 31.6 | 18.5 | 17.6 | 34.5 | 41.0 | 44.2 | 29.1 | 37.3 | | 25.9 | 19.8 | |
| Level of Service | C | B | B | C | D | D | C | D | | C | B | |
| Approach Delay (s) | | 25.4 | | | 42.4 | | | 36.2 | | | 23.4 | |
| Approach LOS | | C | | | D | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 33.1 | | | | HCM Level of Service | | | | C | |
| HCM Volume to Capacity ratio | | | 0.76 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 102.5 | | | | Sum of lost time (s) | | | | 8.0 | |
| Intersection Capacity Utilization | | | 76.3% | | | | ICU Level of Service | | | | D | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

90: Garner & Southcote

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|-------|------|------|------|-------|------|-------|-------|------|
| Lane Configurations | ↙ | ↗↗ | ↗ | ↙ | ↗↗ | ↗ | ↙ | ↗↗ | | ↙ | ↗↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.0 | 3.5 | 3.3 | 3.0 | 3.5 | 3.3 | 3.3 | 3.3 | 3.3 | 3.0 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 0.92 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1652 | 3500 | 1531 | 1652 | 3500 | 1531 | 1711 | 3266 | | 1652 | 3228 | |
| Fl _t Permitted | 0.20 | 1.00 | 1.00 | 0.26 | 1.00 | 1.00 | 0.47 | 1.00 | | 0.26 | 1.00 | |
| Satd. Flow (perm) | 346 | 3500 | 1531 | 455 | 3500 | 1531 | 850 | 3266 | | 460 | 3228 | |
| Volume (vph) | 297 | 991 | 37 | 59 | 650 | 138 | 20 | 290 | 125 | 72 | 218 | 235 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 323 | 1077 | 40 | 64 | 707 | 150 | 22 | 315 | 136 | 78 | 237 | 255 |
| RTOR Reduction (vph) | 0 | 0 | 20 | 0 | 0 | 102 | 0 | 48 | 0 | 0 | 171 | 0 |
| Lane Group Flow (vph) | 323 | 1077 | 20 | 64 | 707 | 48 | 22 | 403 | 0 | 78 | 321 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | pm+pt | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 44.7 | 38.6 | 38.6 | 26.2 | 24.1 | 24.1 | 15.2 | 15.2 | | 24.9 | 24.9 | |
| Effective Green, g (s) | 46.7 | 40.6 | 40.6 | 28.2 | 26.1 | 26.1 | 17.2 | 17.2 | | 26.9 | 26.9 | |
| Actuated g/C Ratio | 0.57 | 0.50 | 0.50 | 0.35 | 0.32 | 0.32 | 0.21 | 0.21 | | 0.33 | 0.33 | |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 464 | 1741 | 762 | 188 | 1119 | 490 | 179 | 688 | | 235 | 1064 | |
| v/s Ratio Prot | c0.14 | 0.31 | | 0.01 | 0.20 | | | c0.12 | | 0.02 | c0.10 | |
| v/s Ratio Perm | c0.26 | | 0.01 | 0.11 | | 0.03 | 0.03 | | | 0.09 | | |
| v/c Ratio | 0.70 | 0.62 | 0.03 | 0.34 | 0.63 | 0.10 | 0.12 | 0.59 | | 0.33 | 0.30 | |
| Uniform Delay, d ₁ | 11.8 | 14.9 | 10.4 | 18.2 | 23.7 | 19.5 | 26.1 | 29.0 | | 19.9 | 20.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 4.5 | 0.9 | 0.0 | 1.1 | 1.5 | 0.2 | 0.3 | 1.3 | | 0.8 | 0.2 | |
| Delay (s) | 16.3 | 15.7 | 10.5 | 19.3 | 25.1 | 19.6 | 26.4 | 30.3 | | 20.7 | 20.5 | |
| Level of Service | B | B | B | B | C | B | C | C | | C | C | |
| Approach Delay (s) | | 15.7 | | | 23.8 | | | 30.1 | | | 20.5 | |
| Approach LOS | | B | | | C | | | C | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 20.7 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.63 | | |
| Actuated Cycle Length (s) | 81.6 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 69.7% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

91: Garner & Kitty Murray

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↘ | ↗↗ | ↘ | ↘ | ↗↗ | ↘ | ↘ | ↗ | ↘ | ↘ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3421 | 1531 | 1711 | 3421 | 1531 | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 |
| Flt Permitted | 0.20 | 1.00 | 1.00 | 0.40 | 1.00 | 1.00 | 0.59 | 1.00 | 1.00 | 0.51 | 1.00 | 1.00 |
| Satd. Flow (perm) | 353 | 3421 | 1531 | 724 | 3421 | 1531 | 1062 | 1801 | 1531 | 912 | 1801 | 1531 |
| Volume (vph) | 400 | 604 | 37 | 59 | 672 | 56 | 20 | 290 | 125 | 81 | 218 | 147 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 435 | 657 | 40 | 64 | 730 | 61 | 22 | 315 | 136 | 88 | 237 | 160 |
| RTOR Reduction (vph) | 0 | 0 | 23 | 0 | 0 | 42 | 0 | 0 | 75 | 0 | 0 | 82 |
| Lane Group Flow (vph) | 435 | 657 | 17 | 64 | 730 | 19 | 22 | 315 | 61 | 88 | 237 | 78 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 24.4 | 24.4 | 24.4 | 16.4 | 16.4 | 16.4 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |
| Effective Green, g (s) | 24.4 | 24.4 | 24.4 | 16.4 | 16.4 | 16.4 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |
| Actuated g/C Ratio | 0.42 | 0.42 | 0.42 | 0.28 | 0.28 | 0.28 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 241 | 1429 | 640 | 203 | 961 | 430 | 473 | 802 | 682 | 406 | 802 | 682 |
| v/s Ratio Prot | c0.12 | 0.19 | | | 0.21 | | | c0.17 | | | 0.13 | |
| v/s Ratio Perm | c0.63 | | 0.01 | 0.09 | | 0.01 | 0.02 | | 0.04 | 0.10 | | 0.05 |
| v/c Ratio | 1.80 | 0.46 | 0.03 | 0.32 | 0.76 | 0.04 | 0.05 | 0.39 | 0.09 | 0.22 | 0.30 | 0.12 |
| Uniform Delay, d1 | 16.0 | 12.3 | 10.0 | 16.6 | 19.2 | 15.3 | 9.2 | 10.9 | 9.4 | 9.9 | 10.3 | 9.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 378.3 | 0.2 | 0.0 | 0.9 | 3.5 | 0.0 | 0.2 | 1.4 | 0.3 | 1.2 | 0.9 | 0.3 |
| Delay (s) | 394.3 | 12.5 | 10.0 | 17.5 | 22.7 | 15.3 | 9.4 | 12.3 | 9.6 | 11.2 | 11.3 | 9.8 |
| Level of Service | F | B | B | B | C | B | A | B | A | B | B | A |
| Approach Delay (s) | | 159.1 | | | 21.8 | | | 11.4 | | | 10.8 | |
| Approach LOS | | F | | | C | | | B | | | B | |



























Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 71.1 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.04 | | |
| Actuated Cycle Length (s) | 58.4 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 73.8% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

1: Wilson & Highway 52

11/12/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|--|---|---|--|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |   |  |  |   |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 4.0 | 3.3 | 3.3 | 4.0 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1946 | 1531 | 1711 | 1946 | 1531 |
| Flt Permitted | 0.56 | 1.00 | 1.00 | 0.16 | 1.00 | 1.00 | 0.64 | 1.00 | 1.00 | 0.34 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1017 | 3500 | 1531 | 293 | 3500 | 1531 | 1148 | 1946 | 1531 | 614 | 1946 | 1531 |
| Volume (vph) | 174 | 1081 | 498 | 92 | 282 | 34 | 199 | 351 | 216 | 21 | 149 | 39 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 189 | 1175 | 541 | 100 | 307 | 37 | 216 | 382 | 235 | 23 | 162 | 42 |
| RTOR Reduction (vph) | 0 | 0 | 243 | 0 | 0 | 17 | 0 | 0 | 23 | 0 | 0 | 28 |
| Lane Group Flow (vph) | 189 | 1175 | 298 | 100 | 307 | 20 | 216 | 382 | 212 | 23 | 162 | 14 |
| Turn Type | Perm | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 2 | | | 6 | | | 8 | | | | 4 |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 36.5 | 36.5 | 36.5 | 36.5 | 36.5 | 36.5 | 20.5 | 20.5 | 20.5 | 20.5 | 20.5 | 20.5 |
| Effective Green, g (s) | 38.5 | 38.5 | 38.5 | 38.5 | 38.5 | 38.5 | 23.5 | 23.5 | 23.5 | 23.5 | 23.5 | 23.5 |
| Actuated g/C Ratio | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.34 | 0.34 | 0.34 | 0.34 | 0.34 | 0.34 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Grp Cap (vph) | 559 | 1925 | 842 | 161 | 1925 | 842 | 385 | 653 | 514 | 206 | 653 | 514 |
| v/s Ratio Prot | | 0.34 | | | 0.09 | | | c0.20 | | | 0.08 | |
| v/s Ratio Perm | 0.19 | | 0.19 | c0.34 | | 0.01 | 0.19 | | 0.14 | 0.04 | | 0.01 |
| v/c Ratio | 0.34 | 0.61 | 0.35 | 0.62 | 0.16 | 0.02 | 0.56 | 0.58 | 0.41 | 0.11 | 0.25 | 0.03 |
| Uniform Delay, d1 | 8.7 | 10.7 | 8.8 | 10.8 | 7.8 | 7.2 | 19.0 | 19.2 | 17.9 | 16.0 | 16.8 | 15.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.63 | 0.38 | 0.11 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.6 | 1.5 | 1.2 | 14.8 | 0.2 | 0.0 | 2.3 | 1.6 | 0.7 | 0.3 | 0.3 | 0.0 |
| Delay (s) | 10.3 | 12.1 | 10.0 | 21.6 | 3.1 | 0.8 | 21.3 | 20.8 | 18.7 | 16.4 | 17.1 | 15.6 |
| Level of Service | B | B | A | C | A | A | C | C | B | B | B | B |
| Approach Delay (s) | | 11.3 | | | 7.1 | | | 20.3 | | | 16.8 | |
| Approach LOS | | B | | | A | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 13.3 | | | | HCM Level of Service | | | | B | |
| HCM Volume to Capacity ratio | | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | | | | Sum of lost time (s) | | | | 8.0 | |
| Intersection Capacity Utilization | | | 78.4% | | | | ICU Level of Service | | | | D | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

31: Mohawk/Rosseaux & McNiven

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|-------|------|-------|-------|------|------|------|------|
| Lane Configurations | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1750 | 1842 | 1566 | 1750 | 1842 | 1566 | 1711 | 1842 | 1531 | 1711 | 1781 | |
| Fl _t Permitted | 0.37 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 | 0.73 | 1.00 | 1.00 | 0.73 | 1.00 | |
| Satd. Flow (perm) | 676 | 1842 | 1566 | 180 | 1842 | 1566 | 1321 | 1842 | 1531 | 1306 | 1781 | |
| Volume (vph) | 15 | 582 | 452 | 1116 | 726 | 43 | 756 | 45 | 238 | 16 | 26 | 7 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 16 | 633 | 491 | 1213 | 789 | 47 | 822 | 49 | 259 | 17 | 28 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 141 | 0 | 0 | 16 | 0 | 0 | 162 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 16 | 633 | 350 | 1213 | 789 | 31 | 822 | 49 | 97 | 17 | 31 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 35.1 | 35.1 | 35.1 | 84.1 | 84.1 | 84.1 | 54.3 | 54.3 | 54.3 | 54.3 | 54.3 | 54.3 |
| Effective Green, g (s) | 37.0 | 37.0 | 37.0 | 86.0 | 86.0 | 86.0 | 56.0 | 56.0 | 56.0 | 56.0 | 56.0 | 56.0 |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.25 | 0.57 | 0.57 | 0.57 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 |
| Clearance Time (s) | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 | 5.9 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| Vehicle Extension (s) | 3.5 | 3.5 | 3.5 | 2.0 | 3.5 | 3.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 167 | 454 | 386 | 574 | 1056 | 898 | 493 | 688 | 572 | 488 | 665 | |
| v/s Ratio Prot | | 0.34 | | c0.63 | 0.43 | | | 0.03 | | | 0.02 | |
| v/s Ratio Perm | 0.02 | | 0.22 | c0.58 | | 0.02 | c0.62 | | 0.06 | 0.01 | | |
| v/c Ratio | 0.10 | 1.39 | 0.91 | 2.11 | 0.75 | 0.03 | 1.67 | 0.07 | 0.17 | 0.03 | 0.05 | |
| Uniform Delay, d ₁ | 43.6 | 56.5 | 54.8 | 54.7 | 23.9 | 13.9 | 47.0 | 30.3 | 31.4 | 29.8 | 30.0 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.3 | 190.5 | 24.6 | 506.8 | 3.0 | 0.0 | 309.2 | 0.0 | 0.1 | 0.0 | 0.0 | |
| Delay (s) | 43.9 | 247.0 | 79.5 | 561.5 | 26.9 | 13.9 | 356.2 | 30.3 | 31.5 | 29.9 | 30.0 | |
| Level of Service | D | F | E | F | C | B | F | C | C | C | C | |
| Approach Delay (s) | | 172.0 | | | 343.1 | | | 267.6 | | | 29.9 | |
| Approach LOS | | F | | | F | | | F | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 275.2 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.92 | | |
| Actuated Cycle Length (s) | 150.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 151.0% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

52: Golf Links & Stone Church

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|-------|------|--------|-------|--------|------|------|------|------|
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑ | | ↑ | | ↑ | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.91 | 0.91 | 1.00 |
| Flt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.99 | 1.00 |
| Satd. Flow (prot) | | 4916 | 1531 | 1711 | 3421 | | 1711 | | 1531 | 1628 | 3403 | 1601 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.25 | | 1.00 | 0.95 | 0.99 | 1.00 |
| Satd. Flow (perm) | | 4916 | 1531 | 1711 | 3421 | | 459 | | 1531 | 1628 | 3403 | 1601 |
| Volume (vph) | 0 | 2377 | 284 | 106 | 741 | 0 | 282 | 0 | 433 | 294 | 402 | 351 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 2584 | 309 | 115 | 805 | 0 | 307 | 0 | 471 | 320 | 437 | 382 |
| RTOR Reduction (vph) | 0 | 0 | 173 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 |
| Lane Group Flow (vph) | 0 | 2584 | 136 | 115 | 805 | 0 | 307 | 0 | 471 | 244 | 513 | 282 |
| Turn Type | | | Perm | Prot | | custom | | custom | | Perm | | Perm |
| Protected Phases | | 6 | | 5 | 2 | | 3 | | 5 | 8 | | 4 |
| Permitted Phases | | | 6 | | | | 8 | | 3 | | 4 | 4 |
| Actuated Green, G (s) | | 42.0 | 42.0 | 4.0 | 51.0 | | 37.0 | | 47.0 | 25.0 | 25.0 | 25.0 |
| Effective Green, g (s) | | 44.0 | 44.0 | 5.0 | 53.0 | | 39.0 | | 48.0 | 27.0 | 27.0 | 27.0 |
| Actuated g/C Ratio | | 0.44 | 0.44 | 0.05 | 0.53 | | 0.39 | | 0.48 | 0.27 | 0.27 | 0.27 |
| Clearance Time (s) | | 6.0 | 6.0 | 5.0 | 6.0 | | 3.0 | | | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | 1.0 | 2.0 | | 1.0 | | | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | | 2163 | 674 | 86 | 1813 | | 279 | | 735 | 440 | 919 | 432 |
| v/s Ratio Prot | | c0.53 | | c0.07 | 0.24 | | c0.09 | | 0.31 | | | |
| v/s Ratio Perm | | | 0.09 | | | | c0.34 | | | 0.15 | 0.15 | 0.18 |
| v/c Ratio | | 1.19 | 0.20 | 1.34 | 0.44 | | 1.10 | | 0.64 | 0.55 | 0.56 | 0.65 |
| Uniform Delay, d1 | | 28.0 | 17.2 | 47.5 | 14.4 | | 28.4 | | 19.5 | 31.3 | 31.4 | 32.3 |
| Progression Factor | | 0.99 | 1.62 | 1.05 | 0.96 | | 1.60 | | 1.59 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 88.0 | 0.1 | 190.3 | 0.5 | | 71.8 | | 0.9 | 0.9 | 0.4 | 2.7 |
| Delay (s) | | 115.9 | 28.0 | 240.3 | 14.4 | | 117.1 | | 32.0 | 32.2 | 31.8 | 35.0 |
| Level of Service | | F | C | F | B | | F | | C | C | C | D |
| Approach Delay (s) | | 106.5 | | | 42.6 | | | 65.6 | | | 33.0 | |
| Approach LOS | | F | | | D | | | E | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|------|
| HCM Average Control Delay | 76.1 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.15 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 107.4% | ICU Level of Service | G |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

75: Golf Links Rd & Neville

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|-------|------|------|------|------|------|--------|--------|------|
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘ | ↑↑ | ↗ | ↘ | ↗ | | ↗↘ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Flt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 0.94 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1655 | | 3319 | 1740 | |
| Flt Permitted | 0.23 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.34 | 1.00 | | 0.25 | 1.00 | |
| Satd. Flow (perm) | 409 | 3500 | 1531 | 148 | 3500 | 1531 | 619 | 1655 | | 882 | 1740 | |
| Volume (vph) | 238 | 2342 | 165 | 227 | 808 | 188 | 140 | 118 | 246 | 1124 | 190 | 112 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 259 | 2546 | 179 | 247 | 878 | 204 | 152 | 128 | 267 | 1222 | 207 | 122 |
| RTOR Reduction (vph) | 0 | 0 | 53 | 0 | 0 | 104 | 0 | 75 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 259 | 2546 | 126 | 247 | 878 | 100 | 152 | 320 | 0 | 1222 | 308 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | Perm | | |
| Protected Phases | 1 | 6 | | 5 | 2 | | | 8 | | | 4 | |
| Permitted Phases | 6 | | 6 | 2 | | 2 | 8 | | | 4 | | |
| Actuated Green, G (s) | 58.2 | 48.0 | 48.0 | 55.8 | 46.8 | 46.8 | 28.0 | 28.0 | | 28.0 | 28.0 | |
| Effective Green, g (s) | 59.2 | 50.0 | 50.0 | 56.8 | 48.8 | 48.8 | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Actuated g/C Ratio | 0.59 | 0.50 | 0.50 | 0.57 | 0.49 | 0.49 | 0.30 | 0.30 | | 0.30 | 0.30 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 362 | 1750 | 766 | 209 | 1708 | 747 | 186 | 497 | | 265 | 522 | |
| v/s Ratio Prot | 0.07 | c0.73 | | c0.09 | 0.25 | | | 0.19 | | | 0.18 | |
| v/s Ratio Perm | 0.36 | | 0.08 | 0.58 | | 0.07 | 0.25 | | | c1.39 | | |
| v/c Ratio | 0.72 | 1.45 | 0.16 | 1.18 | 0.51 | 0.13 | 0.82 | 0.64 | | 4.61 | 0.59 | |
| Uniform Delay, d1 | 11.8 | 25.0 | 13.6 | 48.2 | 17.5 | 14.0 | 32.5 | 30.4 | | 35.0 | 29.8 | |
| Progression Factor | 1.05 | 0.96 | 0.82 | 1.15 | 1.00 | 1.56 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.5 | 205.0 | 0.0 | 112.6 | 0.8 | 0.3 | 22.4 | 2.1 | | 1633.7 | 1.2 | |
| Delay (s) | 12.9 | 229.0 | 11.3 | 168.0 | 18.4 | 22.1 | 54.8 | 32.5 | | 1668.7 | 31.0 | |
| Level of Service | B | F | B | F | B | C | D | C | | F | C | |
| Approach Delay (s) | | 197.2 | | | 46.8 | | | 38.7 | | | 1321.3 | |
| Approach LOS | | F | | | D | | | D | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 424.4 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 2.40 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 144.0% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

78: Golf Links & McNiven

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|-------|------|------|-------|------|------|-------|------|------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑ | | ↖ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 0.94 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 | 1711 | 3226 | | 1711 | 1701 | |
| Flt Permitted | 0.62 | 1.00 | 1.00 | 0.15 | 1.00 | 1.00 | 0.24 | 1.00 | | 0.35 | 1.00 | |
| Satd. Flow (perm) | 1117 | 1801 | 1531 | 266 | 1801 | 1531 | 426 | 3226 | | 632 | 1701 | |
| Volume (vph) | 52 | 349 | 129 | 213 | 203 | 603 | 180 | 209 | 128 | 752 | 408 | 236 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 57 | 379 | 140 | 232 | 221 | 655 | 196 | 227 | 139 | 817 | 443 | 257 |
| RTOR Reduction (vph) | 0 | 0 | 106 | 0 | 0 | 423 | 0 | 85 | 0 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 57 | 379 | 34 | 232 | 221 | 232 | 196 | 281 | 0 | 817 | 681 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | pm+pt | | | pm+pt | | |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 23.8 | 23.8 | 23.8 | 35.9 | 35.9 | 35.9 | 31.4 | 22.5 | | 58.8 | 45.9 | |
| Effective Green, g (s) | 25.9 | 25.9 | 25.9 | 38.0 | 38.0 | 38.0 | 33.7 | 24.8 | | 61.1 | 48.2 | |
| Actuated g/C Ratio | 0.24 | 0.24 | 0.24 | 0.35 | 0.35 | 0.35 | 0.31 | 0.23 | | 0.57 | 0.45 | |
| Clearance Time (s) | 6.1 | 6.1 | 6.1 | 4.0 | 6.1 | 6.1 | 4.0 | 6.3 | | 4.0 | 6.3 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 270 | 436 | 370 | 204 | 639 | 543 | 241 | 747 | | 686 | 766 | |
| v/s Ratio Prot | | 0.21 | | c0.09 | 0.12 | | 0.07 | 0.09 | | c0.36 | 0.40 | |
| v/s Ratio Perm | 0.05 | | 0.02 | c0.32 | | 0.15 | 0.19 | | | c0.32 | | |
| v/c Ratio | 0.21 | 0.87 | 0.09 | 1.14 | 0.35 | 0.43 | 0.81 | 0.38 | | 1.19 | 0.89 | |
| Uniform Delay, d1 | 32.4 | 39.0 | 31.5 | 30.5 | 25.4 | 26.3 | 29.7 | 34.6 | | 19.7 | 27.0 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.4 | 16.6 | 0.1 | 104.8 | 0.3 | 0.5 | 18.5 | 0.3 | | 100.0 | 12.2 | |
| Delay (s) | 32.8 | 55.6 | 31.6 | 135.4 | 25.7 | 26.8 | 48.2 | 35.0 | | 119.7 | 39.2 | |
| Level of Service | C | E | C | F | C | C | D | C | | F | D | |
| Approach Delay (s) | | 47.5 | | | 49.3 | | | 39.6 | | | 82.5 | |
| Approach LOS | | D | | | D | | | D | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 61.0 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.15 | | |
| Actuated Cycle Length (s) | 107.1 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 95.0% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

90: Garner & Southcote

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|-------|------|------|------|------|------|-------|------|------|
| Lane Configurations | ↙ | ↑↑ | ↗ | ↙ | ↑↑ | ↗ | ↙ | ↑↑ | | ↙ | ↑↑ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.0 | 3.5 | 3.3 | 3.0 | 3.5 | 3.3 | 3.3 | 3.3 | 3.3 | 3.0 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.91 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1652 | 3500 | 1531 | 1652 | 3500 | 1531 | 1711 | 3307 | | 1652 | 3199 | |
| Fl _t Permitted | 0.20 | 1.00 | 1.00 | 0.29 | 1.00 | 1.00 | 0.38 | 1.00 | | 0.33 | 1.00 | |
| Satd. Flow (perm) | 349 | 3500 | 1531 | 506 | 3500 | 1531 | 691 | 3307 | | 577 | 3199 | |
| Volume (vph) | 245 | 835 | 42 | 64 | 695 | 114 | 51 | 250 | 72 | 170 | 277 | 372 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 266 | 908 | 46 | 70 | 755 | 124 | 55 | 272 | 78 | 185 | 301 | 404 |
| RTOR Reduction (vph) | 0 | 0 | 24 | 0 | 0 | 80 | 0 | 26 | 0 | 0 | 229 | 0 |
| Lane Group Flow (vph) | 266 | 908 | 22 | 70 | 755 | 44 | 55 | 324 | 0 | 185 | 476 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | pm+pt | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 44.1 | 35.9 | 35.9 | 30.8 | 26.6 | 26.6 | 13.2 | 13.2 | | 24.4 | 24.4 | |
| Effective Green, g (s) | 46.1 | 37.9 | 37.9 | 32.8 | 28.6 | 28.6 | 15.2 | 15.2 | | 26.4 | 26.4 | |
| Actuated g/C Ratio | 0.57 | 0.47 | 0.47 | 0.41 | 0.36 | 0.36 | 0.19 | 0.19 | | 0.33 | 0.33 | |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 418 | 1648 | 721 | 266 | 1243 | 544 | 130 | 624 | | 285 | 1049 | |
| v/s Ratio Prot | c0.11 | 0.26 | | 0.01 | 0.22 | | | 0.10 | | c0.06 | 0.15 | |
| v/s Ratio Perm | c0.26 | | 0.01 | 0.09 | | 0.03 | 0.08 | | | c0.15 | | |
| v/c Ratio | 0.64 | 0.55 | 0.03 | 0.26 | 0.61 | 0.08 | 0.42 | 0.52 | | 0.65 | 0.45 | |
| Uniform Delay, d ₁ | 11.1 | 15.2 | 11.4 | 14.8 | 21.3 | 17.2 | 28.8 | 29.4 | | 20.9 | 21.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 3.2 | 0.6 | 0.0 | 0.5 | 1.1 | 0.1 | 2.2 | 0.7 | | 5.0 | 0.3 | |
| Delay (s) | 14.2 | 15.8 | 11.5 | 15.3 | 22.4 | 17.3 | 31.0 | 30.1 | | 25.9 | 21.7 | |
| Level of Service | B | B | B | B | C | B | C | C | | C | C | |
| Approach Delay (s) | | 15.3 | | | 21.3 | | | 30.2 | | | 22.6 | |
| Approach LOS | | B | | | C | | | C | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 20.5 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.62 | | |
| Actuated Cycle Length (s) | 80.5 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 74.1% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

91: Garner & Kitty Murray

11/12/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|------|------|------|------|------|------|------|-------|------|
| Lane Configurations | ↘ | ↗↗ | ↘ | ↘ | ↗↗ | ↘ | ↘ | ↗ | ↘ | ↘ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3421 | 1531 | 1711 | 3421 | 1531 | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 |
| Flt Permitted | 0.21 | 1.00 | 1.00 | 0.30 | 1.00 | 1.00 | 0.49 | 1.00 | 1.00 | 0.53 | 1.00 | 1.00 |
| Satd. Flow (perm) | 370 | 3421 | 1531 | 536 | 3421 | 1531 | 886 | 1801 | 1531 | 946 | 1801 | 1531 |
| Volume (vph) | 135 | 884 | 42 | 64 | 647 | 116 | 51 | 251 | 72 | 48 | 277 | 313 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 147 | 961 | 46 | 70 | 703 | 126 | 55 | 273 | 78 | 52 | 301 | 340 |
| RTOR Reduction (vph) | 0 | 0 | 23 | 0 | 0 | 84 | 0 | 0 | 48 | 0 | 0 | 113 |
| Lane Group Flow (vph) | 147 | 961 | 23 | 70 | 703 | 42 | 55 | 273 | 30 | 52 | 301 | 227 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 29.1 | 29.1 | 29.1 | 19.1 | 19.1 | 19.1 | 23.5 | 23.5 | 23.5 | 23.5 | 23.5 | 23.5 |
| Effective Green, g (s) | 29.1 | 29.1 | 29.1 | 19.1 | 19.1 | 19.1 | 23.5 | 23.5 | 23.5 | 23.5 | 23.5 | 23.5 |
| Actuated g/C Ratio | 0.48 | 0.48 | 0.48 | 0.32 | 0.32 | 0.32 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 310 | 1643 | 735 | 169 | 1078 | 483 | 344 | 698 | 594 | 367 | 698 | 594 |
| v/s Ratio Prot | 0.05 | c0.28 | | | 0.21 | | | 0.15 | | | c0.17 | |
| v/s Ratio Perm | 0.18 | | 0.01 | 0.13 | | 0.03 | 0.06 | | 0.02 | 0.05 | | 0.15 |
| v/c Ratio | 0.47 | 0.58 | 0.03 | 0.41 | 0.65 | 0.09 | 0.16 | 0.39 | 0.05 | 0.14 | 0.43 | 0.38 |
| Uniform Delay, d1 | 10.2 | 11.4 | 8.3 | 16.3 | 17.9 | 14.6 | 12.1 | 13.4 | 11.6 | 12.0 | 13.6 | 13.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.1 | 0.5 | 0.0 | 1.6 | 1.4 | 0.1 | 1.0 | 1.6 | 0.2 | 0.8 | 1.9 | 1.9 |
| Delay (s) | 11.3 | 11.9 | 8.3 | 18.0 | 19.3 | 14.7 | 13.1 | 15.0 | 11.7 | 12.8 | 15.6 | 15.2 |
| Level of Service | B | B | A | B | B | B | B | B | B | B | B | B |
| Approach Delay (s) | | 11.7 | | | 18.6 | | | 14.1 | | | 15.2 | |
| Approach LOS | | B | | | B | | | B | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 14.7 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.52 | | |
| Actuated Cycle Length (s) | 60.6 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 59.2% | ICU Level of Service | B |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

1: Wilson & Highway 52

11/11/2010






















| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|------|-------|------|----------------------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 4.0 | 3.3 | 3.3 | 4.0 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1946 | 1531 | 1711 | 1946 | 1531 |
| Flt Permitted | 0.15 | 1.00 | 1.00 | 0.62 | 1.00 | 1.00 | 0.60 | 1.00 | 1.00 | 0.69 | 1.00 | 1.00 |
| Satd. Flow (perm) | 265 | 3500 | 1531 | 1118 | 3500 | 1531 | 1085 | 1946 | 1531 | 1237 | 1946 | 1531 |
| Volume (vph) | 25 | 192 | 105 | 170 | 1070 | 30 | 456 | 100 | 60 | 17 | 204 | 136 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 27 | 209 | 114 | 185 | 1163 | 33 | 496 | 109 | 65 | 18 | 222 | 148 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 0 | 20 | 0 | 0 | 33 | 0 | 0 | 8 |
| Lane Group Flow (vph) | 27 | 209 | 44 | 185 | 1163 | 13 | 496 | 109 | 32 | 18 | 222 | 140 |
| Turn Type | Perm | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 25.2 | 25.2 | 25.2 | 25.2 | 25.2 | 25.2 | 31.8 | 31.8 | 31.8 | 31.8 | 31.8 | 31.8 |
| Effective Green, g (s) | 27.2 | 27.2 | 27.2 | 27.2 | 27.2 | 27.2 | 34.8 | 34.8 | 34.8 | 34.8 | 34.8 | 34.8 |
| Actuated g/C Ratio | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Grp Cap (vph) | 103 | 1360 | 595 | 434 | 1360 | 595 | 539 | 967 | 761 | 615 | 967 | 761 |
| v/s Ratio Prot | | 0.06 | | | c0.33 | | | 0.06 | | | 0.11 | |
| v/s Ratio Perm | 0.10 | | 0.03 | 0.17 | | 0.01 | c0.46 | | 0.02 | 0.01 | | 0.09 |
| v/c Ratio | 0.26 | 0.15 | 0.07 | 0.43 | 0.86 | 0.02 | 0.92 | 0.11 | 0.04 | 0.03 | 0.23 | 0.18 |
| Uniform Delay, d1 | 14.6 | 13.9 | 13.5 | 15.7 | 19.6 | 13.2 | 16.3 | 9.4 | 9.0 | 9.0 | 10.0 | 9.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.81 | 0.88 | 0.59 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 6.1 | 0.2 | 0.2 | 3.0 | 7.0 | 0.1 | 21.4 | 0.1 | 0.0 | 0.0 | 0.2 | 0.2 |
| Delay (s) | 20.7 | 14.2 | 13.7 | 15.7 | 24.2 | 7.8 | 37.7 | 9.4 | 9.1 | 9.0 | 10.2 | 9.9 |
| Level of Service | C | B | B | B | C | A | D | A | A | A | B | A |
| Approach Delay (s) | | 14.5 | | | 22.7 | | | 30.4 | | | 10.0 | |
| Approach LOS | | B | | | C | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.7 | | | | HCM Level of Service | | | | C | |
| HCM Volume to Capacity ratio | | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | | | | Sum of lost time (s) | | | | 8.0 | |
| Intersection Capacity Utilization | | | 87.2% | | | | ICU Level of Service | | | | E | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

21: Halson & Wilson

11/11/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | |  |  | |  | |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |
| Total Lost time (s) | | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Fr _t | | 1.00 | 0.85 | | 0.97 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Fl _t Protected | | 0.95 | 1.00 | | 0.98 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | | 1715 | 1566 | | 1718 | | 1711 | 1801 | 1531 | 1711 | 1800 | |
| Fl _t Permitted | | 0.72 | 1.00 | | 0.91 | | 0.44 | 1.00 | 1.00 | 0.19 | 1.00 | |
| Satd. Flow (perm) | | 1304 | 1566 | | 1594 | | 785 | 1801 | 1531 | 334 | 1800 | |
| Volume (vph) | 233 | 1 | 195 | 2 | 2 | 1 | 1 | 662 | 252 | 113 | 545 | 2 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 253 | 1 | 212 | 2 | 2 | 1 | 1 | 720 | 274 | 123 | 592 | 2 |
| RTOR Reduction (vph) | 0 | 0 | 124 | 0 | 1 | 0 | 0 | 0 | 126 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 254 | 88 | 0 | 4 | 0 | 1 | 720 | 148 | 123 | 594 | 0 |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | pm+pt | | |
| Protected Phases | | 8 | | | 4 | | | 2 | | 1 | 6 | |
| Permitted Phases | 8 | | 8 | 4 | | | 2 | | 2 | 6 | 6 | |
| Actuated Green, G (s) | | 20.8 | 20.8 | | 20.8 | | 46.5 | 46.5 | 46.5 | 57.2 | 57.2 | |
| Effective Green, g (s) | | 22.8 | 22.8 | | 22.8 | | 48.5 | 48.5 | 48.5 | 59.2 | 59.2 | |
| Actuated g/C Ratio | | 0.25 | 0.25 | | 0.25 | | 0.54 | 0.54 | 0.54 | 0.66 | 0.66 | |
| Clearance Time (s) | | 6.0 | 6.0 | | 6.0 | | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | | 3.5 | 3.5 | 3.5 | 3.0 | 3.5 | |
| Lane Grp Cap (vph) | | 330 | 397 | | 404 | | 423 | 971 | 825 | 322 | 1184 | |
| v/s Ratio Prot | | | | | | | | c0.40 | | 0.03 | c0.33 | |
| v/s Ratio Perm | | c0.19 | 0.06 | | 0.00 | | 0.00 | | 0.10 | 0.22 | | |
| v/c Ratio | | 0.77 | 0.22 | | 0.01 | | 0.00 | 0.74 | 0.18 | 0.38 | 0.50 | |
| Uniform Delay, d ₁ | | 31.2 | 26.6 | | 25.2 | | 9.6 | 15.9 | 10.6 | 10.8 | 7.9 | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.05 | 1.81 | 1.93 | 0.78 | |
| Incremental Delay, d ₂ | | 9.9 | 0.2 | | 0.0 | | 0.0 | 4.9 | 0.5 | 0.7 | 1.5 | |
| Delay (s) | | 41.1 | 26.8 | | 25.2 | | 8.2 | 21.7 | 19.6 | 21.6 | 7.6 | |
| Level of Service | | D | C | | C | | A | C | B | C | A | |
| Approach Delay (s) | | 34.6 | | | 25.2 | | | 21.1 | | | 10.0 | |
| Approach LOS | | C | | | C | | | C | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 20.3 | | | | HCM Level of Service | | | | C | |
| HCM Volume to Capacity ratio | | | 0.74 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | | Sum of lost time (s) | | | | 12.0 | |
| Intersection Capacity Utilization | | | 70.7% | | | | ICU Level of Service | | | | C | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

31: Mohawk/Rosseaux & McNiven

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|-------|-------|------|-------|-------|-------|------|------|------|
| Lane Configurations | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | 1.00 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1750 | 1842 | 1566 | 1750 | 1842 | 1566 | 1711 | 1842 | 1531 | 1711 | 1754 | 1754 |
| Fl _t Permitted | 0.25 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.62 | 1.00 | 1.00 | 0.74 | 1.00 | 1.00 |
| Satd. Flow (perm) | 457 | 1842 | 1566 | 154 | 1842 | 1566 | 1115 | 1842 | 1531 | 1340 | 1754 | 1754 |
| Volume (vph) | 4 | 755 | 782 | 698 | 722 | 7 | 376 | 18 | 1268 | 39 | 40 | 18 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 4 | 821 | 850 | 759 | 785 | 8 | 409 | 20 | 1378 | 42 | 43 | 20 |
| RTOR Reduction (vph) | 0 | 0 | 202 | 0 | 0 | 3 | 0 | 0 | 276 | 0 | 13 | 0 |
| Lane Group Flow (vph) | 4 | 821 | 648 | 759 | 785 | 5 | 409 | 20 | 1102 | 42 | 50 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | pm+pt | | Perm | Perm | | |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 42.1 | 42.1 | 42.1 | 74.1 | 74.1 | 74.1 | 55.4 | 55.4 | 55.4 | 25.0 | 25.0 | |
| Effective Green, g (s) | 44.0 | 44.0 | 44.0 | 76.0 | 76.0 | 76.0 | 57.1 | 57.1 | 57.1 | 26.7 | 26.7 | |
| Actuated g/C Ratio | 0.31 | 0.31 | 0.31 | 0.54 | 0.54 | 0.54 | 0.40 | 0.40 | 0.40 | 0.19 | 0.19 | |
| Clearance Time (s) | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 | 5.9 | 4.0 | 5.7 | 5.7 | 5.7 | 5.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | 3.5 | 2.0 | 3.5 | 3.5 | 3.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 143 | 574 | 488 | 400 | 992 | 843 | 563 | 745 | 620 | 254 | 332 | |
| v/s Ratio Prot | | 0.45 | | c0.38 | 0.43 | | 0.14 | 0.01 | | | 0.03 | |
| v/s Ratio Perm | 0.01 | | 0.41 | c0.65 | | 0.00 | 0.16 | | c0.72 | 0.03 | | |
| v/c Ratio | 0.03 | 1.43 | 1.33 | 1.90 | 0.79 | 0.01 | 0.73 | 0.03 | 1.78 | 0.17 | 0.15 | |
| Uniform Delay, d ₁ | 33.7 | 48.5 | 48.5 | 58.8 | 26.2 | 15.1 | 32.9 | 25.3 | 42.0 | 47.9 | 47.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.1 | 203.6 | 160.9 | 413.2 | 4.5 | 0.0 | 4.6 | 0.0 | 356.2 | 0.1 | 0.1 | |
| Delay (s) | 33.8 | 252.1 | 209.5 | 471.9 | 30.7 | 15.1 | 37.6 | 25.3 | 398.2 | 48.0 | 47.8 | |
| Level of Service | C | F | F | F | C | B | D | C | F | D | D | |
| Approach Delay (s) | | 230.0 | | | 246.4 | | | 312.4 | | | 47.9 | |
| Approach LOS | | F | | | F | | | F | | | D | |

Intersection Summary
























| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 260.2 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.83 | | |
| Actuated Cycle Length (s) | 141.1 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 136.6% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

47: Fiddler's Green & Wilson

11/11/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  |  | |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1678 | | 1750 | 1842 | 1531 | 1750 | 1842 | 1531 |
| Fl _t Permitted | 0.28 | 1.00 | 1.00 | 0.64 | 1.00 | | 0.48 | 1.00 | 1.00 | 0.40 | 1.00 | 1.00 |
| Satd. Flow (perm) | 512 | 1801 | 1531 | 1144 | 1678 | | 892 | 1842 | 1531 | 728 | 1842 | 1531 |
| Volume (vph) | 141 | 125 | 222 | 162 | 179 | 149 | 61 | 419 | 83 | 76 | 326 | 26 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 153 | 136 | 241 | 176 | 195 | 162 | 66 | 455 | 90 | 83 | 354 | 28 |
| RTOR Reduction (vph) | 0 | 0 | 174 | 0 | 40 | 0 | 0 | 0 | 41 | 0 | 0 | 8 |
| Lane Group Flow (vph) | 153 | 136 | 67 | 176 | 317 | 0 | 66 | 455 | 49 | 83 | 354 | 20 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | Perm | pm+pt | | Perm |
| Protected Phases | | 8 | | | 4 | | 5 | 2 | | 1 | | 6 |
| Permitted Phases | 8 | | 8 | 4 | | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 23.1 | 23.1 | 23.1 | 23.1 | 23.1 | | 51.6 | 46.6 | 46.6 | 52.2 | 46.9 | 46.9 |
| Effective Green, g (s) | 25.1 | 25.1 | 25.1 | 25.1 | 25.1 | | 52.6 | 48.6 | 48.6 | 53.2 | 48.9 | 48.9 |
| Actuated g/C Ratio | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | | 0.58 | 0.54 | 0.54 | 0.59 | 0.54 | 0.54 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 2.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 143 | 502 | 427 | 319 | 468 | | 559 | 995 | 827 | 479 | 1001 | 832 |
| v/s Ratio Prot | | 0.08 | | | 0.19 | | 0.01 | c0.25 | | c0.01 | 0.19 | |
| v/s Ratio Perm | c0.30 | | 0.04 | 0.15 | | | 0.06 | | 0.03 | 0.09 | | 0.01 |
| v/c Ratio | 1.07 | 0.27 | 0.16 | 0.55 | 0.68 | | 0.12 | 0.46 | 0.06 | 0.17 | 0.35 | 0.02 |
| Uniform Delay, d ₁ | 32.5 | 25.3 | 24.5 | 27.7 | 28.9 | | 8.3 | 12.6 | 9.8 | 8.5 | 11.6 | 9.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 0.88 | 0.95 | 0.78 | 0.88 | 0.95 | 0.91 |
| Incremental Delay, d ₂ | 95.2 | 0.3 | 0.2 | 2.1 | 3.9 | | 0.0 | 1.5 | 0.1 | 0.1 | 0.8 | 0.0 |
| Delay (s) | 127.6 | 25.6 | 24.6 | 29.7 | 32.7 | | 7.3 | 13.5 | 7.8 | 7.6 | 11.9 | 8.7 |
| Level of Service | F | C | C | C | C | | A | B | A | A | B | A |
| Approach Delay (s) | | 54.6 | | | 31.7 | | | 12.0 | | | 10.9 | |
| Approach LOS | | D | | | C | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 27.2 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.64 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 66.5% | | | | ICU Level of Service | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

51: Golf Links & Kitty Murray

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|-------|-------|------|-------|------|------|------|------|------|
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘↗ | ↑↑ | ↗ | ↘ | ↗ | | ↘↗ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.86 | | 1.00 | 0.95 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 3319 | 3500 | 1531 | 1711 | 1575 | | 3319 | 1750 | |
| Fl _t Permitted | 0.32 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.75 | 1.00 | | 0.37 | 1.00 | |
| Satd. Flow (perm) | 573 | 3500 | 1531 | 3319 | 3500 | 1531 | 1350 | 1575 | | 1277 | 1750 | |
| Volume (vph) | 46 | 397 | 379 | 1031 | 823 | 43 | 129 | 9 | 261 | 43 | 7 | 4 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 50 | 432 | 412 | 1121 | 895 | 47 | 140 | 10 | 284 | 47 | 8 | 4 |
| RTOR Reduction (vph) | 0 | 0 | 302 | 0 | 0 | 20 | 0 | 208 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 50 | 432 | 110 | 1121 | 895 | 27 | 140 | 86 | 0 | 47 | 9 | 0 |
| Turn Type | pm+pt | | Perm | Prot | | Perm | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 25.0 | 22.0 | 22.0 | 31.0 | 50.0 | 50.0 | 22.0 | 22.0 | | 22.0 | 22.0 | |
| Effective Green, g (s) | 26.0 | 24.0 | 24.0 | 30.0 | 52.0 | 52.0 | 24.0 | 24.0 | | 24.0 | 24.0 | |
| Actuated g/C Ratio | 0.29 | 0.27 | 0.27 | 0.33 | 0.58 | 0.58 | 0.27 | 0.27 | | 0.27 | 0.27 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 191 | 933 | 408 | 1106 | 2022 | 885 | 360 | 420 | | 341 | 467 | |
| v/s Ratio Prot | 0.01 | 0.12 | | c0.34 | c0.26 | | | 0.05 | | | 0.01 | |
| v/s Ratio Perm | 0.07 | | 0.07 | | | 0.02 | c0.10 | | | 0.04 | | |
| v/c Ratio | 0.26 | 0.46 | 0.27 | 1.01 | 0.44 | 0.03 | 0.39 | 0.20 | | 0.14 | 0.02 | |
| Uniform Delay, d ₁ | 23.4 | 27.6 | 26.1 | 30.0 | 10.8 | 8.2 | 27.0 | 25.6 | | 25.1 | 24.3 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.08 | 1.17 | 2.11 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.3 | 1.7 | 1.6 | 29.9 | 0.7 | 0.1 | 3.1 | 1.1 | | 0.8 | 0.1 | |
| Delay (s) | 23.7 | 29.3 | 27.7 | 62.3 | 13.2 | 17.3 | 30.1 | 26.7 | | 26.0 | 24.4 | |
| Level of Service | C | C | C | E | B | B | C | C | | C | C | |
| Approach Delay (s) | | 28.2 | | | 40.0 | | | 27.8 | | | 25.6 | |
| Approach LOS | | C | | | D | | | C | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 35.2 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.63 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 71.2% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
52: Golf Links & Stone Church

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|-------|-------|--------|-------|--------|------|------|------|------|
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑ | | ↑ | | ↑ | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.91 | 0.91 | 1.00 |
| Flt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.98 | 1.00 |
| Satd. Flow (prot) | | 4916 | 1531 | 1711 | 3421 | | 1711 | | 1531 | 1628 | 3348 | 1601 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.39 | | 1.00 | 0.95 | 0.98 | 1.00 |
| Satd. Flow (perm) | | 4916 | 1531 | 1711 | 3421 | | 700 | | 1531 | 1628 | 3348 | 1601 |
| Volume (vph) | 0 | 845 | 112 | 243 | 1202 | 0 | 301 | 0 | 327 | 313 | 173 | 236 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 918 | 122 | 264 | 1307 | 0 | 327 | 0 | 355 | 340 | 188 | 257 |
| RTOR Reduction (vph) | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 37 |
| Lane Group Flow (vph) | 0 | 918 | 37 | 264 | 1307 | 0 | 327 | 0 | 350 | 170 | 358 | 220 |
| Turn Type | | | Perm | Prot | | custom | | custom | | Perm | | Perm |
| Protected Phases | | 6 | | 5 | 2 | | 3 | | 5 | | 4 | |
| Permitted Phases | | | 6 | | | | 8 | | 3 | 4 | 4 | 4 |
| Actuated Green, G (s) | | 25.3 | 25.3 | 13.0 | 43.3 | | 34.7 | | 53.7 | 23.7 | 23.7 | 23.7 |
| Effective Green, g (s) | | 27.3 | 27.3 | 14.0 | 45.3 | | 36.7 | | 54.7 | 25.7 | 25.7 | 25.7 |
| Actuated g/C Ratio | | 0.30 | 0.30 | 0.16 | 0.50 | | 0.41 | | 0.61 | 0.29 | 0.29 | 0.29 |
| Clearance Time (s) | | 6.0 | 6.0 | 5.0 | 6.0 | | 3.0 | | | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | 1.0 | 2.0 | | 1.0 | | | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | | 1491 | 464 | 266 | 1722 | | 364 | | 931 | 465 | 956 | 457 |
| v/s Ratio Prot | | 0.19 | | c0.15 | c0.38 | | c0.07 | | 0.23 | | | |
| v/s Ratio Perm | | | 0.02 | | | | c0.30 | | | 0.10 | 0.11 | 0.14 |
| v/c Ratio | | 0.62 | 0.08 | 0.99 | 0.76 | | 0.90 | | 0.38 | 0.37 | 0.37 | 0.48 |
| Uniform Delay, d1 | | 26.9 | 22.4 | 37.9 | 18.0 | | 24.1 | | 9.0 | 25.6 | 25.7 | 26.6 |
| Progression Factor | | 1.24 | 1.90 | 1.04 | 1.28 | | 1.09 | | 1.13 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.7 | 0.3 | 41.5 | 2.0 | | 23.2 | | 0.1 | 0.2 | 0.1 | 0.3 |
| Delay (s) | | 34.9 | 42.7 | 81.2 | 25.0 | | 49.6 | | 10.2 | 25.8 | 25.8 | 26.9 |
| Level of Service | | C | D | F | C | | D | | B | C | C | C |
| Approach Delay (s) | | 35.9 | | | 34.4 | | | 29.1 | | | 26.2 | |
| Approach LOS | | D | | | C | | | C | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 32.3 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.84 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 74.5% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
72: Golf Links Rd & Martindale

11/11/2010



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|------------------------|-------|------|-------|------|-------|------|
| Lane Configurations | ↖↗ | ↕ | ↕ | ↖ | ↖↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.5 | 3.3 | 3.3 | 3.5 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 0.97 | 0.95 | 0.95 | 1.00 | 0.97 | |
| Flt | 1.00 | 1.00 | 1.00 | 0.85 | 0.94 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.97 | |
| Satd. Flow (prot) | 3319 | 3500 | 3500 | 1531 | 3185 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.97 | |
| Satd. Flow (perm) | 3319 | 3500 | 3500 | 1531 | 3185 | |
| Volume (vph) | 169 | 501 | 1333 | 236 | 261 | 180 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 184 | 545 | 1449 | 257 | 284 | 196 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 98 | 160 | 0 |
| Lane Group Flow (vph) | 184 | 545 | 1449 | 159 | 320 | 0 |
| Turn Type | Prot | | Perm | | | |
| Protected Phases | 1 | 6 | 2 | | 4 | |
| Permitted Phases | | 1 | | 2 | | |
| Actuated Green, G (s) | 7.6 | 64.4 | 53.8 | 53.8 | 13.6 | |
| Effective Green, g (s) | 6.6 | 66.4 | 55.8 | 55.8 | 15.6 | |
| Actuated g/C Ratio | 0.07 | 0.74 | 0.62 | 0.62 | 0.17 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 4.0 | 1.0 | |
| Lane Grp Cap (vph) | 243 | 2582 | 2170 | 949 | 552 | |
| v/s Ratio Prot | c0.06 | 0.16 | c0.41 | | c0.10 | |
| v/s Ratio Perm | | | | 0.10 | | |
| v/c Ratio | 0.76 | 0.21 | 0.67 | 0.17 | 0.58 | |
| Uniform Delay, d1 | 40.9 | 3.7 | 11.1 | 7.3 | 34.2 | |
| Progression Factor | 0.79 | 1.10 | 0.30 | 0.02 | 1.00 | |
| Incremental Delay, d2 | 10.8 | 0.0 | 1.1 | 0.3 | 0.9 | |
| Delay (s) | 43.1 | 4.0 | 4.5 | 0.4 | 35.1 | |
| Level of Service | D | A | A | A | D | |
| Approach Delay (s) | | 13.9 | 3.9 | | 35.1 | |
| Approach LOS | | B | A | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 11.5 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.66 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 64.8% | ICU Level of Service | C |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

75: Golf Links Rd & Neville

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|-------|------|------|-------|-------|------|------|------|------|-------|------|------|
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘ | ↑↑ | ↗ | ↘ | ↗ | | ↗↘ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | | 1.00 | 0.93 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1629 | | 3319 | 1715 | |
| Fl _t Permitted | 0.07 | 1.00 | 1.00 | 0.31 | 1.00 | 1.00 | 0.63 | 1.00 | | 0.40 | 1.00 | |
| Satd. Flow (perm) | 134 | 3500 | 1531 | 565 | 3500 | 1531 | 1136 | 1629 | | 1410 | 1715 | |
| Volume (vph) | 53 | 690 | 22 | 125 | 1525 | 148 | 115 | 50 | 167 | 279 | 63 | 53 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 58 | 750 | 24 | 136 | 1658 | 161 | 125 | 54 | 182 | 303 | 68 | 58 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 55 | 0 | 143 | 0 | 0 | 42 | 0 |
| Lane Group Flow (vph) | 58 | 750 | 14 | 136 | 1658 | 106 | 125 | 93 | 0 | 303 | 84 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | Perm | | |
| Protected Phases | 1 | 6 | | 5 | 2 | | | 8 | | | 4 | |
| Permitted Phases | 6 | | 6 | 2 | | 2 | 8 | | | 4 | | |
| Actuated Green, G (s) | 55.7 | 51.6 | 51.6 | 59.3 | 53.4 | 53.4 | 17.5 | 17.5 | | 17.5 | 17.5 | |
| Effective Green, g (s) | 56.7 | 53.6 | 53.6 | 60.3 | 55.4 | 55.4 | 19.5 | 19.5 | | 19.5 | 19.5 | |
| Actuated g/C Ratio | 0.63 | 0.60 | 0.60 | 0.67 | 0.62 | 0.62 | 0.22 | 0.22 | | 0.22 | 0.22 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 139 | 2084 | 912 | 441 | 2154 | 942 | 246 | 353 | | 306 | 372 | |
| v/s Ratio Prot | 0.01 | 0.21 | | c0.02 | c0.47 | | | 0.06 | | | 0.05 | |
| v/s Ratio Perm | 0.25 | | 0.01 | 0.19 | | 0.07 | 0.11 | | | c0.21 | | |
| v/c Ratio | 0.42 | 0.36 | 0.02 | 0.31 | 0.77 | 0.11 | 0.51 | 0.26 | | 0.99 | 0.23 | |
| Uniform Delay, d1 | 11.5 | 9.4 | 7.4 | 5.8 | 12.6 | 7.1 | 31.0 | 29.3 | | 35.2 | 29.0 | |
| Progression Factor | 0.95 | 0.89 | 0.80 | 0.67 | 0.95 | 0.65 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.7 | 0.5 | 0.0 | 0.1 | 1.8 | 0.2 | 0.6 | 0.1 | | 48.6 | 0.1 | |
| Delay (s) | 11.5 | 8.8 | 6.0 | 4.0 | 13.9 | 4.8 | 31.6 | 29.4 | | 83.7 | 29.2 | |
| Level of Service | B | A | A | A | B | A | C | C | | F | C | |
| Approach Delay (s) | | 8.9 | | | 12.4 | | | 30.2 | | | 67.7 | |
| Approach LOS | | A | | | B | | | C | | | E | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 20.0 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.81 | | |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 80.9% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

78: Golf Links & McNiven

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|------|------|-------|------|------|-------|-------|------|
| Lane Configurations | ↖ | ↗ | ↘ | ↖ | ↗ | ↘ | ↖ | ↗↘ | | ↖ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 | 1711 | 3293 | | 1711 | 1787 | |
| Flt Permitted | 0.12 | 1.00 | 1.00 | 0.63 | 1.00 | 1.00 | 0.12 | 1.00 | | 0.22 | 1.00 | |
| Satd. Flow (perm) | 220 | 1801 | 1531 | 1135 | 1801 | 1531 | 214 | 3293 | | 389 | 1787 | |
| Volume (vph) | 281 | 187 | 207 | 82 | 376 | 534 | 66 | 418 | 139 | 365 | 685 | 38 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 305 | 203 | 225 | 89 | 409 | 580 | 72 | 454 | 151 | 397 | 745 | 41 |
| RTOR Reduction (vph) | 0 | 0 | 113 | 0 | 0 | 321 | 0 | 27 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 305 | 203 | 112 | 89 | 409 | 259 | 72 | 578 | 0 | 397 | 784 | 0 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | pm+pt | | | pm+pt | | |
| Protected Phases | 5 | 2 | | | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 48.7 | 48.7 | 48.7 | 26.7 | 26.7 | 26.7 | 34.5 | 31.4 | | 58.5 | 51.4 | |
| Effective Green, g (s) | 50.8 | 50.8 | 50.8 | 28.8 | 28.8 | 28.8 | 36.8 | 33.7 | | 60.8 | 53.7 | |
| Actuated g/C Ratio | 0.42 | 0.42 | 0.42 | 0.24 | 0.24 | 0.24 | 0.31 | 0.28 | | 0.51 | 0.45 | |
| Clearance Time (s) | 4.0 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 4.0 | 6.3 | | 4.0 | 6.3 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 318 | 765 | 650 | 273 | 434 | 369 | 105 | 928 | | 453 | 802 | |
| v/s Ratio Prot | c0.14 | 0.11 | | | 0.23 | | 0.02 | 0.18 | | c0.17 | c0.44 | |
| v/s Ratio Perm | c0.26 | | 0.07 | 0.08 | | 0.17 | 0.19 | | | 0.28 | | |
| v/c Ratio | 0.96 | 0.27 | 0.17 | 0.33 | 0.94 | 0.70 | 0.69 | 0.62 | | 0.88 | 0.98 | |
| Uniform Delay, d1 | 34.5 | 22.3 | 21.4 | 37.4 | 44.6 | 41.5 | 36.2 | 37.4 | | 22.3 | 32.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 39.1 | 0.2 | 0.1 | 0.7 | 29.0 | 5.9 | 17.0 | 1.3 | | 17.1 | 26.1 | |
| Delay (s) | 73.6 | 22.5 | 21.5 | 38.1 | 73.6 | 47.4 | 53.2 | 38.7 | | 39.4 | 58.5 | |
| Level of Service | E | C | C | D | E | D | D | D | | D | E | |
| Approach Delay (s) | | 43.4 | | | 56.6 | | | 40.3 | | | 52.1 | |
| Approach LOS | | D | | | E | | | D | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 49.5 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.97 | | |
| Actuated Cycle Length (s) | 119.6 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 90.7% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

90: Garner & Southcote

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|------|------|------|------|------|-------|------|------|
| Lane Configurations | ↖ | ↗↗ | ↖ | ↖ | ↗↗ | ↖ | ↖ | ↗↗ | | ↖ | ↗↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.0 | 3.5 | 3.3 | 3.0 | 3.5 | 3.3 | 3.3 | 3.3 | 3.3 | 3.0 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 0.92 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1652 | 3500 | 1531 | 1652 | 3500 | 1531 | 1711 | 3254 | | 1652 | 3203 | |
| Fl _t Permitted | 0.16 | 1.00 | 1.00 | 0.14 | 1.00 | 1.00 | 0.19 | 1.00 | | 0.16 | 1.00 | |
| Satd. Flow (perm) | 283 | 3500 | 1531 | 237 | 3500 | 1531 | 343 | 3254 | | 278 | 3203 | |
| Volume (vph) | 415 | 1643 | 54 | 79 | 671 | 162 | 31 | 472 | 229 | 187 | 400 | 520 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 451 | 1786 | 59 | 86 | 729 | 176 | 34 | 513 | 249 | 203 | 435 | 565 |
| RTOR Reduction (vph) | 0 | 0 | 29 | 0 | 0 | 124 | 0 | 59 | 0 | 0 | 233 | 0 |
| Lane Group Flow (vph) | 451 | 1786 | 30 | 86 | 729 | 52 | 34 | 703 | 0 | 203 | 767 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | pm+pt | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 56.2 | 49.1 | 49.1 | 30.5 | 27.4 | 27.4 | 19.0 | 19.0 | | 31.0 | 31.0 | |
| Effective Green, g (s) | 58.2 | 51.1 | 51.1 | 32.5 | 29.4 | 29.4 | 21.0 | 21.0 | | 33.0 | 33.0 | |
| Actuated g/C Ratio | 0.59 | 0.52 | 0.52 | 0.33 | 0.30 | 0.30 | 0.21 | 0.21 | | 0.33 | 0.33 | |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 508 | 1803 | 789 | 122 | 1037 | 454 | 73 | 689 | | 203 | 1066 | |
| v/s Ratio Prot | c0.22 | c0.51 | | 0.02 | 0.21 | | | 0.22 | | c0.08 | 0.24 | |
| v/s Ratio Perm | 0.30 | | 0.02 | 0.21 | | 0.03 | 0.10 | | | c0.25 | | |
| v/c Ratio | 0.89 | 0.99 | 0.04 | 0.70 | 0.70 | 0.11 | 0.47 | 1.02 | | 1.00 | 0.72 | |
| Uniform Delay, d ₁ | 23.1 | 23.8 | 11.9 | 30.3 | 31.0 | 25.4 | 34.2 | 39.1 | | 30.1 | 29.0 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 17.0 | 19.0 | 0.0 | 16.9 | 2.5 | 0.2 | 4.6 | 39.5 | | 63.2 | 2.4 | |
| Delay (s) | 40.1 | 42.8 | 11.9 | 47.2 | 33.5 | 25.6 | 38.8 | 78.6 | | 93.3 | 31.4 | |
| Level of Service | D | D | B | D | C | C | D | E | | F | C | |
| Approach Delay (s) | | 41.4 | | | 33.3 | | | 76.9 | | | 41.8 | |
| Approach LOS | | D | | | C | | | E | | | D | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 45.3 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 0.99 | | |
| Actuated Cycle Length (s) | 99.2 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 99.2% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

91: Garner & Kitty Murray

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|-------|------|------|-------|------|------|-------|------|------|------|------|
| Lane Configurations | ↘ | ↗↗ | ↘ | ↘ | ↗↗ | ↘ | ↘ | ↗ | ↘ | ↘ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3421 | 1531 | 1711 | 3421 | 1531 | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 |
| Flt Permitted | 0.19 | 1.00 | 1.00 | 0.27 | 1.00 | 1.00 | 0.39 | 1.00 | 1.00 | 0.32 | 1.00 | 1.00 |
| Satd. Flow (perm) | 343 | 3421 | 1531 | 494 | 3421 | 1531 | 700 | 1801 | 1531 | 568 | 1801 | 1531 |
| Volume (vph) | 128 | 859 | 54 | 79 | 811 | 68 | 31 | 472 | 230 | 142 | 400 | 253 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 139 | 934 | 59 | 86 | 882 | 74 | 34 | 513 | 250 | 154 | 435 | 275 |
| RTOR Reduction (vph) | 0 | 0 | 32 | 0 | 0 | 42 | 0 | 0 | 34 | 0 | 0 | 75 |
| Lane Group Flow (vph) | 139 | 934 | 27 | 86 | 882 | 32 | 34 | 513 | 216 | 154 | 435 | 200 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 24.1 | 24.1 | 24.1 | 17.0 | 17.0 | 17.0 | 26.2 | 26.2 | 26.2 | 26.2 | 26.2 | 26.2 |
| Effective Green, g (s) | 24.1 | 24.1 | 24.1 | 17.0 | 17.0 | 17.0 | 26.2 | 26.2 | 26.2 | 26.2 | 26.2 | 26.2 |
| Actuated g/C Ratio | 0.41 | 0.41 | 0.41 | 0.29 | 0.29 | 0.29 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 215 | 1414 | 633 | 144 | 998 | 446 | 315 | 809 | 688 | 255 | 809 | 688 |
| v/s Ratio Prot | 0.03 | c0.27 | | | c0.26 | | | c0.28 | | | 0.24 | |
| v/s Ratio Perm | 0.23 | | 0.02 | 0.17 | | 0.02 | 0.05 | | 0.14 | 0.27 | | 0.13 |
| v/c Ratio | 0.65 | 0.66 | 0.04 | 0.60 | 0.88 | 0.07 | 0.11 | 0.63 | 0.31 | 0.60 | 0.54 | 0.29 |
| Uniform Delay, d1 | 12.9 | 13.8 | 10.2 | 17.7 | 19.7 | 14.9 | 9.3 | 12.4 | 10.3 | 12.1 | 11.7 | 10.2 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 6.5 | 1.2 | 0.0 | 6.5 | 9.4 | 0.1 | 0.7 | 3.8 | 1.2 | 10.2 | 2.6 | 1.1 |
| Delay (s) | 19.5 | 15.0 | 10.2 | 24.2 | 29.1 | 15.0 | 10.0 | 16.1 | 11.5 | 22.3 | 14.2 | 11.2 |
| Level of Service | B | B | B | C | C | B | A | B | B | C | B | B |
| Approach Delay (s) | | 15.3 | | | 27.7 | | | 14.4 | | | 14.7 | |
| Approach LOS | | B | | | C | | | B | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 18.3 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.75 | | |
| Actuated Cycle Length (s) | 58.3 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 75.6% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

1: Wilson & Highway 52

11/11/2010






















| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|-------|------|------|----------------------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 4.0 | 3.3 | 3.3 | 4.0 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | 0.99 | 1.00 |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1946 | 1531 | | 1934 | 1531 |
| Fl _t Permitted | 0.56 | 1.00 | 1.00 | 0.16 | 1.00 | 1.00 | 0.60 | 1.00 | 1.00 | | 0.91 | 1.00 |
| Satd. Flow (perm) | 1017 | 3500 | 1531 | 293 | 3500 | 1531 | 1089 | 1946 | 1531 | | 1777 | 1531 |
| Volume (vph) | 174 | 1081 | 498 | 92 | 282 | 34 | 199 | 351 | 216 | 21 | 149 | 39 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 189 | 1175 | 541 | 100 | 307 | 37 | 216 | 382 | 235 | 23 | 162 | 42 |
| RTOR Reduction (vph) | 0 | 0 | 243 | 0 | 0 | 17 | 0 | 0 | 23 | 0 | 0 | 28 |
| Lane Group Flow (vph) | 189 | 1175 | 298 | 100 | 307 | 20 | 216 | 382 | 212 | 0 | 185 | 14 |
| Turn Type | Perm | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | 4 |
| Actuated Green, G (s) | 36.5 | 36.5 | 36.5 | 36.5 | 36.5 | 36.5 | 20.5 | 20.5 | 20.5 | | 20.5 | 20.5 |
| Effective Green, g (s) | 38.5 | 38.5 | 38.5 | 38.5 | 38.5 | 38.5 | 23.5 | 23.5 | 23.5 | | 23.5 | 23.5 |
| Actuated g/C Ratio | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.55 | 0.34 | 0.34 | 0.34 | | 0.34 | 0.34 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 7.0 | 7.0 | 7.0 | | 7.0 | 7.0 |
| Vehicle Extension (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Grp Cap (vph) | 559 | 1925 | 842 | 161 | 1925 | 842 | 366 | 653 | 514 | | 597 | 514 |
| v/s Ratio Prot | | 0.34 | | | 0.09 | | | 0.20 | | | | |
| v/s Ratio Perm | 0.19 | | 0.19 | c0.34 | | 0.01 | c0.20 | | 0.14 | | 0.10 | 0.01 |
| v/c Ratio | 0.34 | 0.61 | 0.35 | 0.62 | 0.16 | 0.02 | 0.59 | 0.58 | 0.41 | | 0.31 | 0.03 |
| Uniform Delay, d ₁ | 8.7 | 10.7 | 8.8 | 10.8 | 7.8 | 7.2 | 19.3 | 19.2 | 17.9 | | 17.2 | 15.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.23 | 1.03 | 1.45 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 |
| Incremental Delay, d ₂ | 1.6 | 1.5 | 1.2 | 14.8 | 0.2 | 0.0 | 3.0 | 1.6 | 0.7 | | 0.4 | 0.0 |
| Delay (s) | 10.3 | 12.1 | 10.0 | 28.0 | 8.2 | 10.4 | 22.2 | 20.8 | 18.7 | | 17.6 | 15.6 |
| Level of Service | B | B | A | C | A | B | C | C | B | | B | B |
| Approach Delay (s) | | 11.3 | | | 12.8 | | | 20.6 | | | 17.3 | |
| Approach LOS | | B | | | B | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 14.2 | | | | HCM Level of Service | | | | B | |
| HCM Volume to Capacity ratio | | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.0 | | | | Sum of lost time (s) | | | | 8.0 | |
| Intersection Capacity Utilization | | | 79.0% | | | | ICU Level of Service | | | | D | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

21: Halson & Wilson

11/11/2010

| |  |  |  |  |  |  |  |  |  |  |  |  | |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|-----|
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR | |
| Lane Configurations | |  |  | |  | |  |  |  |  |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Lane Width | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | |
| Total Lost time (s) | | 4.0 | 4.0 | | 4.0 | | | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | | | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Flt | | 1.00 | 0.85 | | 1.00 | | | 1.00 | 0.85 | 1.00 | 1.00 | | |
| Flt Protected | | 0.95 | 1.00 | | 0.98 | | | 1.00 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (prot) | | 1711 | 1566 | | 1771 | | | 1801 | 1531 | 1711 | 1801 | | |
| Flt Permitted | | 0.75 | 1.00 | | 0.89 | | | 1.00 | 1.00 | 0.10 | 1.00 | | |
| Satd. Flow (perm) | | 1350 | 1566 | | 1611 | | | 1801 | 1531 | 185 | 1801 | | |
| Volume (vph) | 517 | 0 | 169 | 4 | 7 | 0 | 0 | 604 | 346 | 202 | 667 | 0 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Adj. Flow (vph) | 562 | 0 | 184 | 4 | 8 | 0 | 0 | 657 | 376 | 220 | 725 | 0 | |
| RTOR Reduction (vph) | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 230 | 0 | 0 | 0 | |
| Lane Group Flow (vph) | 0 | 562 | 140 | 0 | 12 | 0 | 0 | 657 | 146 | 220 | 725 | 0 | |
| Turn Type | Perm | | Perm | Perm | | | Perm | | Perm | pm+pt | | | |
| Protected Phases | | 8 | | | 4 | | | 2 | | 1 | 6 | | |
| Permitted Phases | 8 | | 8 | 4 | | | 2 | | 2 | 6 | 6 | | |
| Actuated Green, G (s) | | 33.0 | 33.0 | | 33.0 | | | 34.0 | 34.0 | 47.0 | 47.0 | | |
| Effective Green, g (s) | | 34.0 | 34.0 | | 34.0 | | | 35.0 | 35.0 | 48.0 | 48.0 | | |
| Actuated g/C Ratio | | 0.38 | 0.38 | | 0.38 | | | 0.39 | 0.39 | 0.53 | 0.53 | | |
| Clearance Time (s) | | 5.0 | 5.0 | | 5.0 | | | 5.0 | 5.0 | 3.0 | 5.0 | | |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | | | 3.5 | 3.5 | 3.0 | 3.5 | | |
| Lane Grp Cap (vph) | | 510 | 592 | | 609 | | | 700 | 595 | 251 | 961 | | |
| v/s Ratio Prot | | | | | | | | 0.36 | | c0.09 | 0.40 | | |
| v/s Ratio Perm | | c0.42 | 0.09 | | 0.01 | | | | 0.10 | c0.38 | | | |
| v/c Ratio | | 1.10 | 0.24 | | 0.02 | | | 0.94 | 0.25 | 0.88 | 0.75 | | |
| Uniform Delay, d1 | | 28.0 | 19.1 | | 17.6 | | | 26.5 | 18.6 | 21.7 | 16.4 | | |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | | | 0.73 | 0.50 | 1.45 | 0.69 | | |
| Incremental Delay, d2 | | 70.7 | 0.2 | | 0.0 | | | 21.1 | 0.9 | 24.2 | 4.7 | | |
| Delay (s) | | 98.7 | 19.3 | | 17.6 | | | 40.5 | 10.2 | 55.6 | 16.1 | | |
| Level of Service | | F | B | | B | | | D | B | E | B | | |
| Approach Delay (s) | | 79.1 | | | 17.6 | | | 29.5 | | | 25.3 | | |
| Approach LOS | | E | | | B | | | C | | | C | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM Average Control Delay | | | 41.5 | | | | | | | | | HCM Level of Service | D |
| HCM Volume to Capacity ratio | | | 0.96 | | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | | | | | | | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | | | 88.7% | | | | | | | | | ICU Level of Service | E |
| Analysis Period (min) | | | 15 | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

31: Mohawk/Rosseaux & McNiven

11/11/2010
























| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|--------|-------|-------|------|----------------------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1750 | 1842 | 1566 | 1750 | 1842 | 1566 | 1711 | 1842 | 1531 | 1711 | 1782 | |
| Fl _t Permitted | 0.29 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 | 0.73 | 1.00 | 1.00 | 0.72 | 1.00 | |
| Satd. Flow (perm) | 527 | 1842 | 1566 | 175 | 1842 | 1566 | 1320 | 1842 | 1531 | 1290 | 1782 | |
| Volume (vph) | 15 | 740 | 427 | 1167 | 660 | 42 | 1392 | 57 | 774 | 18 | 27 | 7 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 16 | 804 | 464 | 1268 | 717 | 46 | 1513 | 62 | 841 | 20 | 29 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 105 | 0 | 0 | 17 | 0 | 0 | 289 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 16 | 804 | 359 | 1268 | 717 | 29 | 1513 | 62 | 552 | 20 | 33 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | 8 | 4 | | |
| Actuated Green, G (s) | 36.1 | 36.1 | 36.1 | 72.1 | 72.1 | 72.1 | 66.3 | 66.3 | 66.3 | 66.3 | 66.3 | |
| Effective Green, g (s) | 38.0 | 38.0 | 38.0 | 74.0 | 74.0 | 74.0 | 68.0 | 68.0 | 68.0 | 68.0 | 68.0 | |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.25 | 0.49 | 0.49 | 0.49 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 | |
| Clearance Time (s) | 5.9 | 5.9 | 5.9 | 3.0 | 5.9 | 5.9 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 | |
| Vehicle Extension (s) | 3.5 | 3.5 | 3.5 | 2.0 | 3.5 | 3.5 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 134 | 467 | 397 | 422 | 909 | 773 | 598 | 835 | 694 | 585 | 808 | |
| v/s Ratio Prot | | 0.44 | | c0.64 | 0.39 | | | 0.03 | | | 0.02 | |
| v/s Ratio Perm | 0.03 | | 0.23 | c0.84 | | 0.02 | c1.15 | | 0.36 | 0.02 | | |
| v/c Ratio | 0.12 | 1.72 | 0.90 | 3.00 | 0.79 | 0.04 | 2.53 | 0.07 | 0.80 | 0.03 | 0.04 | |
| Uniform Delay, d ₁ | 43.1 | 56.0 | 54.2 | 61.2 | 31.5 | 19.6 | 41.0 | 23.2 | 35.1 | 22.8 | 22.8 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.5 | 333.7 | 23.6 | 908.5 | 4.7 | 0.0 | 693.5 | 0.0 | 5.9 | 0.0 | 0.0 | |
| Delay (s) | 43.6 | 389.7 | 77.9 | 969.6 | 36.3 | 19.6 | 734.5 | 23.2 | 41.0 | 22.8 | 22.8 | |
| Level of Service | D | F | E | F | D | B | F | C | D | C | C | |
| Approach Delay (s) | | 272.7 | | | 618.6 | | | 474.8 | | | 22.8 | |
| Approach LOS | | F | | | F | | | F | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 476.0 | | | | HCM Level of Service | | | F | | |
| HCM Volume to Capacity ratio | | | 2.75 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 150.0 | | | | Sum of lost time (s) | | 8.0 | | | |
| Intersection Capacity Utilization | | | 197.4% | | | | ICU Level of Service | | H | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

47: Fiddler's Green & Wilson

11/11/2010

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  |  | |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1661 | | 1750 | 1842 | 1531 | 1750 | 1842 | 1531 |
| Fl _t Permitted | 0.46 | 1.00 | 1.00 | 0.69 | 1.00 | | 0.20 | 1.00 | 1.00 | 0.29 | 1.00 | 1.00 |
| Satd. Flow (perm) | 823 | 1801 | 1531 | 1244 | 1661 | | 370 | 1842 | 1531 | 529 | 1842 | 1531 |
| Volume (vph) | 188 | 94 | 126 | 51 | 108 | 115 | 151 | 511 | 244 | 228 | 648 | 11 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 204 | 102 | 137 | 55 | 117 | 125 | 164 | 555 | 265 | 248 | 704 | 12 |
| RTOR Reduction (vph) | 0 | 0 | 99 | 0 | 54 | 0 | 0 | 0 | 121 | 0 | 0 | 2 |
| Lane Group Flow (vph) | 204 | 102 | 38 | 55 | 188 | 0 | 164 | 555 | 144 | 248 | 704 | 10 |
| Turn Type | Perm | | Perm | Perm | | | pm+pt | | Perm | pm+pt | | Perm |
| Protected Phases | | 8 | | | 4 | | 5 | 2 | | 1 | | 6 |
| Permitted Phases | 8 | | 8 | 4 | | | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 22.7 | 22.7 | 22.7 | 22.7 | 22.7 | | 50.9 | 43.3 | 43.3 | 53.7 | 44.7 | 44.7 |
| Effective Green, g (s) | 24.7 | 24.7 | 24.7 | 24.7 | 24.7 | | 51.9 | 45.3 | 45.3 | 54.7 | 46.7 | 46.7 |
| Actuated g/C Ratio | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | | 0.58 | 0.50 | 0.50 | 0.61 | 0.52 | 0.52 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 2.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 226 | 494 | 420 | 341 | 456 | | 315 | 927 | 771 | 430 | 956 | 794 |
| v/s Ratio Prot | | 0.06 | | | 0.11 | | 0.04 | 0.30 | | c0.05 | c0.38 | |
| v/s Ratio Perm | c0.25 | | 0.02 | 0.04 | | | 0.26 | | 0.09 | 0.30 | | 0.01 |
| v/c Ratio | 0.90 | 0.21 | 0.09 | 0.16 | 0.41 | | 0.52 | 0.60 | 0.19 | 0.58 | 0.74 | 0.01 |
| Uniform Delay, d ₁ | 31.5 | 25.1 | 24.3 | 24.8 | 26.7 | | 12.5 | 15.9 | 12.3 | 10.4 | 16.9 | 10.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.04 | 0.90 | 0.62 | 1.01 | 1.02 | 1.01 |
| Incremental Delay, d ₂ | 34.6 | 0.2 | 0.1 | 0.2 | 0.6 | | 0.7 | 2.7 | 0.5 | 0.5 | 2.2 | 0.0 |
| Delay (s) | 66.1 | 25.3 | 24.4 | 25.0 | 27.3 | | 13.7 | 17.0 | 8.1 | 11.0 | 19.4 | 10.6 |
| Level of Service | E | C | C | C | C | | B | B | A | B | B | B |
| Approach Delay (s) | | 43.8 | | | 26.9 | | | 14.0 | | | 17.1 | |
| Approach LOS | | D | | | C | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.5 | | | | HCM Level of Service | | | | C | |
| HCM Volume to Capacity ratio | | | 0.75 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | | Sum of lost time (s) | | | | 8.0 | |
| Intersection Capacity Utilization | | | 78.9% | | | | ICU Level of Service | | | | D | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

51: Golf Links & Kitty Murray

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|-------|------|------|------|------|-------|-------|------|
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘↗ | ↑↑ | ↗ | ↘ | ↗ | | ↘↗ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.86 | | 1.00 | 0.92 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 3319 | 3500 | 1531 | 1711 | 1586 | | 3319 | 1693 | |
| Fl _t Permitted | 0.29 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.71 | 1.00 | | 0.16 | 1.00 | |
| Satd. Flow (perm) | 531 | 3500 | 1531 | 3319 | 3500 | 1531 | 1287 | 1586 | | 542 | 1693 | |
| Volume (vph) | 158 | 1139 | 122 | 273 | 670 | 228 | 361 | 38 | 477 | 221 | 28 | 32 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 172 | 1238 | 133 | 297 | 728 | 248 | 392 | 41 | 518 | 240 | 30 | 35 |
| RTOR Reduction (vph) | 0 | 0 | 79 | 0 | 0 | 140 | 0 | 183 | 0 | 0 | 22 | 0 |
| Lane Group Flow (vph) | 172 | 1238 | 54 | 297 | 728 | 108 | 392 | 376 | 0 | 240 | 43 | 0 |
| Turn Type | pm+pt | | Perm | Prot | | Perm | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 2 | | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 46.4 | 37.8 | 37.8 | 11.2 | 40.4 | 40.4 | 34.0 | 34.0 | | 34.0 | 34.0 | |
| Effective Green, g (s) | 48.4 | 40.8 | 40.8 | 10.2 | 43.4 | 43.4 | 37.0 | 37.0 | | 37.0 | 37.0 | |
| Actuated g/C Ratio | 0.48 | 0.41 | 0.41 | 0.10 | 0.43 | 0.43 | 0.37 | 0.37 | | 0.37 | 0.37 | |
| Clearance Time (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 7.0 | 7.0 | | 7.0 | 7.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 347 | 1428 | 625 | 339 | 1519 | 664 | 476 | 587 | | 201 | 626 | |
| v/s Ratio Prot | 0.04 | c0.35 | | c0.09 | c0.21 | | | 0.24 | | | 0.03 | |
| v/s Ratio Perm | 0.20 | | 0.04 | | | 0.07 | 0.30 | | | c0.44 | | |
| v/c Ratio | 0.50 | 0.87 | 0.09 | 0.88 | 0.48 | 0.16 | 0.82 | 0.64 | | 1.19 | 0.07 | |
| Uniform Delay, d ₁ | 15.3 | 27.1 | 18.2 | 44.3 | 20.2 | 17.2 | 28.5 | 26.0 | | 31.5 | 20.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.4 | 7.3 | 0.3 | 20.9 | 1.1 | 0.5 | 14.9 | 5.3 | | 125.6 | 0.2 | |
| Delay (s) | 15.7 | 34.4 | 18.4 | 65.2 | 21.3 | 17.8 | 43.4 | 31.3 | | 157.1 | 20.6 | |
| Level of Service | B | C | B | E | C | B | D | C | | F | C | |
| Approach Delay (s) | | 31.0 | | | 30.9 | | | 36.3 | | | 128.0 | |
| Approach LOS | | C | | | C | | | D | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 39.4 | HCM Level of Service | D |
| HCM Volume to Capacity ratio | 1.04 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 16.0 |
| Intersection Capacity Utilization | 92.4% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

52: Golf Links & Stone Church

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|-------|------|------|--------|------|--------|------|------|------|
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑ | | ↑ | | ↑ | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.95 | | 1.00 | | 1.00 | 0.91 | 0.91 | 1.00 |
| Flt | | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | | 1.00 | 0.95 | 0.99 | 1.00 |
| Satd. Flow (prot) | | 4916 | 1531 | 1711 | 3421 | | 1711 | | 1531 | 1628 | 3403 | 1601 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | 0.25 | | 1.00 | 0.95 | 0.99 | 1.00 |
| Satd. Flow (perm) | | 4916 | 1531 | 1711 | 3421 | | 459 | | 1531 | 1628 | 3403 | 1601 |
| Volume (vph) | 0 | 2377 | 284 | 106 | 741 | 0 | 282 | 0 | 433 | 294 | 402 | 351 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 2584 | 309 | 115 | 805 | 0 | 307 | 0 | 471 | 320 | 437 | 382 |
| RTOR Reduction (vph) | 0 | 0 | 173 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 |
| Lane Group Flow (vph) | 0 | 2584 | 136 | 115 | 805 | 0 | 307 | 0 | 471 | 244 | 513 | 282 |
| Turn Type | | | Perm | Prot | | | custom | | custom | Perm | | Perm |
| Protected Phases | | 6 | | 5 | 2 | | 3 | | 5 | | 4 | |
| Permitted Phases | | | 6 | | | | 8 | | 3 | 4 | 4 | 4 |
| Actuated Green, G (s) | | 42.0 | 42.0 | 4.0 | 51.0 | | 37.0 | | 47.0 | 25.0 | 25.0 | 25.0 |
| Effective Green, g (s) | | 44.0 | 44.0 | 5.0 | 53.0 | | 39.0 | | 48.0 | 27.0 | 27.0 | 27.0 |
| Actuated g/C Ratio | | 0.44 | 0.44 | 0.05 | 0.53 | | 0.39 | | 0.48 | 0.27 | 0.27 | 0.27 |
| Clearance Time (s) | | 6.0 | 6.0 | 5.0 | 6.0 | | 3.0 | | | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | 1.0 | 2.0 | | 1.0 | | | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | | 2163 | 674 | 86 | 1813 | | 279 | | 735 | 440 | 919 | 432 |
| v/s Ratio Prot | | c0.53 | | c0.07 | 0.24 | | c0.09 | | 0.31 | | | |
| v/s Ratio Perm | | | 0.09 | | | | c0.34 | | | 0.15 | 0.15 | 0.18 |
| v/c Ratio | | 1.19 | 0.20 | 1.34 | 0.44 | | 1.10 | | 0.64 | 0.55 | 0.56 | 0.65 |
| Uniform Delay, d1 | | 28.0 | 17.2 | 47.5 | 14.4 | | 28.4 | | 19.5 | 31.3 | 31.4 | 32.3 |
| Progression Factor | | 0.99 | 1.62 | 1.05 | 0.96 | | 1.60 | | 1.59 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 88.0 | 0.1 | 190.3 | 0.5 | | 71.8 | | 0.9 | 0.9 | 0.4 | 2.7 |
| Delay (s) | | 115.9 | 28.0 | 240.3 | 14.4 | | 117.1 | | 32.0 | 32.2 | 31.8 | 35.0 |
| Level of Service | | F | C | F | B | | F | | C | C | C | D |
| Approach Delay (s) | | 106.5 | | | 42.6 | | | 65.6 | | | 33.0 | |
| Approach LOS | | F | | | D | | | E | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|------|
| HCM Average Control Delay | 76.1 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.15 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 107.4% | ICU Level of Service | G |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
72: Golf Links Rd & Martindale

11/11/2010



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|------------------------|------|-------|------|------|-------|------|
| Lane Configurations | ↖↖ | ↑↑ | ↗↗ | ↗ | ↘↘ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.5 | 3.3 | 3.3 | 3.5 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 0.97 | 0.95 | 0.95 | 1.00 | 0.97 | |
| Flt | 1.00 | 1.00 | 1.00 | 0.85 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.96 | |
| Satd. Flow (prot) | 3319 | 3500 | 3500 | 1531 | 3298 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.96 | |
| Satd. Flow (perm) | 3319 | 3500 | 3500 | 1531 | 3298 | |
| Volume (vph) | 408 | 2290 | 948 | 262 | 942 | 87 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 443 | 2489 | 1030 | 285 | 1024 | 95 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 161 | 7 | 0 |
| Lane Group Flow (vph) | 443 | 2489 | 1030 | 124 | 1112 | 0 |
| Turn Type | Prot | | Perm | | | |
| Protected Phases | 1 | 6 | 2 | | 4 | |
| Permitted Phases | | 1 | | 2 | | |
| Actuated Green, G (s) | 15.6 | 60.0 | 41.4 | 41.4 | 28.0 | |
| Effective Green, g (s) | 14.6 | 62.0 | 43.4 | 43.4 | 30.0 | |
| Actuated g/C Ratio | 0.15 | 0.62 | 0.43 | 0.43 | 0.30 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 4.0 | 1.0 | |
| Lane Grp Cap (vph) | 485 | 2170 | 1519 | 664 | 989 | |
| v/s Ratio Prot | 0.13 | c0.71 | 0.29 | | c0.34 | |
| v/s Ratio Perm | | | | 0.08 | | |
| v/c Ratio | 0.91 | 1.15 | 0.68 | 0.19 | 1.12 | |
| Uniform Delay, d1 | 42.1 | 19.0 | 22.7 | 17.4 | 35.0 | |
| Progression Factor | 1.00 | 1.00 | 0.88 | 1.77 | 1.00 | |
| Incremental Delay, d2 | 21.2 | 72.1 | 2.2 | 0.5 | 69.3 | |
| Delay (s) | 63.3 | 91.1 | 22.1 | 31.4 | 104.3 | |
| Level of Service | E | F | C | C | F | |
| Approach Delay (s) | | 86.9 | 24.1 | | 104.3 | |
| Approach LOS | | F | C | | F | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 75.1 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.14 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 99.6% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

75: Golf Links Rd & Neville

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|-------|------|------|------|------|------|--------|--------|------|
| Lane Configurations | ↘ | ↑↑ | ↗ | ↘ | ↑↑ | ↗ | ↘ | ↗ | | ↗↘ | ↗ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 | 3.3 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | | 0.97 | 1.00 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 0.94 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 3500 | 1531 | 1711 | 3500 | 1531 | 1711 | 1655 | | 3319 | 1740 | |
| Fl _t Permitted | 0.23 | 1.00 | 1.00 | 0.08 | 1.00 | 1.00 | 0.34 | 1.00 | | 0.25 | 1.00 | |
| Satd. Flow (perm) | 409 | 3500 | 1531 | 148 | 3500 | 1531 | 619 | 1655 | | 882 | 1740 | |
| Volume (vph) | 238 | 2342 | 165 | 227 | 808 | 188 | 140 | 118 | 246 | 1124 | 190 | 112 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 259 | 2546 | 179 | 247 | 878 | 204 | 152 | 128 | 267 | 1222 | 207 | 122 |
| RTOR Reduction (vph) | 0 | 0 | 53 | 0 | 0 | 104 | 0 | 75 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 259 | 2546 | 126 | 247 | 878 | 100 | 152 | 320 | 0 | 1222 | 308 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | Perm | | |
| Protected Phases | 1 | 6 | | 5 | 2 | | | 8 | | | 4 | |
| Permitted Phases | 6 | | 6 | 2 | | 2 | 8 | | | 4 | | |
| Actuated Green, G (s) | 58.2 | 48.0 | 48.0 | 55.8 | 46.8 | 46.8 | 28.0 | 28.0 | | 28.0 | 28.0 | |
| Effective Green, g (s) | 59.2 | 50.0 | 50.0 | 56.8 | 48.8 | 48.8 | 30.0 | 30.0 | | 30.0 | 30.0 | |
| Actuated g/C Ratio | 0.59 | 0.50 | 0.50 | 0.57 | 0.49 | 0.49 | 0.30 | 0.30 | | 0.30 | 0.30 | |
| Clearance Time (s) | 3.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 6.0 | 6.0 | |
| Vehicle Extension (s) | 1.0 | 4.0 | 4.0 | 1.0 | 4.0 | 4.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 362 | 1750 | 766 | 209 | 1708 | 747 | 186 | 497 | | 265 | 522 | |
| v/s Ratio Prot | 0.07 | c0.73 | | c0.09 | 0.25 | | | 0.19 | | | 0.18 | |
| v/s Ratio Perm | 0.36 | | 0.08 | 0.58 | | 0.07 | 0.25 | | | c1.39 | | |
| v/c Ratio | 0.72 | 1.45 | 0.16 | 1.18 | 0.51 | 0.13 | 0.82 | 0.64 | | 4.61 | 0.59 | |
| Uniform Delay, d ₁ | 11.8 | 25.0 | 13.6 | 48.2 | 17.5 | 14.0 | 32.5 | 30.4 | | 35.0 | 29.8 | |
| Progression Factor | 1.05 | 0.96 | 0.82 | 1.15 | 1.00 | 1.56 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 0.5 | 205.0 | 0.0 | 112.6 | 0.8 | 0.3 | 22.4 | 2.1 | | 1633.7 | 1.2 | |
| Delay (s) | 12.9 | 229.0 | 11.3 | 168.0 | 18.4 | 22.1 | 54.8 | 32.5 | | 1668.7 | 31.0 | |
| Level of Service | B | F | B | F | B | C | D | C | | F | C | |
| Approach Delay (s) | | 197.2 | | | 46.8 | | | 38.7 | | | 1321.3 | |
| Approach LOS | | F | | | D | | | D | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 424.4 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 2.40 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 144.0% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

78: Golf Links & McNiven

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|-------|------|-------|------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↔ | ↑ | ↔ | ↔ | ↑ | ↔ | ↔ | ↑↔ | | ↔ | ↔ | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 0.95 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 | 1711 | 3347 | | 1711 | 1711 | |
| Flt Permitted | 0.57 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 | 0.13 | 1.00 | | 0.11 | 1.00 | |
| Satd. Flow (perm) | 1031 | 1801 | 1531 | 193 | 1801 | 1531 | 230 | 3347 | | 204 | 1711 | |
| Volume (vph) | 41 | 538 | 107 | 213 | 284 | 663 | 297 | 756 | 128 | 739 | 443 | 220 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 45 | 585 | 116 | 232 | 309 | 721 | 323 | 822 | 139 | 803 | 482 | 239 |
| RTOR Reduction (vph) | 0 | 0 | 66 | 0 | 0 | 331 | 0 | 11 | 0 | 0 | 15 | 0 |
| Lane Group Flow (vph) | 45 | 585 | 50 | 232 | 309 | 390 | 323 | 950 | 0 | 803 | 706 | 0 |
| Turn Type | Perm | | Perm | pm+pt | | Perm | pm+pt | | | pm+pt | | |
| Protected Phases | | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 31.3 | 31.3 | 31.3 | 43.3 | 43.3 | 43.3 | 46.0 | 29.0 | | 64.0 | 43.0 | |
| Effective Green, g (s) | 33.4 | 33.4 | 33.4 | 45.4 | 45.4 | 45.4 | 48.3 | 31.3 | | 66.3 | 45.3 | |
| Actuated g/C Ratio | 0.28 | 0.28 | 0.28 | 0.38 | 0.38 | 0.38 | 0.40 | 0.26 | | 0.55 | 0.38 | |
| Clearance Time (s) | 6.1 | 6.1 | 6.1 | 4.0 | 6.1 | 6.1 | 4.0 | 6.3 | | 4.0 | 6.3 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 288 | 503 | 427 | 175 | 683 | 581 | 303 | 875 | | 503 | 648 | |
| v/s Ratio Prot | | 0.32 | | c0.09 | 0.17 | | 0.15 | 0.28 | | c0.41 | 0.41 | |
| v/s Ratio Perm | 0.04 | | 0.03 | c0.42 | | 0.25 | 0.28 | | | c0.47 | | |
| v/c Ratio | 0.16 | 1.16 | 0.12 | 1.33 | 0.45 | 0.67 | 1.07 | 1.09 | | 1.60 | 1.09 | |
| Uniform Delay, d1 | 32.5 | 43.2 | 32.2 | 58.1 | 27.8 | 30.9 | 35.5 | 44.2 | | 36.1 | 37.2 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 93.4 | 0.1 | 180.6 | 0.5 | 3.0 | 70.3 | 56.4 | | 277.6 | 62.2 | |
| Delay (s) | 32.8 | 136.6 | 32.3 | 238.6 | 28.3 | 34.0 | 105.7 | 100.6 | | 313.7 | 99.4 | |
| Level of Service | C | F | C | F | C | C | F | F | | F | F | |
| Approach Delay (s) | | 114.1 | | | 70.2 | | | 101.9 | | | 212.3 | |
| Approach LOS | | F | | | E | | | F | | | F | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 130.4 | HCM Level of Service | F |
| HCM Volume to Capacity ratio | 1.45 | | |
| Actuated Cycle Length (s) | 119.7 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 119.4% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

HCM Signalized Intersection Capacity Analysis

90: Garner & Southcote

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|-------|------|------|-------|------|------|-------|------|------|
| Lane Configurations | ↙ | ↕ | ↘ | ↙ | ↕ | ↘ | ↙ | ↕ | ↘ | ↙ | ↕ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.0 | 3.5 | 3.3 | 3.0 | 3.5 | 3.3 | 3.3 | 3.3 | 3.3 | 3.0 | 3.5 | 3.3 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.92 | |
| Fl _t Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1652 | 3500 | 1531 | 1652 | 3500 | 1531 | 1711 | 3332 | | 1652 | 3219 | |
| Fl _t Permitted | 0.11 | 1.00 | 1.00 | 0.31 | 1.00 | 1.00 | 0.22 | 1.00 | | 0.18 | 1.00 | |
| Satd. Flow (perm) | 188 | 3500 | 1531 | 530 | 3500 | 1531 | 400 | 3332 | | 316 | 3219 | |
| Volume (vph) | 541 | 862 | 67 | 117 | 1152 | 295 | 74 | 459 | 97 | 200 | 452 | 519 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 588 | 937 | 73 | 127 | 1252 | 321 | 80 | 499 | 105 | 217 | 491 | 564 |
| RTOR Reduction (vph) | 0 | 0 | 36 | 0 | 0 | 147 | 0 | 18 | 0 | 0 | 207 | 0 |
| Lane Group Flow (vph) | 588 | 937 | 37 | 127 | 1252 | 174 | 80 | 586 | 0 | 217 | 848 | 0 |
| Turn Type | pm+pt | | Perm | pm+pt | | Perm | Perm | | | pm+pt | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | 7 | 4 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 61.0 | 48.9 | 48.9 | 39.1 | 31.0 | 31.0 | 16.0 | 16.0 | | 27.0 | 27.0 | |
| Effective Green, g (s) | 63.0 | 50.9 | 50.9 | 41.1 | 33.0 | 33.0 | 18.0 | 18.0 | | 29.0 | 29.0 | |
| Actuated g/C Ratio | 0.63 | 0.51 | 0.51 | 0.41 | 0.33 | 0.33 | 0.18 | 0.18 | | 0.29 | 0.29 | |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 499 | 1782 | 779 | 309 | 1155 | 505 | 72 | 600 | | 185 | 934 | |
| v/s Ratio Prot | c0.31 | 0.27 | | 0.03 | 0.36 | | | 0.18 | | c0.08 | 0.26 | |
| v/s Ratio Perm | c0.44 | | 0.02 | 0.14 | | 0.11 | 0.20 | | | c0.26 | | |
| v/c Ratio | 1.18 | 0.53 | 0.05 | 0.41 | 1.08 | 0.35 | 1.11 | 0.98 | | 1.17 | 0.91 | |
| Uniform Delay, d ₁ | 39.2 | 16.5 | 12.4 | 18.8 | 33.5 | 25.3 | 41.0 | 40.8 | | 33.2 | 34.2 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d ₂ | 99.5 | 0.5 | 0.0 | 0.9 | 52.3 | 0.7 | 139.6 | 30.6 | | 120.5 | 12.3 | |
| Delay (s) | 138.7 | 16.9 | 12.4 | 19.7 | 85.8 | 26.0 | 180.6 | 71.3 | | 153.7 | 46.5 | |
| Level of Service | F | B | B | B | F | C | F | E | | F | D | |
| Approach Delay (s) | | 61.5 | | | 69.6 | | | 84.1 | | | 64.8 | |
| Approach LOS | | E | | | E | | | F | | | E | |

Intersection Summary

| | | | |
|-----------------------------------|--------|----------------------|-----|
| HCM Average Control Delay | 67.9 | HCM Level of Service | E |
| HCM Volume to Capacity ratio | 1.14 | | |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 112.7% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

91: Garner & Kitty Murray

11/11/2010



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|-------|------|------|------|------|------|------|-------|------|------|------|------|
| Lane Configurations | ↘ | ↗↗ | ↘ | ↘ | ↗↗ | ↘ | ↘ | ↗ | ↘ | ↘ | ↗ | ↘ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 3421 | 1531 | 1711 | 3421 | 1531 | 1711 | 1801 | 1531 | 1711 | 1801 | 1531 |
| Flt Permitted | 0.15 | 1.00 | 1.00 | 0.24 | 1.00 | 1.00 | 0.23 | 1.00 | 1.00 | 0.22 | 1.00 | 1.00 |
| Satd. Flow (perm) | 263 | 3421 | 1531 | 440 | 3421 | 1531 | 408 | 1801 | 1531 | 390 | 1801 | 1531 |
| Volume (vph) | 233 | 1066 | 67 | 117 | 919 | 203 | 74 | 459 | 97 | 59 | 451 | 100 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 253 | 1159 | 73 | 127 | 999 | 221 | 80 | 499 | 105 | 64 | 490 | 109 |
| RTOR Reduction (vph) | 0 | 0 | 28 | 0 | 0 | 98 | 0 | 0 | 41 | 0 | 0 | 24 |
| Lane Group Flow (vph) | 253 | 1159 | 45 | 127 | 999 | 123 | 80 | 499 | 64 | 64 | 490 | 85 |
| Turn Type | pm+pt | | Perm | Perm | | Perm | Perm | | Perm | Perm | | Perm |
| Protected Phases | 7 | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 35.4 | 35.4 | 35.4 | 23.4 | 23.4 | 23.4 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Effective Green, g (s) | 35.4 | 35.4 | 35.4 | 23.4 | 23.4 | 23.4 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Actuated g/C Ratio | 0.53 | 0.53 | 0.53 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 315 | 1824 | 816 | 155 | 1206 | 540 | 141 | 624 | 530 | 135 | 624 | 530 |
| v/s Ratio Prot | c0.10 | 0.34 | | | 0.29 | | | c0.28 | | | 0.27 | |
| v/s Ratio Perm | c0.33 | | 0.03 | 0.29 | | 0.08 | 0.20 | | 0.04 | 0.16 | | 0.06 |
| v/c Ratio | 0.80 | 0.64 | 0.06 | 0.82 | 0.83 | 0.23 | 0.57 | 0.80 | 0.12 | 0.47 | 0.79 | 0.16 |
| Uniform Delay, d1 | 12.1 | 10.9 | 7.5 | 19.6 | 19.7 | 15.1 | 17.7 | 19.6 | 14.8 | 17.0 | 19.5 | 15.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 13.7 | 0.7 | 0.0 | 27.4 | 4.8 | 0.2 | 15.5 | 10.3 | 0.5 | 11.5 | 9.6 | 0.6 |
| Delay (s) | 25.8 | 11.7 | 7.5 | 47.0 | 24.5 | 15.4 | 33.2 | 29.9 | 15.3 | 28.4 | 29.1 | 15.7 |
| Level of Service | C | B | A | D | C | B | C | C | B | C | C | B |
| Approach Delay (s) | | 13.9 | | | 25.1 | | | 28.1 | | | 26.8 | |
| Approach LOS | | B | | | C | | | C | | | C | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 21.9 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.78 | | |
| Actuated Cycle Length (s) | 66.4 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 79.5% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |
| c Critical Lane Group | | | |

APPENDIX D
ARCHAEOLOGICAL MEMO



Hamilton

Planning and Economic
Development Department

Memorandum

To:

From: Joseph Muller, Cultural Heritage Planner
Community Planning and Design Section
Planning Division

Phone: 905-546-2424 Ext. 1214

Fax: 905-643-7250

Date: February 11, 2009

File:

Subject: **Proposed Ancaster Transportation Master Plan:
City of Hamilton Archaeology Management Plan
Evaluation of archaeological Potential**

The following comments are provided by the Community Planning and Design Section:

As requested, Heritage Staff have compiled archeological evaluations of the Ancaster area. The evaluations identify the applicable archaeological potential criteria that the Ministry of Culture and the City of Hamilton use and a mapping of the archaeological potential criteria for the applicable area. While many of the areas show surface disturbance, archaeological potential is presumed to exist except where displaced by extant buildings or other development. The legend below includes the layers used to determine the archaeological potential of each area:

| <u>Archaeological Potential Legend:</u> | |
|--|--|
| Streetcenterline (17,659) | HAMP_Unusual_Landforms_catch100m (1) |
| Railway Line (1,396) | HAMP_Historic_Transportation_catch100m (1) |
| Major Lakes (4) | HAMP_Water_catch_Lakes (1) |
| Escarpment (166) | HAMP_Historic_Urban_Boundary (7) |
| Archae_Sites (735) | Heritage (584) |
| HAMP_Archae_Sites_catch250m (735) | Cemeteries (110) |
| HAMP_UnReg_Archae_Sites_Jan07_catch250m | Parks (477) |
| HAMP_Historic_Activity (3,565) | Land Parcels (292,723) |
| HAMP_Historic_Activity_catch100m (2,509) | |
| HAMP_Soil_Types_Sand (630) | |

Western Ancaster

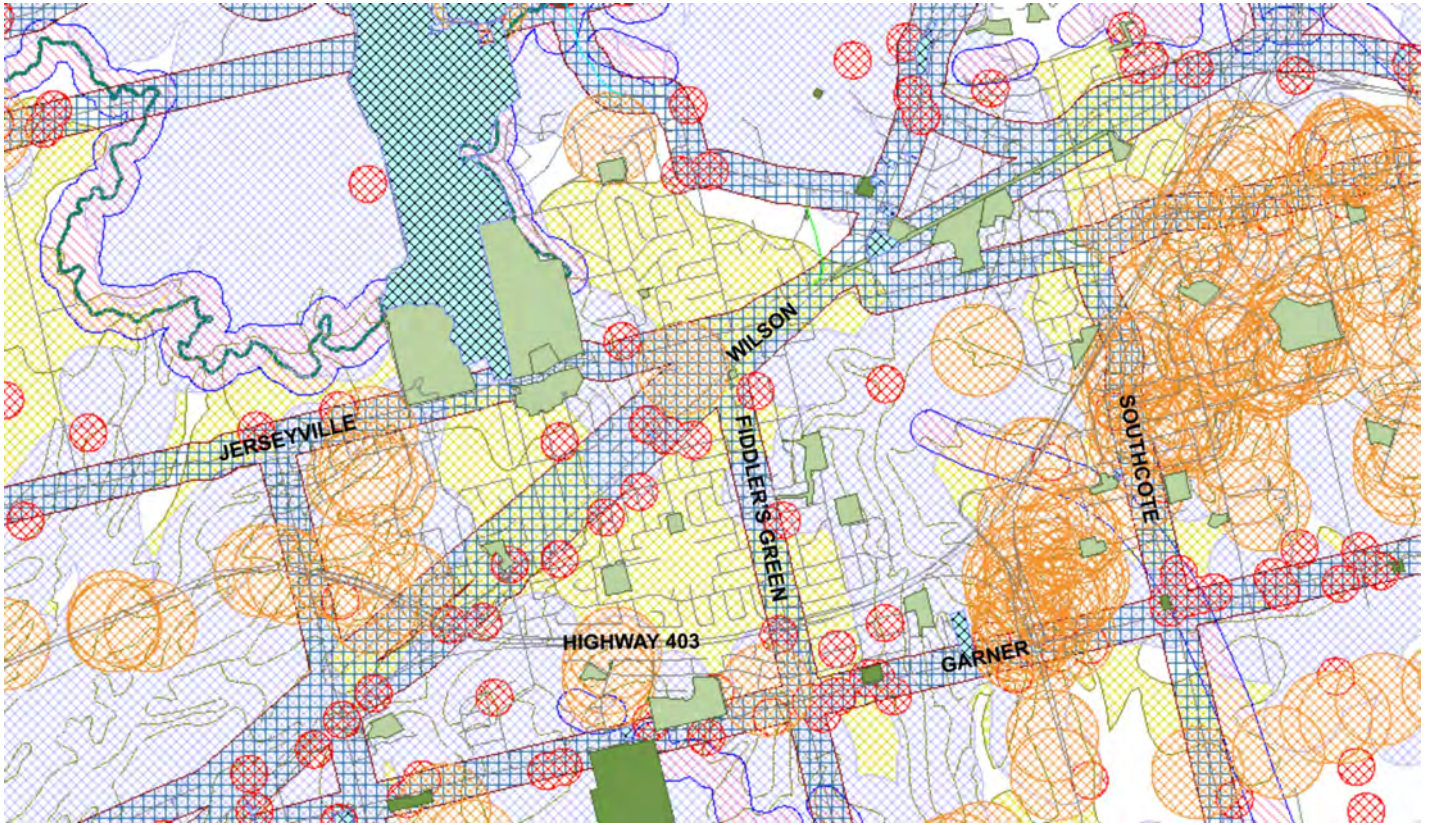


The subject property meets seven of the 11 criteria used by the City of Hamilton and Ministry of Culture for determining archaeological potential:

- 1) Within 250 metres of a known archaeological site/in an area dense with archaeological sites;
- 2) Within 300 metres of water or prehistoric water, or 200 metres of a secondary watercourse;
- 3) Documentary evidence, local knowledge or oral history associates the property with historic activities, events or occupations;
- 4) On well-drained, sandy soil within a clay/stone matrix;
- 5) Associated with unusual landforms;
- 6) Within 100 metres of a historic transportation corridor; and,
- 7) A property designated under the *Ontario Heritage Act*.

These criteria define the property as having archaeological potential.

Central Ancaster

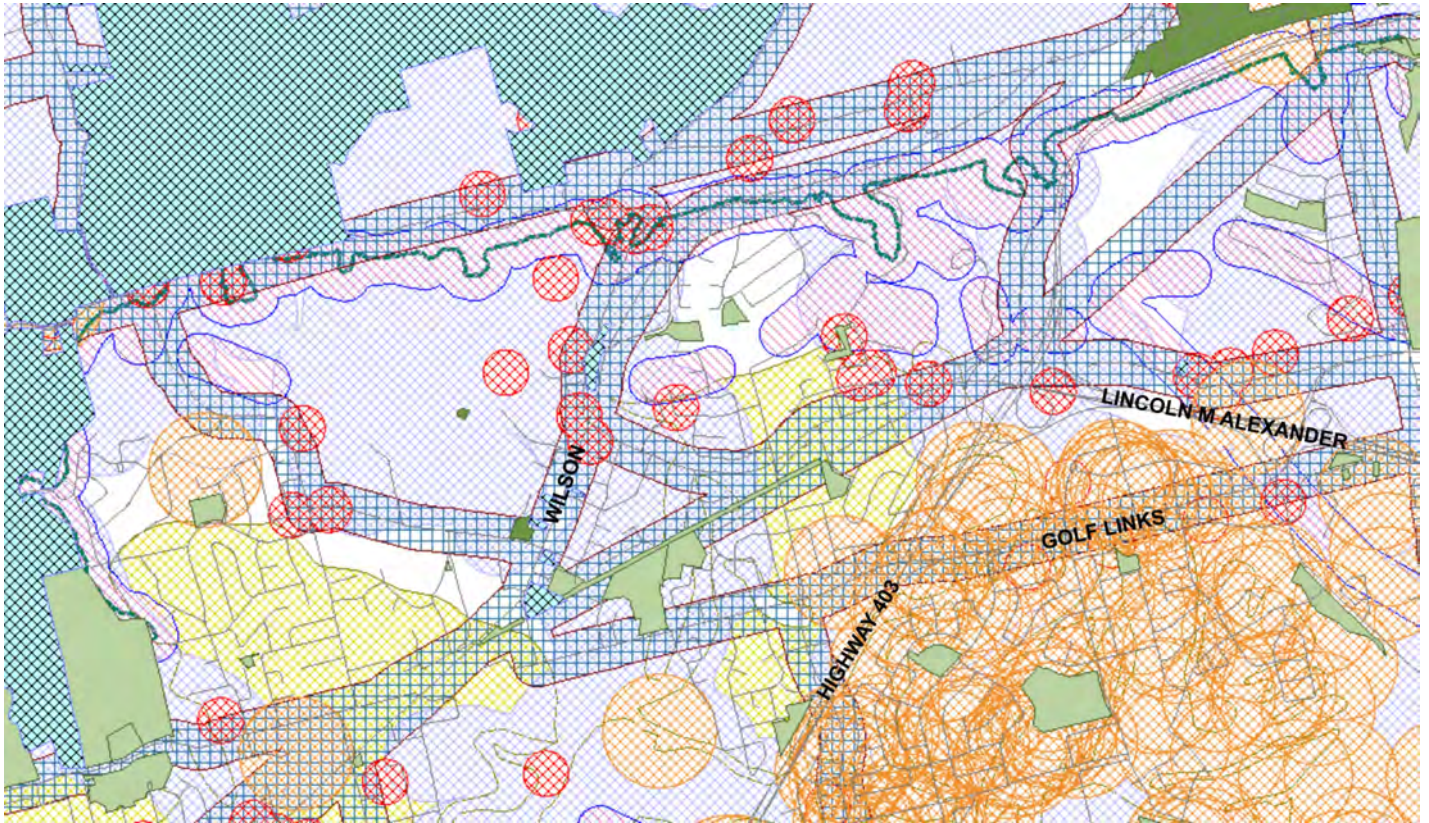


The subject property meets eight of the 11 criteria used by the City of Hamilton and Ministry of Culture for determining archaeological potential:

- 1) Within 250 metres of a known archaeological site/in an area dense with archaeological sites;
- 2) Within 300 metres of water or prehistoric water, or 200 metres of a secondary watercourse;
- 3) Documentary evidence, local knowledge or oral history associates the property with historic activities, events or occupations;
- 4) In an area of elevated topography;
- 5) On well-drained, sandy soil within a clay/stone matrix;
- 6) Associated with unusual landforms;
- 7) Within 100 metres of a historic transportation corridor; and,
- 8) A property designated under the *Ontario Heritage Act*.

These criteria define the property as having archaeological potential.

Northwestern Ancaster

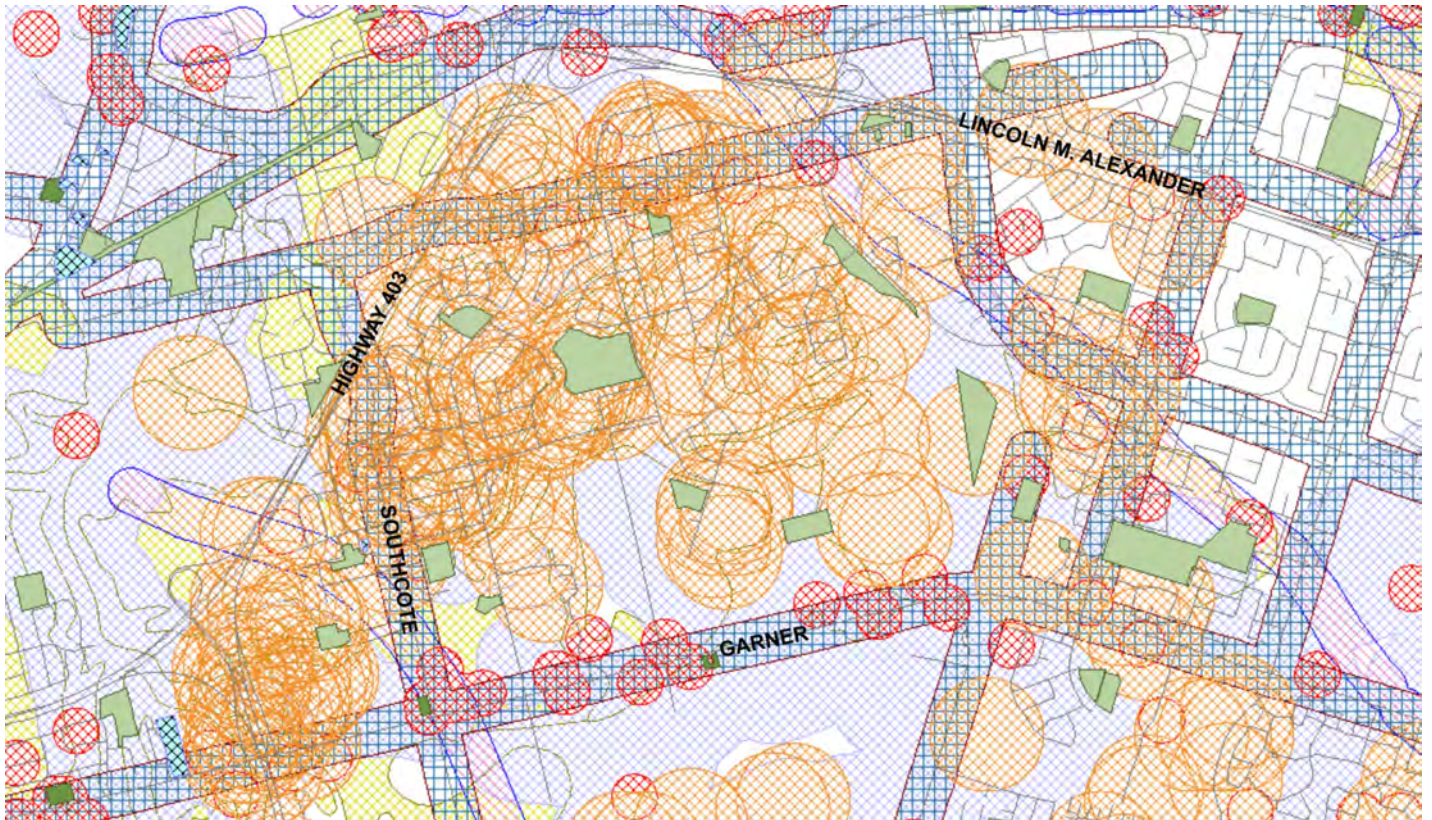


The subject property meets eight of the 11 criteria used by the City of Hamilton and Ministry of Culture for determining archaeological potential:

- 1) Within 250 metres of a known archaeological site/in an area dense with archaeological sites;
- 2) Within 300 metres of water or prehistoric water, or 200 metres of a secondary watercourse;
- 3) Documentary evidence, local knowledge or oral history associates the property with historic activities, events or occupations;
- 4) In an area of elevated topography
- 5) On well-drained, sandy soil within a clay/stone matrix;
- 6) Associated with unusual landforms;
- 7) Within 100 metres of a historic transportation corridor; and,
- 8) A property designated under the *Ontario Heritage Act*.

These criteria define the property as having archaeological potential.

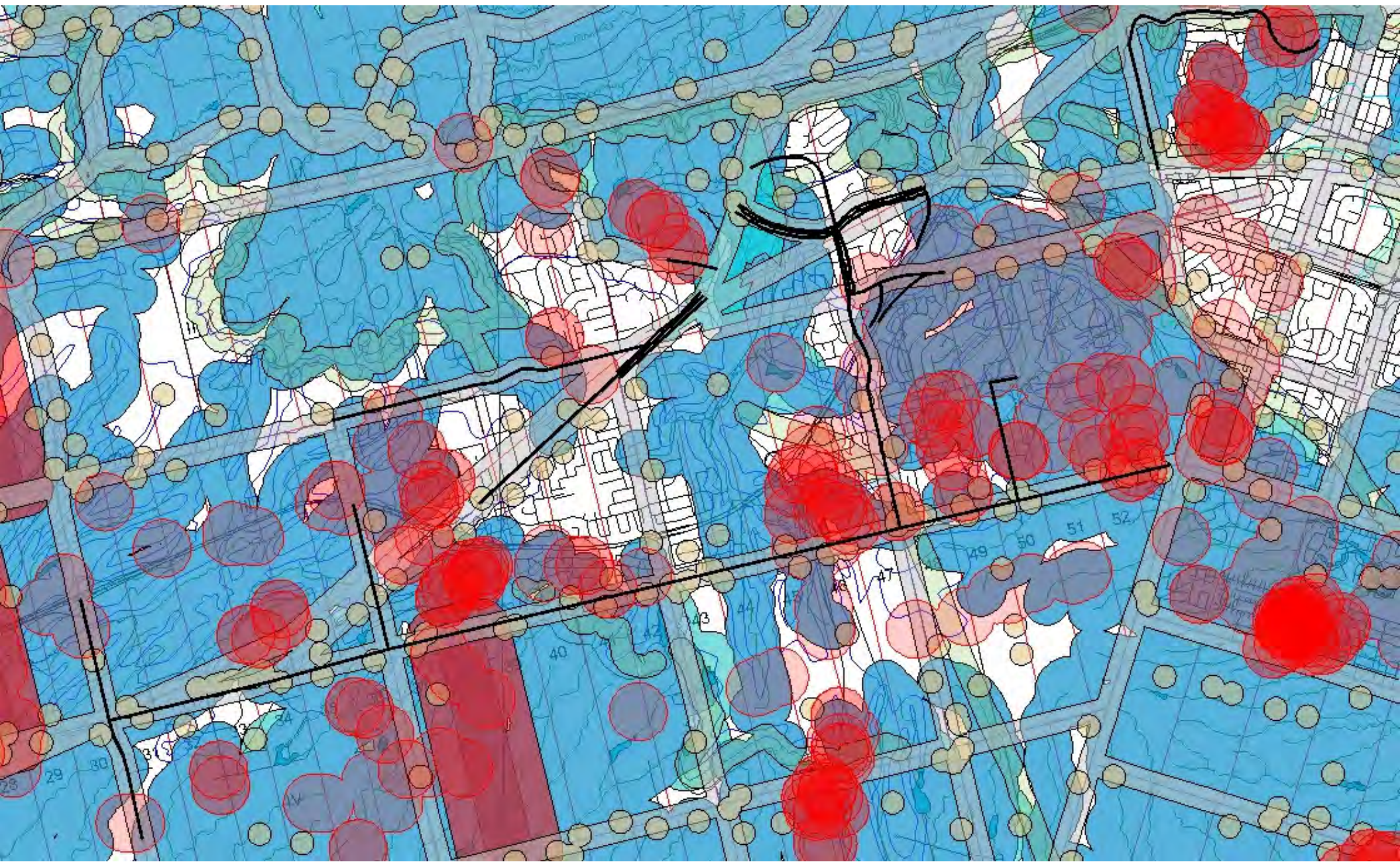
Southeastern Ancaster



The subject property meets eight of the 11 criteria used by the City of Hamilton and Ministry of Culture for determining archaeological potential:

- 1) Within 250 metres of a known archaeological site/in an area dense with archaeological sites;
- 2) Within 300 metres of water or prehistoric water, or 200 metres of a secondary watercourse;
- 3) Documentary evidence, local knowledge or oral history associates the property with historic activities, events or occupations;
- 4) In an area of elevated topography
- 5) On well-drained, sandy soil within a clay/stone matrix;
- 6) Associated with unusual landforms;
- 7) Within 100 metres of a historic transportation corridor; and,
- 8) A property designated under the *Ontario Heritage Act*.

These criteria define the property as having archaeological potential.



Note: Updated archaeology mapping provided by the City of Hamilton March 17, 2011

